# SR 3 Freight Corridor <br> Transportation Discipline Report 

Prepared for
Washington State Department of Transportation


January 2024

## Parametrix

# SR 3 Freight Corridor Transportation Discipline Report 

Prepared for

Washington State Department of Transportation<br>Olympic Region Planning Office<br>5720 Capitol Boulevard, SE<br>Tumwater, WA 98501-5201

Prepared by

## Parametrix

719 2nd Avenue, Suite 200
Seattle, WA 98104
T. 206.394.3700 F. 1.855.542.6353
www.parametrix.com

## Citation

Parametrix. 2024. SR 3 Freight Corridor
Transportation Discipline Report.
Prepared for Washington State Department of Transportation by Parametrix, Seattle, Washington. January 2024.

## Certification

The technical material and data contained in this document were prepared under the supervision and direction of the undersigned, whose seal, as a professional engineer licensed to practice as such, is affixed below.

Prepared by Alex Atchison

Checked and Approved by Mark Yand

## Contents

Executive Summary ..... 1
What is the purpose of this report? ..... 1
What is the Project Description? ..... 1
What is the purpose and need of the project? ..... 1
What are the alternatives analyzed? ..... 4
How were the study limits determined? ..... 4
What methodology was used for traffic analysis and identifying transportation facilities within the area? ..... 4
What is the affected environment? ..... 5
What are the key transportation systems in the study area? ..... 5
What is the existing roadway operative condition in the study area? ..... 6
What are the direct effects and construction impacts? ..... 6
What are the project impacts? ..... 6
What are the effects of the Project Action on highway operations? ..... 7
What are the advantages and disadvantages of No-Build and Project Action? ..... 7
Indirect and Cumulative Effects. ..... 8
Mitigation and Conclusion ..... 8

1. Project Description ..... 1-1
1.1 Report Organization. ..... 1-1
1.2 Description of Project ..... 1-1
1.3 Purpose and Need of Project ..... 1-4
1.4 Report Objectives and Goal ..... 1-4
1.5 Project Alternative (No-Build and Project Action) ..... 1-4
2. Methodology and Transportation Studies ..... 2-1
2.1 Transportation Studies ..... 2-1
2.2 Methodology ..... 2-4
2.2.1 Performance Measures ..... 2-4
2.2.2 Data ..... 2-4
2.2.3 Travel Demand Forecasting ..... 2-4
2.2.4 Traffic operations analysis ..... 2-5
2.2.5 Highway segment analysis ..... 2-5
2.2.6 Intersection Analysis ..... 2-5

## Contents (Continued)

2.2.7 Travel Time Analysis ..... 2-5
2.2.8 Safety ..... 2-5
3. Affected Environment ..... 3-1
3.1 Land Uses ..... 3-1
3.2 Key Transportation Systems in the Study Area ..... 3-1
3.2.1 State and National Highway Classifications ..... 3-3
3.2.2 Freight and Goods Transportation System Classifications ..... 3-3
3.2.3 Transit Operations ..... 3-3
3.2.4 Active Transportation ..... 3-4
3.2.5 Rail Operations ..... 3-4
3.2.6 Emergency services and response ..... 3-4
3.3 Existing Roadway Operative Conditions in Study Area ..... 3-4
3.3.1 Traffic Volumes ..... 3-4
3.3.2 Highway Segment Analyses ..... 3-5
3.3.3 Intersection Operations Analyses ..... 3-9
3.3.4 Travel Times ..... 3-10
3.3.5 Origin Destination Analysis ..... 3-11
3.4 Collision History / Safety Analysis ..... 3-13
3.4.1 Intersection Collisions ..... 3-13
3.4.2 Segment Collisions. ..... 3-15
4. Potential Effects of the Project ..... 4-1
4.1 Direct Effects. ..... 4-1
4.1.1 Construction impacts ..... 4-1
4.1.2 Project impacts ..... 4-1
4.1.3 Intersection Traffic Operations ..... 4-7
4.1.4 Future Highway Traffic Operations ..... 4-13
4.1.5 The No-Build Future ..... 4-13
4.1.6 The Project Alternative Future ..... 4-14
4.2 Indirect and Cumulative Effects ..... 4-14
5. Mitigation and Conclusion ..... 5-1
5.1 What the Required Project Would Achieve ..... 5-1
5.1.1 What Existing and Future Transportation Needs Are Addressed ..... 5-1

## Contents (Continued)

5.2 Any Mitigation to Avoid or Minimize Adverse Effect ..... 5-1
5.2.1 SR 3 Freight Corridor Capacity. ..... 5-1
5.2.2 Existing SR 3 Capacity ..... 5-1
5.2.3 Intersection Control and Capacity ..... 5-2
5.2.4 Local Connections ..... 5-2
5.2.5 Findings and Conclusions ..... 5-2
5.2.6 Conclusions ..... 5-3
6. References ..... 6-1
FIGURES
Figure ES-1. SR 3 Freight Corridor - Freight Corridor Alignment ..... 2
Figure ES-2. SR 3 Freight Corridor - North End Connection at Lake Flora Road ..... 3
Figure ES-3. SR 3 Freight Corridor - South End Connection at SR 302 ..... 3
Figure 1-1. SR 3 Freight Corridor - Freight Corridor Alignment ..... 1-2
Figure 1-2. SR 3 Freight Corridor - North End Connection at Lake Flora Road ..... 1-3
Figure ES-3. SR 3 Freight Corridor - South End Connection at SR 302 ..... 1-3
Figure 3-1. SR 3 Freight Corridor Study Area ..... 3-2
Figure 3-2. 2019 Existing AM Peak Hour Volumes ..... 3-6
Figure 3-3. 2019 Existing PM Peak Hour Volumes ..... 3-7
Figure 3-4. 2019 Existing Midweek Average Daily Traffic. ..... 3-8
Figure 3-5. 2019 Existing Origin/Destination Travel Patterns ..... 3-12
Figure 4-1. 2028 AM Peak Hour No-Build Volumes ..... 4-2
Figure 4-2. 2028 PM Peak Hour No-Build Volumes ..... 4-3
Figure 4-3. 2050 AM Peak Hour No-Build Volumes ..... 4-4
Figure 4-4. 2050 PM Peak Hour No-Build Volumes ..... 4-5
Figure 4-5. Forecasted Peak Hour Travel Patterns ..... 4-6
Figure 4-6. Future Travel Times ..... 4-8
Figure 4-7. North End Connection at Lake Flora Road ..... 4-11
Figure 4-8. South End Connection at SR 302 ..... 4-12

## Contents (Continued)

## TABLES

Table 3-1. Comparison of Seasonal Traffic Volumes on SR 3, South of Lake Flora Road ..... 3-5
Table 3-2. Existing Year (2019) PM Two-Way Two-Lane Highway LOS ..... 3-5
Table 3-3. Level of Service Criteria ..... 3-9
Table 3-4. Existing Year (2019) AM and PM Peak Hour Intersection Operations ..... 3-10
Table 3-5. Existing Travel Time along SR 3 Freight Corridor between Lake Flora Road and SR 302 ..... 3-11
Table 3-6. Historical Crash Rates and Crashes Summarized by Severity and Type for Study Intersections and Segments ..... 3-14
Table 4-1. Change in SR 3 Bi-Directional Volumes - 2050 PM Peak Hour Traffic Forecast ..... 4-7
Table 4-2. 2028 AM and PM Peak Hour Intersection Operations ..... 4-9
Table 4-3. 2050 AM and PM Peak Hour Intersection Operations ..... 4-9
Table 4-4. Future Peak Hour Operations - North end Connection at Lake Flora Road Intersection ..... 4-10
Table 4-5. Future Peak Hour Operations - Southern Endpoint
Table 4-6. Future Conditions PM Peak Hour Highway Operations ..... 4-13

## APPENDICES

A Existing Traffic Counts
B Traffic Operations Modeling Output

## Acronyms and Abbreviations

| ADT | average daily traffic |
| :---: | :---: |
| BAWSI | Belfair Area Widening and Safety Improvements |
| BBTAR | Belfair Bypass Traffic Analysis Report |
| BBTDR | Belfair Bypass Transportation Discipline Report |
| CAC | collision analysis corridor |
| CAL | collision analysis location |
| EA | Environmental Assessment |
| FGTS | Freight Goods Transportation System |
| FHWA | Federal Highway Administration |
| FONSI | Finding of No Significant Impact |
| HCM | Highway Capacity Manual |
| HCS | Highway Capacity Software |
| HSS | Highway of Statewide Significance |
| IAL | intersection analysis locations |
| ICE | Intersection Control Evaluation |
| LOS | level of service |
| MP | milepost |
| MTA | Mason Transit Authority |
| mph | miles per hour |
| NHFN | National Highway Freight Network |
| NHS | National Highway System |
| OD | origin destination |
| PDO | property damage only |
| PSAP | Puget Sound and Pacific Railroad |
| PSIC | Puget Sound Industrial Center |
| PSRC | Puget Sound Regional Council |
| SR | state route |
| UGA | urban growth area |
| v/c | volume to capacity |
| WSDOT | Washington State Department of Transportation |

## Executive Summary

## What is the purpose of this report?

This transportation discipline report addresses the purpose and need of the State Route (SR) 3 Freight Corridor; assesses the potential effects of the project; and identifies possible mitigation measures, if any. This report is intended to be part of the NEPA Environmental Assessment documentation for the project.

## What is the Project Description?

The SR 3 Freight Corridor Project would construct a two-lane limited access highway on a new alignment running approximately north-south to the east of existing SR 3 in Mason County and a small portion in Kitsap County. The proposed Freight Corridor would carry through traffic between Shelton and Bremerton and would serve as the main line for SR 3. The existing SR 3 alignment would become a "Business Loop" serving downtown Belfair, SR 106, and SR 300 (Old Belfair Highway). The proposed design speed of highway would be 50 miles per hour and the posted speed would be 50 miles per hour.

Figure ES-1 displays the location and alignment of the proposed SR Freight Corridor. The proposed corridor would be 6 miles long, branching from the existing SR 3 corridor at milepost (MP) 22.81 and reconnecting at MP 29.49. A roundabout would be constructed at the north end of the alignment to connect the existing SR 3 corridor to the Freight Corridor at Lake Flora Road (see Figure ES-2). Lake Flora Road would be realigned to accommodate the roundabout. Two roundabouts are proposed to connect the south end of the new corridor to the existing SR 3 corridor at SR 302 (see Figure ES-3). At this south connection, the western roundabout would provide access to the existing SR 3 corridor. The eastern roundabout would provide access to SR 302 and the SR 3 Freight Corridor. Between the two roundabouts, right-in-right-out access is proposed to provide access to North Mason High School and Belwood Lane. The dual roundabouts would function as a system to allow traffic to circulate and exit to the desired route. The roadway configuration would consist of two twelve-foot lanes and eightfoot shoulders. The approximate width of the proposed right-of-way is 120 feet.

## What is the purpose and need of the project?

Project Purpose: The purpose of developing a new corridor around the Belfair Urban area is to provide a reliable high speed regional route between Kitsap and Mason Counties. The SR 3 Freight Corridor would also reduce congestion in Belfair and provide an alternate route for emergency vehicles. Implementation of this project would provide safe and reliable access to regional jobs, goods, and services, improve efficiencies for all public service providers, and would improve congestion related safety conditions on SR 3 in Belfair. The proposed SR 3 Freight Corridor Project would provide a solution to the immediate and long-range regional transportation mobility and safety of the SR 3 corridor in northeast Mason and southwest Kitsap counties.

The completed project would provide a two-lane highway on a new alignment with the proposed posted speed of 50 miles per hour that would more reliably move regional traffic between Shelton and Bremerton. The freight corridor would ensure efficient movement of regional freight, commute trips between Kitsap and Mason counties, accommodate seasonal influxes of tourist traffic, and serve general traffic needs through to the design year (2050). It would also serve as an alternate route during occasional highway closures on existing SR 3 in Belfair.

SR 3 Freight Corridor Transportation Discipline Report
Washington State Department of Transportation


Figure ES-1. SR 3 Freight Corridor - Freight Corridor Alignment


Figure ES-2. SR 3 Freight Corridor - North End Connection at Lake Flora Road


Figure ES-3. SR 3 Freight Corridor - South End Connection at SR 302

Project Need: SR 3 is a Highway of Statewide Significance and a National Highway System designated route with 19,000 annual average daily vehicles per day in 2018 in Belfair. The route experiences congestion during peak commute hours, weekends, holidays, and at various times during the tourist season. Considerable delay occurs at intersections located in the Belfair business and retail area.

Traffic projections show that without development of improvements for regional traffic, operational levels of service (LOS) on the portion of SR 3 through Belfair will continue to decline. This conclusion is supported by several studies conducted over the last decade.

A new Freight Corridor around Belfair that serves regional traffic would improve mobility and reduce congestion through Belfair.

## What are the alternatives analyzed?

The alternatives analyzed are the No-Build condition and the Project Action (SR 3 Freight Corridor). The following are the major components of these alternatives:

No-Build - The SR 3 Freight Corridor would not be constructed. This alternative may have some minor improvement during normal maintenance activities of the existing SR 3 highway.

Project Action (SR 3 Freight Corridor) - The SR 3 Freight Corridor Project would construct a two-lane limited access highway on a new alignment to the east of existing State Route 3. The proposed freight corridor would be the main line of SR 3, carrying through traffic between Shelton and Bremerton. The proposed alignment would begin at milepost (MP) 22.81 on SR 3 and connect back at MP 29.49.

## How were the study limits determined?

The study limits for the project were determined during travel demand modeling and alternatives analysis in prior efforts. The model developed for the study incorporated Mason County and Kitsap County models and ensured influence areas of all the alternatives were adequately considered.

## What methodology was used for traffic analysis and identifying transportation facilities within the area?

This report addresses the No-Build and the Project Action alternatives. The approach taken is to leverage information that was already available from previous studies and analyses along with associated models and assumptions, to demonstrate how the Project Action addresses the purpose and need. Data and analyses were updated only where appropriate. This report references the methodology and results from previous studies when applicable.

Travel forecasts were updated to reflect current input from Mason and Kitsap County models and updated network and land use assumptions. This update was done in coordination with Mason County, Kitsap County, and City of Bremerton staff.

Travel forecasts along SR 3 were estimated using a combination of historical growth and peripheral travel demand data from PSRC and SR 16 Travel Demand Models. Forecast traffic conditions were analyzed using forecast data and software such as Highway Capacity Software (HCS)+, Synchro and SIDRA, applying Highway Capacity Manual (HCM) methodologies. Similar to the 2013 Environmental Assessment, the updated EA assumes up to three connections would be provided on the new Freight Corridor. A design year of 2050 and an opening year of 2028 were modeled in the analysis.

Traffic operations analysis was conducted to assess effects of the Project Action relative to the NoBuild condition. HCM methodologies were applied to evaluate arterial and intersection operative conditions for the No-Build and the Project Action. Forecast traffic conditions were analyzed using forecast data and software such HCS, Synchro and SIDRA.

HCS using the HCM 6th Edition methodologies were used to perform highway segment LOS analyses on the existing SR 3 mainline from SR 302 to Lake Flora Road without the SR 3 Freight Corridor (the No-Build Alternative) and with the SR 3 Freight Corridor (the Project Action) for the year 2028 (opening year) and 2050 (design or horizon year). Seven key intersections were analyzed to assess intersection operations without and with the freight corridor, including SR 3 / Lake Flora Road, SR 3 / Log Yard Road, SR 3 / NE Clifton Lane, SR 3 / Old Belfair Highway, SR 3 / SR 106 and SR 3 / SR 302. Intersections were analyzed based on WSDOT's analysis policies and protocols as of the date of this report using two software packages. Synchro 11.0 software was used to analyze the operation of signalized and stop-controlled intersections; SIDRA 7 software was used to analyze roundaboutcontrolled intersections. Focused analyses were performed at the north and south end connections with SR 3 to gain an understanding of the operations with intersection layout options.

Increased safety along the SR 3 corridor in the Belfair area is another purpose of the Project Action. Five years of collision history data from 2018 to 2022 were analyzed. Collision types, occurrences, and collision rates were summarized. The WSDOT Safety Program methodology generates an Intersection Analysis Location List that is reviewed by WSDOT for possible scoping and programming requests. Collision analysis locations (CAL) and collision analysis corridors (CAC) are also identified. Currently, two IALs and one CAL are within the study limits. These analysis locations and associated programmed safety projects in the vicinity were identified.

## What is the affected environment?

## What are the key transportation systems in the study area?

SR 3 provides service between Shelton and Bremerton, connecting with US 101 in Shelton and SR 16 in Bremerton. SR 3 is a Highway of Statewide Significance (HSS) and also part of the National Highway System (NHS). Within the limits of the proposed project, SR 3 is a two-lane rural principal arterial with speed limit of 30 miles per hour (mph), except from milepost 27 to milepost 29 where the speed limit is 50 mph . The average daily traffic (ADT) on the route was 19,000 vehicles in 2018. The route handles a little over 3 million tons of freight per year (T-3 classification). The intersections with SR 106 and NE Clifton Lane are signalized with full signals and the intersection with the Belfair Elementary School Exit has a pedestrian crossing signal. Access control on the route varies from managed access to limited access control. Within the project study area, SR 3 connects with SR 106, SR 302, and Old Belfair Highway in Belfair, all of which are non-HSS facilities. The remainder of the public roadway network consists of county roads.

Mason Transportation Authority provides scheduled bus service five to six days a week between Belfair, Bremerton, and Shelton. Local service is provided in Belfair, between downtown Belfair to North Mason High School on SR 3, and Belfair State Park on Old Belfair Highway. Two park-and-ride lots are available in Belfair.

Active transportation facilities are limited in Belfair and along SR 3 in the study area. Within the Belfair urban center, sidewalks and non-signed bicycle lanes exist on both sides of SR 3. Clearly marked pedestrian crosswalks are present at major intersections within Belfair and there is signalized pedestrian crossing on SR 3 at the elementary school. Outside the urban center, paved shoulders are present on SR 3, ranging in width from 5 feet to 12 feet.

The Puget Sound and Pacific Railroad (PSAP) operates a freight rail line that runs through the study area. The rail line is grade separated from SR 3 where it crosses the highway on the north and south sides of Belfair.

## What is the existing roadway operative condition in the study area?

Highway LOS analysis shows the one-mile segment of the SR 3 mainline segment north of Lake Flora Road (MP 28.78 to MP 29.78) is LOS D. The signalized intersection at NE Clifton Lane operates at LOS D and E during the AM and PM peak periods, respectively, failing to meet LOS standards. The unsignalized intersection at Old Belfair Highway is operating at failing conditions of LOS E and F during the AM and PM peak periods, respectively.

Crash records collected in the study area between January 1, 2019 and December 31, 2022 indicate that the type and severity of crashes appears to be consistent with congested urban conditions. Rear-end and property damage only (PDO) or non-injury crashes account for the greatest number of crashes. The number of crashes tends to increase under congested conditions, but the severity of those crashes is generally lower, due to lower speeds. At the study area intersections, between January 2018 and December 2022, one serious injury crash occurred. There were no fatal crashes. The intersections of SR 3/NE Clifton Lane and SR 3/Lake Flora Road had the highest crash rates in the study area, ranging from 3.0 crashes per year to 5.0 crashes per year. On SR 3 segments, between the study intersections, 330 crashes were reported, with the majority occurring between Lake Flora Road to NE Clifton Lane (42 percent) and between NE Clifton Lane to SR 106 (40 percent).

## What are the direct effects and construction impacts?

Under a No-Build alternative, direct effects such as construction impacts and temporary traffic disruption would not occur. Noise, air quality, water quality, and other construction related direct effects would likewise be absent. However, travelers would continue to experience congestion and delay during peak periods. Access to and from business and other services would continue to be difficult as gaps between vehicle platoons progressing through the corridor become nonexistent.

Direct effects of the Project Action would entail temporary construction effects. Travelers would experience construction related traffic delay and might need to take detour routes for a period of time. Since the majority of the Freight Corridor alignment is through forested land, a major portion of the work would not lead to direct disruption to traffic. There would be an increase in traffic as construction workers go to work sites or bring in and remove equipment and materials. There may be temporary air quality, water quality, and noise effects due to construction, but on-site mitigation measures and standard procedures should offset the effects and render the effects not significant. Direct benefits of building the Freight Corridor would include the creation of construction jobs and increased network capacity at its completion.

## What are the project impacts?

Travel demand modeling and traffic operations analysis results provide the basis for evaluating the long-term and cumulative effects of the Project Action relative to the No-Build condition. The most straightforward measure of the project's value is its potential to affect a reduction in traffic volumes on SR 3. Model data indicates the SR 3 Freight Corridor may be able to reduce 2050 PM peak hour intersection approach volumes in the Belfair commercial area, by as much as 43 percent relative to No-Build conditions. This confirms there are no significant traffic impacts as a result of the project.

As capacity is added to the Belfair network with the SR 3 Freight Corridor, vehicle trips are redistributed across a greater number of trip path choices, resulting in a generalized reduction in congestion and improvement in travel time and average operating speed. This again demonstrates that building the Freight Corridor has no significant long term cumulative impact on traffic operations through Belfair but rather reduces congestion and delay, increases safety potential, and improves travel times particularly for regional traffic.

## What are the effects of the Project Action on highway operations?

Highway LOS analysis shows SR 3 operates at LOS D under 2019 existing conditions. Analysis shows that SR 3 would experience increased congestion under No-Build conditions. LOS would continue to decline along the corridor, reaching LOS E by 2050 and the volume to capacity (v/c) ratio would increase. With development of the project, LOS and the v/c ratio along the corridor in 2050would be comparable to existing 2019 conditions, demonstrating the Project Action has no significant adverse effect on SR 3 highway operations.

The Project Action would also improve intersection performance. Under the No-Build condition, the intersections at NE Clifton Lane and Old Belfair Highway are forecast to reach LOS F in the AM and PM peaks by 2050. The intersection at SR 106 is also forecast to operate at LOS F during the PM peak by 2050. The Project Action would improve operations and decrease delay at all intersections in the study area. The reduction in intersection approach volumes and delay at the intersection result in improved intersection operations, therefore, there is no significant impact at intersections due to Project Action.

## What are the advantages and disadvantages of No-Build and Project Action?

No-Build: The No-Build alternative would result in additional congestion, increased duration of delay, longer travel times, exacerbation of safety issues, and potential impacts to air quality precipitated by idling engines in very long queues at signalized and minor street unsignalized intersections. Access to and from business and other services would become difficult as gaps between vehicle platoons progressing through the corridor become nonexistent.

Project Action: Construction of the SR 3 Freight Corridor would provide an alternative route around the Belfair community, mitigating aesthetic, noise pollution, air quality, commercial and retail activities, and separating local ingress and egress access issues from regional throughput. The project offers the best prospects for improving travel times through the corridor for pass-through traffic, presuming access is limited. Construction of the Freight Corridor would lessen traffic volumes through Belfair, which could have both positive and negative consequences for commercial and retail businesses along SR 3.

The project would result in diversion of regional through traffic to the SR 3 Freight Corridor. With reduced traffic volumes, SR 3 through Belfair would experience less congestion, less delay and improved travel times. Lower volumes would lessen exposure and is likely to ease congestion related rear-end collisions. With lower volumes, left turning movement would find more gaps to turn safely.

The Freight Corridor would be designed to include accommodations for the bicyclist and pedestrians that will meet WSDOT's Complete Streets guidelines for limited access facilities.

The project would provide an alternate route during emergencies and for emergency services. Regional response time would likely improve.

The project is expected to have beneficial impacts to transit operations. Reduced congestion and delay would allow for efficient transit operations and the Freight Corridor would provide alternate faster regional transit routes.

## Indirect and Cumulative Effects

Improved travel times would allow for growth in activities and associated travel connected to businesses, commercial enterprises, and residences served by SR 3 outside of Belfair that are particularly dependent on regional traffic. However, both Mason and Kitsap counties come under the state's Growth Management Act and have comprehensive planning in place to address the magnitude, form, and process associated with such land use changes.

Since no direct or indirect increase in total traffic in the study area is predicted as a result of the Project Action, the cumulative traffic impacts are assumed to be negligible.

## Mitigation and Conclusion

The SR 3 Freight Corridor would offer a good level of service for regional traffic using SR 3 in the study area. The Project Action would address existing and forecast travel delay for those using SR 3 between Kitsap County and Mason County. The results of this analysis support the conclusion that there would be beneficial transportation impacts due to the Project Action.

## 1. Project Description

### 1.1 Report Organization

This report is organized as follows:

- Chapter 1 provides description of the project, states its purpose and need, outlines objectives and the goal of this report, and discusses project alternatives (No-Build and Project Action)
- Chapter 2 documents methodology and transportation studies that have been performed for the Project Action
- Chapter 3 discusses the affected environment in terms of key roadway operative conditions, collision history, and current and future projects in the area
- Chapter 4 addresses the potential effects of the Project Action, including direct effects and the indirect and cumulative effects
- Chapter 5 provides concluding discussions, including what the required project would achieve and describes any mitigation to avoid or minimize adverse effects
- Chapter 6 provides a list of references


### 1.2 Description of Project

The State Route (SR 3) Freight Corridor would provide an alternative route to SR 3 and allow users to bypass the urban area of Belfair in Mason County and Kitsap County (see Figure 1-1). This new corridor would be a two-lane, limited-access highway, east of the existing SR 3 corridor, and would act as the mainline for through traffic.

The SR 3 Freight Corridor would run north and south, with a proposed design speed of 50 miles per hour (mph) and a posted speed of 50 mph . The existing SR 3 route would be converted to a "Business Loop," which would provide access to Belfair, SR 106, SR 300 and Old Belfair Highway. The roadway configuration would consist of two twelve-foot lanes and eight-foot shoulders. The approximate width of the existing right-of-way is 120 feet.

The proposed 6-mile corridor would branch from the existing SR 3 corridor at milepost (MP) 22.81 and reconnect at MP 29.49. A roundabout is proposed at the north end of the alignment to connect the existing SR 3 corridor to the Freight Corridor at Lake Flora Road (see Figure 1-2). Lake Flora Road would be realigned to accommodate the roundabout. Two roundabouts are proposed to connect the south end of the new corridor to the existing SR 3 corridor at SR 302 (see Figure 1-3). At this south connection, the western roundabout would provide access to the existing SR 3 corridor. The eastern roundabout would provide access to SR 302 and the proposed SR 3 Freight Corridor. Between the two roundabouts, right-in-right-out access is proposed to provide access to North Mason High School and Belwood Lane. The dual roundabouts would function as a system to allow traffic to circulate and exit to the desired route.


QMapbax, © OpenStreetMap

Figure 1-1. SR 3 Freight Corridor - Freight Corridor Alignment


Figure 1-2. SR 3 Freight Corridor - North End Connection at Lake Flora Road


Figure ES-3. SR 3 Freight Corridor - South End Connection at SR 302

### 1.3 Purpose and Need of Project

The purpose of the SR 3 Freight Corridor project is to provide a reliable high speed regional route that will improve congestion and safety between Kitsap and Mason Counties. The proposed corridor would reduce congestion in the urban Belfair area by providing an alternative route around the downtown area and also provide access to regional jobs, goods, and services. With less congestion in Belfair, the efficiency and safety of the transportation system would improve. Emergency vehicles would experience fewer delays from congestion and gain better access to the region.

The proposed SR 3 Freight Corridor would provide an efficient and reliable route for regional traffic between Shelton and Bremerton through the year 2050. The SR 3 Freight Corridor would relieve the existing SR 3 route, improving efficiency through the region and accommodating regular commercial and seasonal tourist traffic. This project would also serve as an alternative route to the existing SR 3 during any highway closures in Belfair.

### 1.4 Report Objectives and Goal

This transportation discipline report is part of that overall work and will be used for preparing a NEPA Environmental Assessment. Objectives of this report are to:

- Address the purpose and need of the Project Action
- Assess the potential effects of the project
- Identify possible mitigation measures


### 1.5 Project Alternative (No-Build and Project Action)

Two alternatives were analyzed for this report - the No-Build and the Project Action (SR 3 Freight Corridor).

No-Build - In the No-Build alternative, the SR 3 Freight Corridor would not be constructed. It is assumed that normal maintenance activities or planned projects would continue, which may improve some conditions, but they are expected to be relatively minor.

Project Action (SR 3 Freight Corridor) - The Build Scenario assumes construction of a two-lane, limited access highway on a new alignment east of the existing SR 3 highway. Roundabouts would provide connections at both the north and south end of the alignment, where the new corridor ties back into the existing SR 3 corridor. SR 3 Freight Corridor assumptions include:

- A two-lane limited access roadway
- 50 mph design speed on the corridor
- 50 mph posted speed limit on the corridor
- A roundabout at the north end of the alignment to connect the existing SR 3 corridor to the new corridor at Lake Flora Road
- Two roundabouts to connect the south end of the new corridor to the existing SR 3 corridor at SR 302
$\rightarrow$ The western roundabout would provide access to the existing SR 3 corridor
$\rightarrow$ The eastern roundabout would provide access to SR 302 and the proposed SR 3 Freight Corridor
- Right-in-right-out access to provide access to North Mason High School and Belwood Lane


## 2. Methodology and Transportation Studies

The intent of this section of the report is to describe contribution of past transportation studies on development of the SR 3 Freight Corridor concept. This section summarizes the methodology, assumptions, and findings that led to the SR 3 Freight Corridor alternative. At its inception, the SR 3 Freight Corridor project was known as the Belfair Bypass project. The project name was changed in 2019.

### 2.1 Transportation Studies

## Belfair Bypass Analysis - 1997

The WSDOT Reconnaissance Study (1966) identified a new roadway alignment in northeast Mason County to improve mobility through capacity improvement. In 1997, WSDOT completed the Belfair Bypass Analysis, which concluded that the concept of providing a SR 3 bypass around the community of Belfair appeared to be a viable means of improving mobility in the corridor.

## Mason County Belfair Bypass Environmental Assessment - 2001

In 2001, the Mason County Belfair Bypass Environmental Assessment (EA) for a refined bypass alignment was completed. The Bypass was proposed as an undivided two-lane principal arterial with a design speed of 60 mph and a posted speed of 55 mph . The EA was signed by the Federal Highway Administration (FHWA) in November 2001. However, a Finding of No Significant Impact (FONSI) was not issued for the EA.

## Belfair Bypass Traffic Forecast and Analysis - 2006

In 2006, The Transpo Group performed Belfair Bypass Traffic Forecast and Analysis traffic study. This study developed a travel demand forecasting model, produced traffic forecasts, evaluated future traffic operations, and documented impact of the bypass on traffic operations. One of the outcomes from this effort included assessment of the number of lanes needed and when. It noted a four-lane bypass would attract few additional trips and be underutilized in 2030.

## Preferred Connection Alternative Selection, SR 3 Belfair Bypass - 2007

WSDOT conducted a Preferred Connection Alternative Selection, SR 3 Belfair Bypass in 2007. It analyzed various alternatives for how the proposed bypass would connect with existing SR 3. A criteriabased methodology was used to evaluate options for the north and south connections. Operational functionality, safety, cost, public approval, property impacts, and environmental and permitting factors were evaluated. Alternatives were scored in terms of their impacts relative to these criteria.

## Belfair Bypass Traffic Analysis Report - 2008

In 2008, The Transpo Group developed a 2035 travel demand model used for the Belfair Bypass Traffic Analysis Report (BBTAR). Alternatives analyzed were baseline conditions (no Belfair Bypass) and Belfair Bypass assuming the preferred connections. For the north connection, it was assumed the junction would result in a dead-end segment, to be used as an access road to existing properties only. The report concluded that the bypass is needed by 2035. However, in 2035 a two-lane bypass would operate at capacity for southbound traffic.

An analysis of intersection operations relative to a 2035 two-lane bypass with Newkirk Road connection was provided. In addition, two layouts of the north junction of the bypass with Lake Flora Road and existing SR 3 were studied and compared. The study concluded that, with construction of the retained bypass alternative, several intersection improvements were still needed, including signalization of currently two-way-stop-control locations, and channelization.

The BBTAR report examined transportation improvement alternatives for the Belfair Bypass. Based on a comparison of the modeling results, a 2035 Belfair two-lane bypass with Newkirk Road connection was selected for further study. The BBTAR provides 2035 traffic operations relative to 2035 Belfair two-lane bypass with Newkirk Road connection. It also evaluated two North End options for connecting existing SR 3 to the Belfair Bypass. North End Option 1 consisted of creating a deadend segment that would serve adjacent property owners only. North End Option 2 consisted of providing a southbound only connection from the Belfair Bypass to SR 3 .

## SR3 Belfair Area Widening and Safety Improvements (BAWSI), Traffic Analysis Report - 2008

Completed in 2008, the SR3 Belfair Area Widening and Safety Improvements (BAWSI) Traffic Analysis Report provided an analysis specific to the capacity and safety improvements to SR 3 in the Belfair area. An option resulting in a dead-end segment was assumed for the north end connection of the Bypass to SR 3. The report predicted intersection level of service (LOS) for three scenarios: no improvements, improvements currently identified as part of the BAWSI project, and additional improvements needed to maintain LOS D or better at SR 3 intersections. The report concluded traffic operations on SR 3 would be improved, assuming the Belfair Bypass with a connection at Newkirk Road was constructed, and that the BAWSI project improvements are implemented.

## Belfair Bypass Transportation Discipline Report - 2009

In June 2009, WSDOT Eastern Region completed a draft Belfair Bypass Transportation Discipline Report. It considered a 2035 Belfair two-lane bypass without the Newkirk road connection.

## Summary Report - SR 3, Belfair Bypass - 2009

The 2005 Transportation Partnership Account legislation included funding for work on the preconstruction phase of the SR 3, Belfair Bypass - New Alignment project. The purpose of the project was to address congestion on SR 3 by construction of a new alignment around Belfair. The 20092011 Transportation Budget contained no funding for the Bypass project from July 2009 through 2018. As a result, WSDOT work was curtailed in June 2009. In June 2009, WSDOT documented the development work on this project by preparing a Summary Report - SR 3, Belfair Bypass. The purpose was to provide a consolidated document that described the work conducted between 2006 and 2009, document what had been learned, and for use when work was re-started on the project.

## SR 3 Belfair Bypass Proviso, Alternatives Outreach Report - 2010

In the 2009 State Transportation Budget, the Legislature included a proviso directing WSDOT to conduct a public outreach process to be used in reconsidering the scope and budget of the Belfair Bypass project. In June 2010, WSDOT submitted the SR 3 Belfair Bypass Proviso, Alternatives Outreach Report to the legislature. The four most promising alternatives examined by an Expert Panel were forwarded to WSDOT staff for further consideration.

## Bremerton Economic Development Study (BEDS) - 2012

The Bremerton Economic Development Study (BEDS), published in 2012, did not reanalyze the Belfair Bypass but did adopt the findings from previous studies regarding this project. It identified the Belfair Bypass as one of the top priority projects for the stakeholders and the Belfair community. The study called for the construction of an "alternate two-lane divided highway around Belfair with full limited access control."

## Belfair Bypass Environmental Assessment - 2011

In the 2010 supplemental budget, the Washington State Legislature provided \$750,000 to continue work on the Belfair Bypass EA. The EA analyzed a No-Build alternative as well as a project alternative that would construct a two-lane limited access highway on a new alignment running approximately north-south to the east of SR 3 in Mason County and a small portion in Kitsap County. The project alternative included a north end connection to SR 3 at Lake Flora Road and a south connection just south of the intersection with SR 302.

## SR 3 Belfair Bypass Transportation Discipline Report - 2011

Conducted by WSDOT, this report analyzes and summarizes the need for the Belfair Bypass. It describes the need for a new alignment to relieve congestion on the SR 3 corridor and in the Belfair urban area. Using a design year of 2035, the analysis in this study showed conditions on the SR 3 corridor are expected to continue to deteriorate without the project.

## SR 3 - Belfair Bypass Revised Environmental Assessment - 2013

Conducted by WSDOT, this assessment analyzed the environmental impacts of the construction of the Belfair Bypass. The results of the assessment showed wetland, wildlife, land use, property, public services, utilities, visual quality, and geology and soils would all experience potential impacts under the Build Scenario of this project. Mitigation measures were proposed to offset some of these impacts.

## SR 3 Freight Corridor Study Existing Conditions Summary Technical Memorandum - 2019

Prepared by Parametrix on behalf of WSDOT, this technical memorandum detailed the existing conditions of SR 3. The study area for the analysis covered approximately 6.7 miles from MP 22.81 (south of SR 302) to MP 29.49 (north of Lake Flora Road). The study used 2019 traffic data to update the traffic analysis that was prepared for the 2013 SR 3 Belfair Bypass Environmental Assessment. Existing level of service (LOS), travel time, safety, and origin destination (OD) data were analyzed and reviewed for the corridor.

## SR 3 Freight Corridor Study Future Conditions Summary Technical Memorandum - 2020

Prepared by Parametrix on behalf of WSDOT, this technical memorandum detailed the evaluation of intersection control alternatives for the proposed north and south end connections for the SR 3 Freight Corridor (previously known as the Belfair Bypass) in both opening year (2028) and horizon year (2050) conditions. Analysis results showed that a single-lane roundabout at the south end connection would operate acceptably for both future year scenarios. The north end connection may require a multi-lane roundabout because Kitsap County is projected to grow due to the Puget Sound Industrial Center (PSIC) and increased population in the Belfair Urban Growth Area (UGA). This project would construct a single-lane roundabout at the north end of the connection. If future growth triggers the need for a multi-lane roundabout, the developer or proponent for the new development would be responsible for improvements to the roundabout, as required under Mason County Concurrency ordinances and the Growth Management Act. The mainline is expected to meet WSDOT LOS standards for a two-lane highway.

## SR 3 Freight Corridor Study Transportation Analysis Methodology Memorandum - 2020

Prepared by Parametrix, this methodology memorandum identified the analysis needed to update the transportation analysis prepared in December 2011 for the SR 3 - Belfair Bypass Project Environmental Assessment (2013) to support current design analysis and obtain design approvals. Updates to the methodology described in this memorandum include performance measures, data, travel demand forecasting, traffic operations analysis, highway segment analysis, intersection analysis, travel time analysis, and safety.

### 2.2 Methodology

The latest description of the Project Action and the purpose and need statement provides the basis for this Transportation Discipline Report for the SR 3 Freight Corridor project. A review of prior transportation studies was undertaken and incorporated as part of the project analysis. This report addresses the No-Build and the Project Action alternatives. The description of the Project Action includes construction of a two-lane, limited access highway on a new alignment east of the existing SR 3 highway with roundabouts at both the north and south end of the alignment where the Freight Corridor ties back into the existing SR 3 corridor.
The focus of the Project Action is to improve regional mobility in the Belfair urban area with a reliable high speed regional route between Kitsap and Mason Counties.

The approach taken in this report was to use information that was already available from previous studies and analyses, using these models and assumptions to demonstrate how the Project Action addresses the purpose and need. The Project Action would reduce congestion through Belfair by providing an alternative route around Belfair for regional through traffic, thereby reducing delay and improving travel times.

### 2.2.1 Performance $\operatorname{Measures}$

The study team selected multiple performance measures to assess how regional mobility may be improved and congestion may be reduced through the Project Action alternative relative to the NoBuild alternative. These measures include traffic volume reduction through diversion to the Freight Corridor, travel times, intersection delay, operating speeds, and LOS. For purposes of analysis, the corridor in Belfair was considered urban, as it exhibits urban characteristics, particularly in the Belfair commercial core. The performance measures were analyzed for the years 2019, 2028 and 2050.

### 2.2.2 Data

Traffic data collected in May of 2019 as part of the planning-level analysis for the SR 3 Freight Corridor project were used for this analysis. In addition to the updated traffic data, WSDOT GIS Workbench data layers, county, transit, and other agency plans and programs were used to identify non-roadway transportation systems.

Traffic data collected by WSDOT at the permanent traffic counter on SR 3, south of Lake Flora Road (R089S) was evaluated to determine potential growth between 2023 and 2019. While the data indicates a significant decrease in traffic volumes during the COVID pandemic in 2020, there has been a rebound, and current volumes are now roughly equivalent to those recorded in 2019. Consequently, the 2019 count data remains suitable for representing Existing Conditions.

### 2.2.3 Travel Demand Forecasting

Travel forecasts were updated to reflect current input ${ }^{1}$ from Mason and Kitsap County models and updated network and land use assumptions. This update was done in coordination with Mason County, Kitsap County, and City of Bremerton staff. Travel forecasts along SR 3 were estimated using a combination of historical growth and peripheral travel demand data from PSRC and SR 16 Travel Demand Models. Similar to the 2013 Environmental Assessment, the updated EA assumes up to three connections would be provided on the new Freight Corridor, including connections at Log Yard Road, Romance Hill Road, and Alta Drive.

[^0]A design year of 2050 ² and an opening year of 2028 were modeled in the analysis.

### 2.2.4 Traffic operations analysis

The objective of the traffic operations analysis was to determine whether the proposed Freight Corridor would improve regional mobility by providing an alternative route around Belfair and to identify any significant project impacts. Another objective was to determine whether congestion through Belfair would be reduced, as lower traffic volumes can decrease congestion and delay and improve travel times.

### 2.2.5 Highway segment analysis

HCS using the HCM 6th Edition methodologies were used to perform highway segment LOS analyses on the existing SR 3 mainline from SR 302 to Lake Flora Road without the SR 3 Freight Corridor (the No-Build Alternative) and with the SR 3 Freight Corridor (the Project Alternative) for the year 2028 (opening year) and 2050 (design or horizon year).

### 2.2.6 Intersection Analysis

Intersections were analyzed based on WSDOT's analysis policies and protocols as of July 2020 using two software packages. Synchro 10.0 software was used to analyze the operation of signalized and stop-controlled intersections and SIDRA 7 software was used to analyze roundabout-controlled intersections.

### 2.2.7 Travel Time Analysis

Future travel times on the SR 3 corridor and along the proposed Freight Corridor was calculated using a combination of existing travel times observed during field visits, Google Maps, and changes to intersection delays in the Synchro and SIDRA models. SimTraffic software was not used during the travel time analysis for existing or future conditions.

### 2.2.8 Safety

A basic safety level analysis, following WSDOT guidelines and direction, was conducted for this study. This type of safety analysis presents only factual conclusions about current conditions. A more detailed quantitative measure of how well the Freight Corridor addresses safety along the corridor using an intermediate or advanced safety level analysis was not performed as part of this work. Crash data between January 1, 2018, and December 31, 2022, was evaluated. Data from the safety study was reviewed and used in a qualitative assessment of potential safety improvements that the Freight Corridor could include. The change in intersection control at the termini intersections alters the existing safety conditions at these intersections as documented in Intersection Control Evaluation (ICE) reports prepared for each.

[^1]
## 3. Affected Environment

### 3.1 Land Uses

Existing land use within the study area is a mix of rural, commercial, and residential. The proposed roadway would pass through the Belfair UGA and the City of Bremerton. Within Belfair's commercial core, the land use comprises mixed use (integrated retail, commercial and industrial uses), general commercial, education, and residential. Most of the residential use consists of single-family dwelling units. Outside of the Belfair UGA, land use is primarily rural and mostly undeveloped forested land.

The 2003 Belfair Urban Growth Area Plan determined that most of Belfair's future growth potential is on the plateau north and east of the existing SR 3, along the new SR 3 alignment. Zoning has been adopted in the UGA to support this anticipated growth, including residential and mixed-use zoning.

### 3.2 Key Transportation Systems in the Study Area

SR 3 connects Mason and Kitsap counties along the Kitsap Peninsula, connecting with US 101 in Shelton and SR 16 in Bremerton. This study evaluates the existing SR 3 corridor between Lake Flora Road in the north (MP 29.49) to SR 302 (MP 22.81) in the south. Within the study area, SR 3 connects with SR 106, SR 302, and (SR 300) Old Belfair Highway in Belfair.

SR 3 is a two-lane road between Belfair Elementary School (MP 25.42) and NE Ridgepoint Boulevard (MP 26.86), with a two-way left turn lane through Belfair. Turn lanes were present in the vicinity near Log Yard Road when existing data were collected. A single lane roundabout was constructed in late spring 2020 at the intersection of SR 3 and Log Yard Road. SR 3 has a truck climbing lane beginning at MP 26.93 (approximately 400 feet north of NE Ridgepoint Boulevard) and ending at MP 27.66.

SR 3 within the study area has posted speed limits ranging from 30 mph in Belfair to 50 mph outside of the Belfair commercial area. Existing counts recorded 85th percentile speeds which represents the speed that 85 percent of vehicles travel at or below. On SR 3 north of Lake Flora Road, it was roughly 60 mph and south of SR 302 it was roughly 50 mph . The spot speed studies show the posted speed limit corresponds with the 85th percentile speed near SR 302, however, 85th percentile travel speeds near Lake Flora Road exceed the posted travel speed by almost 10 mph .

Three intersections on the route are currently signalized - SR 3 at SR 106, SR 3 at NE Clifton Lane, and an exit at Belfair Elementary School which is active only during school release. There are numerous commercial and retail accesses located along the route, as well as two-way stop and oneway stop controlled intersections. Due to heavy northbound and southbound traffic flows on SR 3, especially during the AM and PM peak periods, motorist delay at these locations can be significant. Access control on the route varies from managed access to limited access control.

There are two existing SR 3 under-crossings within the study limits, both crossing USG railroad bridges. Bridge number 003-021 begins at MP 27.38 and bridge number 003/017 begins at MP 23.81.

The study area is shown in Figure 3-1.


[^2]Figure 3-1. SR 3 Freight Corridor Study Area

### 3.2.1 State and National Highway Classifications

WSDOT classifies SR 3 within the study area as a Rural Other Principal Arterial. This section of SR 3 is designated as a critical rural freight corridor and is part of the National Highway Freight Network (NHFN). SR 3 is also identified as an NHS route and as a Highway of Statewide Significance (HSS). The NHS was established by the U.S. Congress and implemented by FHWA as a way of focusing resources on the nation's most important highways. The NHS includes the Interstate Highway System, as well as other roads important to the nation's economy, defense, and mobility. HSS facilities include interstate highways and other principal arterials that are needed to connect major communities in the state. The designation assists with the allocation and direction of funding.

SR 3 within the study area is not designated as one of Washington's Scenic and Recreational Highways. However, SR 3 is often used to access the Pacific Coast Scenic Byway, either at the northern terminus at Hood Canal or at the southern terminus at US 101. US 101 and SR 16 are HSS facilities and SR 106, Old Belfair Highway, and SR 302 are non-HSS facilities.

### 3.2.2 Freight and Goods Transportation System Classifications

WSDOT classifies all highways, county roads, and city streets by reported annual gross truck tonnage, ranging from $\mathrm{T}-1$, the highest tonnage, to $\mathrm{T}-5$, the least tonnage. SR 3 in the study area (MP 23.26 to MP 28.78) handles a little over 3 million tons of freight per year and is classified as a T-3 facility in the Statewide Freight and Goods Transportation System (FGTS) with an existing daily truck percentage of 6 percent.
The Puget Sound and Pacific Railroad (PSAP) operates a freight rail line that runs through the study area. Headquartered in Elma, WA, the PSAP operates 131 miles of track between Chehalis in the south, Hoquiam to the west, and Bangor Naval Base to the north. Major commodities shipped on the line are lumber, logs, and chemicals for pulp and paper mills. PSAP also provides service to the U.S. Navy at Bremerton.

### 3.2.3 Transit Operations

Mason Transit Authority (MTA) operates transit service in Mason County, providing connections to the surrounding communities and important commuter destinations. Four routes serve Belfair:

- Route 1: Service between Shelton and Belfair via SR 3
- Route 3: Service between Belfair and Bremerton via SR 3 through Gorst with local service on Old Belfair Highway
- Route 4: Service within Belfair via a loop route connection to local destinations
- Route 23: Express service between Belfair and Bremerton via SR 3 with limited daily trips MTA provides scheduled service five to six days a week. Bus stops are present along each route, however, riders can also flag a bus down anywhere along the route provided they pick a safe location where the bus can pull completely off the road.
In addition to fixed route service, MTA operates dial-a-ride services, paratransit, worker/driver buses, and vanpool programs. More than half of the vanpools connect communities in Mason County to the Naval Station in Bremerton, while others serve Bangor, Keyport, and Seattle.

MTA maintains two park-and-ride lots in the Belfair area, one at the Belfair Assembly of God parking lot and one on Roy Road behind the Safeway. Mason County recently constructed a new park-and ride lot just east of the existing SR 3/Log Yard Road intersection. The new park-and-ride was opened in May 2023.

Although a portion of the project study area near Lake Flora Road is in Kitsap County, Kitsap Transit service does not provide fixed route service in the study area.

Transit travel within Mason County is free. When traveling outside Mason County to Bremerton there is a $\$ 1.50$ one-way charge for youths and adults and a $\$ 0.50$ charge for seniors and persons with disabilities.

### 3.2.4 Active Transportation

Within the Belfair urban center, sidewalks and non-signed bicycle lanes exist on both sides of SR 3. Clearly marked pedestrian crosswalks are present at major intersections within Belfair and there is a signalized pedestrian crossing on SR 3 at Belfair Elementary School. Outside the urban center, paved shoulders are present on SR 3, ranging in width from 5 feet to 12 feet. Mason County does not have long-distance trails near the SR 3 study corridor that serve nonmotorized users and commuters. The Theler Wildlife Refuge, however, is a popular county trail with access off SR 3 near Belfair Elementary School.

### 3.2.5 Rail Operations

The PSAP operates a freight rail line that runs through the study area. The rail line is grade separated from SR 3 where it crosses the highway on the north and south sides of Belfair. There is no passenger service provided on this rail line. The PSAP is headquartered in Elma, Washington and operates 131 miles of track extending to Chehalis in the south, Hoquiam to the west, and Bangor Naval Base to the north. The PSAP interchanges with the Burlington Northern Santa Fe and Union Pacific Class I carriers in Centralia. Major commodities shipped on the line are lumber, logs, and chemicals for pulp and paper mills. The PSAP provides service to the US Navy at Bremerton.

### 3.2.6 Emergency services and response

Congestion on SR 3 results in delays in emergency response. A common consequence of emergency vehicle response through a highway corridor such as Belfair is disruption of normal traffic flows and operation of the highway and arterials.

### 3.3 Existing Roadway Operative Conditions in Study Area

### 3.3.1 Traffic Volumes

Traffic volumes along SR 3 fluctuate with the seasons due to the high tourist and recreational use along the highway on weekends, holidays, and during the summer months. Table 3-1 illustrates the seasonal variations in traffic volumes on SR 3 south of Lake Flora Road at MP 28.68. Traffic volumes were slightly higher on the average Friday than during mid-week in 2019. Summer weekends in June, July, and August experienced higher traffic volumes than average weekends throughout the year, as do holiday weekends, such as Memorial Day and Labor Day. Figures 3-2 and 3-3 summarize 2019 AM and PM peak hour traffic volumes along SR 3. Figure 3-4 summarizes midweek ADT volumes in the study area.

Table 3-1. Comparison of Seasonal Traffic Volumes on SR 3, South of Lake Flora Road

| Time Period | 2018 Average Daily Traffica |
| :--- | :---: |
| Average Midweek (Tuesday-Thursday) | 19,000 |
| Average Friday | 20,300 |
| Average Weekend | 16,500 |
| Average Non-Holiday Summer Weekend | 19,400 |
| Average Summer Holiday Weekend <br> (Memorial Day and Labor Day) | 18,900 |

a 2018 counts taken at WSDOT permanent traffic recorder (PTR) at MP 28.68

### 3.3.2 Highway Segment Analyses

LOS standards for HSS facilities, such as SR 3, are established by WSDOT. The standard is LOS C for rural areas and LOS D for urban areas. For the purposes of this report, the corridor along the section of highway in the Belfair vicinity was considered urban as it displays urban characteristics, particularly at the Belfair commercial core.

Consistent with the previous EA published in 2013, a mainline LOS analysis for the entire SR 3 Freight Corridor was performed. The software program HCS 7 was used to evaluate LOS for the existing one-mile highway segment north of Lake Flora Road. Table 3-2 shows the highway operations for the existing section of SR 3. The level of service for Class I highways is determined by average travel speed (ATS) and percent time spent following (PTSF). The worse of the ATS or PTSF is used to determine the prevailing LOS.

Table 3-2. Existing Year (2019) PM Two-Way Two-Lane Highway LOS

| State Route 3 Mainline Segment | Percent Time Spent Following <br> (PTSF)a | Average Travel <br> Speed (ATS) | Level of Service |
| :---: | :---: | :---: | :---: |
| MP 28.78 (Lake Flora Road) to MP 29.78 | $77 \%$ | 47 mph | LOS D |

[^3]

OMapbox, O OpenStreetMap

Figure 3-2. 2019 Existing AM Peak Hour Volumes


[^4]Figure 3-3. 2019 Existing PM Peak Hour Volumes

© Mapbox, O OpenStreetMap
Figure 3-4. 2019 Existing Midweek Average Daily Traffic

### 3.3.3 Intersection Operations Analyses

Traffic operations were measured using the LOS method, which is defined in terms of delay on a scale ranging from A to F, depending on the delay conditions at the intersection. Signalized intersection level of service (LOS) is defined in terms of a weighted average control delay for the entire intersection. Control delay quantifies the increase in travel time that a vehicle experiences due to the traffic signal control as well as provides a surrogate measure for driver discomfort and fuel consumption. Signalized intersection LOS is stated in terms of average control delay per vehicle (in seconds) during a specified time period (e.g., weekday PM peak hour). Control delay is a complex measure based on many variables, including signal phasing and coordination (i.e., progression of movements through the intersection and along the corridor), signal cycle length, and traffic volumes with respect to intersection capacity and resulting queues.

Unsignalized intersection LOS criteria can be further reduced into two intersection types: all-way stop and two-way stop control. All-way stop control intersection LOS is expressed in terms of the weighted average control delay of the overall intersection or by approach. Two-way stop-controlled intersection LOS is defined in terms of the average control delay for each minor-street movement (or shared movement) as well as major-street left-turns. This approach is because major street through vehicles are assumed to experience zero delay, a weighted average of all movements results in very low overall average delay, and this calculated low delay could mask deficiencies of minor movements.
Table 3-3 summarizes the criteria used to define LOS.
Traffic operations during the AM and PM peak hours were analyzed for the 2019 existing year. The operations analysis for the study intersections used the software program Synchro (version 10) for signalized and unsignalized intersections. ${ }^{3}$ Synchro is a macroscopic analysis and optimization software application that supports the Transportation Research Board Highway Capacity Manual's methodology (2000, 2010, and 6th Edition methods) for signalized and unsignalized intersections. The Synchro model was calibrated to accurately reflect existing congestion during the PM peak commute.

Table 3-3. Level of Service Criteria

|  | Signalized <br> Intersections <br> (seconds per vehicle) | Unsignalized <br> Intersections <br> (seconds per vehicle) | Traffic Flow Characteristics <br> (seconds per vehicle) |
| :---: | :---: | :---: | :--- |
| A | $<10$ | $<10$ | Virtually free flow; completely unimpeded |
| B | $>10$ and $<20$ | $>10$ and $<15$ | Stable flow with slight delays; less freedom to <br> maneuver |
| C | $>20$ and $<35$ | $>15$ and $<25$ | Stable flow with delays; less freedom to maneuver |
| D | $>35$ and $<55$ | $>25$ and $<35$ | High density but stable flow |
| E | $>55$ and $<80$ | $>35$ and $<50$ | Operating conditions at or near capacity; unstable flow |
| F | $>80$ | $>50$ | Forced flow; breakdown conditions |

SOURCE: Highway Capacity Manual 2010 (Transportation Research Board 2010)
a The LOS criteria are based on control delay, which includes initial deceleration delay, final deceleration delay, stopped delay, and queue move-up time.

[^5]LOS operation standards for the study intersections differ between Kitsap and Mason County intersections. Based on Puget Sound Regional Council (PSRC) standards for Highways of Statewide and Regional Significance, the LOS standard for the SR 3/Lake Flora intersection is LOS D. For the remaining study intersections, all of which are in Mason County, the WSDOT standard is LOS C, consistent with the standard for rural highways of statewide significance.

SR 3 in Belfair regularly experiences congestion during peak commute hours. During the PM peak, commute queues often extend through Belfair and as far north as Log Yard Road. SR 3 also experiences seasonal fluctuations from tourist traffic and recreational users, resulting in congested conditions on Friday afternoons and summer weekends.

As shown in Table 3-4, the intersections of SR 3 and NE Clifton Lane and SR 3 and Old Belfair Highway do not meet LOS standards during either of the existing AM and PM peak hours.

Table 3-4. Existing Year (2019) AM and PM Peak Hour Intersection Operations

| Intersection on SR 3 | Traffic Controla | LOS <br> Standard | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | LOS ${ }^{\text {b }}$ | Delay (sec/veh) | $\begin{aligned} & \text { V/C } \\ & \text { Ratio } \end{aligned}$ | LOS | Delay (sec/veh) | $\begin{aligned} & \text { V/C } \\ & \text { Ratio } \end{aligned}$ |
| Lake Flora Road | Stop Signa | D | C | 24 | 0.34 | D | 27 | 0.33 |
| Log Yard Road | Stop Sign | C | C | 17 | 0.11 | C | 16 | 0.06 |
| NE Clifton Lane | Signal | C | D | 40 | 1.02 | E | 76 | 1.28 |
| Old Belfair Highway | Stop Sign | C | E | 42 | 0.45 | F | 54 | 0.90 |
| SR 106 | Signal | C | B | 18 | 0.66 | C | 23 | 0.94 |
| SR 302 | Stop Sign | C | C | 15 | 0.24 | B | 13 | 0.24 |

a Stop controlled on minor leg(s).
${ }^{b}$ For unsignalized intersections, the LOS and delay are reported for the worst movement. For signalized intersections, LOS and delay are reported for the intersections as a whole.
c $\mathrm{V} / \mathrm{C}$ ratio provided represents $\mathrm{v} / \mathrm{c}$ ratio of the worst approach at the intersection.

### 3.3.4 Travel Times

Existing AM and PM peak travel times on SR 3 through the study area were collected from three sources: field observations, Google Maps, and the Synchro model. Travel time was collected in the field on May 1, 2019, which coincided with the collection of traffic counts and tube counts in the study area. Dash camera video was taken during the travel time runs. The video of the travel time run provides context and allows congested segments of the roadway to be identified, but because it provides only a single data point, travel times collected via the dash camera video may differ from typical conditions.

Google Maps is a web-based mapping service that can be used to provide typical travel times between two points. The travel time for Google Maps is often presented as a range of times because the travel time data is aggregated. For the SR 3 Freight Corridor study, the lowest and highest travel times from the peak hour on a typical midweek day were used.

Synchro travel times were calculated using signal delay and the link travel time (link distance divided by posted speed limit). While Synchro does account for the delay at signals, the model tends to underestimate delay when approach volumes are over capacity. Because of these limitations, the Synchro travel times typically underestimate travel times in comparison to field observations and Google Maps travel times. Table 3-5 shows the northbound and southbound travel times from each source.

Table 3-5. Existing Travel Time along SR 3 Freight Corridor between Lake Flora Road and SR 302

|  | AM Peak Hour |  | PM Peak Hour |  |
| :--- | :---: | :---: | :---: | :---: |
|  | Northbound <br> Direction <br> (mins) | Southbound <br> Direction <br> (mins) | Northbound <br> Direction <br> (mins) | Southbound <br> Direction <br> (mins) |
|  | 7 | 9 | 7 | 11 |
| Travel Time via Dashcam | 9 | 11 | 8 | 17 |
| Travel Time via Google Maps <br> $(\text { Low-High })^{a}$ | 10 | 10 | $9-13$ | $10-21$ |

a Google Maps results show a range of values for the PM peak hour due to congestion in the area. Google Maps does not show a range for the AM peak hour, as travel times tend to be more consistent during this time period.

### 3.3.5 Origin Destination Analysis

For this study, origin destination (OD) data were collected using StreetLight Data. StreetLight Data is a company that provides data from smartphones and other devices with location-based services to track to the overall origin and destination of trips through an area. Survey data from a 12-month period (February 2018 through January 2019) were used to estimate vehicle origins and destinations in the study area. OD data were collected at:

- SR 302 east of SR 3
- SR 106 west of SR 3
- Old Belfair Highway west of SR 3
- NE Old Belfair Highway north of Old Belfair Highway
- SR 3 North of Lake Flora Road
- SR 3 South of SR 302

Figure 3-5 illustrates the percentage of vehicles recorded with Streetlight Data that passed completely through Belfair. During midweek (Tuesday through Thursday) the percentage of vehicles traveling northbound between SR 302 and Lake Flora Road ranged from 33 percent to 50 percent, depending on the time of day. In the southbound direction, the percentage of traffic is consistent at 25 during midweek.

Data were also collected and reported for the Friday PM peaks and average weekend days at various times throughout the year. The data show that higher percentages of northbound traffic than southbound traffic pass completely through Belfair for all time periods reported, except for the average Friday PM peak hour, where the percentage of southbound traffic traveling from Lake Flora Road to SR 302 is higher than the northbound (39 percent versus 28 percent).

SR 3 Freight Corridor Transportation Discipline Report Washington State Department of Transportation


OMapbox, © OpenStreetMap

Figure 3-5. 2019 Existing Origin/Destination Travel Patterns

### 3.4 Collision History / Safety Analysis

Under 23 United States Code $\S 148$ and 23 United States Code §407, safety data, reports, surveys, schedules, lists compiled or collected for the purpose of identifying, evaluating, or planning the safety enhancement of potential crash sites, hazardous roadway conditions, or railway-highway crossings are not subject to discovery or admitted into evidence in a Federal or State court proceeding or considered for other purposes in any action for damages arising from any occurrence at a location mentioned or addressed in such reports, surveys, schedules, lists, or data.

A basic safety level analysis of the corridor was performed that assessed current safety performance, summarized recent crash history, and reported on any major contributing factors to fatal and serious injury crashes. Crash data were collected between January 1, 2018, through December 31, 2022, on the SR 3 corridor between MPs 22.81 and 29.49. During this time, 402 crashes were reported, of which 72 occurred at the study intersections.

Table 3-6 summarizes crashes at intersections and along the SR 3 study area segment by severity and type. Crash records indicate the type and severity of crashes appears to be consistent with congested urban conditions in other areas of Washington State. Rear-end and property damage only (PDO) or non-injury crashes account for the greatest number of crashes. The number of crashes tends to increase under congested conditions but the severity of those crashes is generally lower, due to lower speeds.

### 3.4.1 Intersection Collisions

Between January 2018 and December 31, 2022, one serious injury crash occurred at a study area intersection. There were no fatal intersection crashes.

The serious injury crash occurred at the Lake Flora Rd intersection (MP 28.78). This crash is listed as an angle collision with a driver attempting to turn left. Contributing factors include one vehicle not granting the right-of-way to the vehicle traveling on SR 3 and the other vehicle exceeding the posted speed limit. This crash also involved a motorcycle.

The types of crashes that occurred most frequently at the study intersections were rear-end crashes and left-turn angle crashes, which accounted for 49 percent and $15 \%$, respectively, of the total intersection crashes. The intersections of SR 3/NE Clifton Lane (MP 26.55) and SR 3/Lake Flora Road (MP 28.78) had the highest crash rates in the study area with 3.0 and 5.0 crashes per year, respectively.

## Table 3-6. Historical Crash Rates and Crashes Summarized by Severity and Type for Study Intersections and Segments

| Intersection/ Segment |  |  | Crash Severity |  |  |  | Crash Type |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Minor or Possible Injury | O | $\begin{aligned} & \text { 이 } \\ & \frac{\mathbb{Z}}{1} \\ & \text { 区1 } \end{aligned}$ | $\frac{0}{900} \frac{0}{\frac{10}{6}}$ |  |  | $\begin{aligned} & \text { 든 } \\ & \text { 든 } \\ & \text { 은 } \\ & \text { 후 } \end{aligned}$ |  |  |  |  |  | 㐫 |
| Intersection Crashes |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| (1) SR 3/Lake Flora Road | 3.0 | 15 | 0 | 1 | 5 | 9 | 0 | 5 | 0 | 1 | 0 | 4 | 0 | 0 | 0 | 5 | 0 |
| (2) SR 3/Log Yard Road | 0.6 | 3 | 0 | 0 | 0 | 3 | 0 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (3) SR 3/NE Clifton Lane | 5.0 | 25 | 0 | 0 | 7 | 18 | 0 | 3 | 0 | 15 | 6 | 0 | 1 | 0 | 0 | 0 | 0 |
| (4) SR 3/OId Belfair Highway | 2.0 | 10 | 0 | 0 | 0 | 10 | 0 | 2 | 1 | 4 | 0 | 1 | 0 | 0 | 0 | 1 | 1 |
| (5) SR 3/SR 106 | 1.6 | 8 | 0 | 0 | 1 | 7 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| (6) SR 3/SR 302 | 2.2 | 11 | 0 | 0 | 2 | 9 | 0 | 0 | 0 | 5 | 2 | 2 | 0 | 0 | 0 | 2 | 0 |
| Intersection Total | 14.4 | 72 | 0 | 1 | 15 | 56 | 0 | 11 | 1 | 35 | 8 | 7 | 1 | 0 | 0 | 8 | 1 |
| Segment Crashes ${ }^{\text {c }}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| SR 3: Lake Flora Road to NE Clifton (MP 29.00 to 26.55) | 28.0 | 140 | 1 | 2 | 23 | 114 | 2 | 35 | 11 | 51 | 10 | 6 | 0 | 0 | 13 | 6 | 6 |
| SR 3: NE Clifton to SR 106 (MP 26.55 to 24.91) | 26.6 | 133 | 0 | 4 | 17 | 112 | 2 | 25 | 7 | 65 | 8 | 11 | 1 | 2 | 1 | 6 | 5 |
| SR 3: SR 106 to SR <br> 302 (MP 24.91 to <br> 23.26) | 11.4 | 57 | 1 | 1 | 10 | 45 | 2 | 2 | 3 | 20 | 1 | 12 | 0 | 0 | 4 | 11 | 2 |
| Segments Total | 66.0 | 330 | 2 | 7 | 50 | 271 | 6 | 62 | 21 | 136 | 19 | 29 | 1 | 2 | 18 | 23 | 13 |

Source: January 2018 - December 2022 data from WSDOT Crash Database
a PDO = Property damage only
b Off-Road crashes refer to crash types involving roadway ditches, embankments, overturned vehicles, or crash cushions.
c Segment crashes refer to crashes on SR 3 between MP 23.26 and MP 29.00 that were not related and/or did not occur at a study intersection.

### 3.4.2 Segment Collisions

On SR 3 segments, 330 crashes were reported with the majority occurring between Lake Flora Road at MP 28.78 and NE Clifton Lane at MP 26.55 (42 percent), and between NE Clifton Lane and SR 106 at MP 24.91 (40 percent).

Two fatal crashes occurred in the study area during the study period. One was at MP 24.21, about halfway between SR 302 and SR 106. This was a fixed object collision that occurred negotiating a curve but did not list a contributing factor. The other fatal crash occurred at MP 26.78, north of NE Clinton Ln at a driveway. It was an angle crash that occurred during wet roadway conditions.

Seven of the segment crashes were serious injury crashes. The SR 3 milepost where the crash occurred and the type of crash are listed below:

- MP 24.38 - off-road collision involving a roadway ditch, involved alcohol
- MP 25.16 - opposite-direction sideswipe collisions, involved alcohol
- MP 25.20 - fixed object collision while operating defective equipment
- MP 25.63 - fixed object collision, involved alcohol
- MP 26.01 - angle collision with a failure to grant right-of-way to oncoming vehicle
- MP 26.72 - angle collision with a failure to grant right-of-way to oncoming vehicle
- MP 28.98 - rear end collision involving a distracted driver

The top contributing factor noted in these serious injury crashes included alcohol (43 percent). Other contributing factors also included exceeding the stated/safe speed (29 percent), failure to grant right-of-way (29 percent). ${ }^{4}$

Similar to the crashes reported at the study area intersections, rear-end crashes were the most common crash along the corridor (41 percent). The majority of rear end crashes were attributed to following too closely ( 46 percent) followed by speeding ( 24 percent). Overall, for segment crashes, the key contributing factors were following too closely, distraction/inattention, failure to grant right-ofway/disregard traffic control, and speeding. The factors accounted for over 62 percent of segment crash contributing factors. Additionally, of the 330 crashes not related to the study intersections (segment crashes), approximately 25 percent occurred at or were related to driveways in the study corridor.

[^6]
## 4. Potential Effects of the Project

### 4.1 Direct Effects

### 4.1.1 Construction impacts

Under a No-Build alternative, direct effects such as temporary traffic disruption due to construction would not occur. Noise, air quality, water quality, and other construction related direct effects would likewise be absent. However, travelers would continue to experience congestion and delay during peak periods. Access to and from business and other services would continue to be difficult as gaps between vehicle platoons progressing through the corridor become nonexistent.

Direct effects of the Build alternative, i.e. the Project Action or the SR 3 Freight Corridor would entail temporary construction effects. Travelers would experience construction related traffic delay and may need to take detour routes for a period of time. Since the majority of the Freight Corridor alignment is through forested land, a major portion of the work would not lead to direct disruption to traffic. There would be an increase in traffic on existing streets as construction workers go to work sites or bring in and remove equipment and materials. Temporary closures of roadway segments may be required while the new corridor is connected to the existing SR 3 alignment. Other than minor increases in travel times, no impacts to transit services through the corridor are expected. There may be temporary air quality, water quality, and noise effects due to construction, but on-site mitigation measures and standard procedures should offset the effects and render the effects not significant.

Direct benefits of constructing the freight corridor include creation of construction jobs created and increase to network capacity at the completion of the project.

### 4.1.2 Project impacts

The future transportation network without the SR 3 Freight Corridor would mean the network would continue to be capacity constrained, particularly SR 3 north of NE Clifton Lane. In 2050, the travel delay at many of the key intersections associated with the No-Build alternative would fail. Travel demand modeling and traffic operations analysis results provide the basis for evaluating the long term and cumulative effects of the Project Action relative to the No-Build condition.

A number of network performance measures related to the direct effect of the SR 3 Freight Corridor alternative were measured, including:

- Roadway traffic volumes
- Route travel times
- Intersection traffic operations


### 4.1.2.1 Forecast Roadway Traffic Volumes

Travel forecasts along SR 3 were estimated using a combination of historical growth and peripheral travel demand data from PSRC and SR 16 Travel Demand Models. Historical data about SR 3 from the past 10 years show an average growth rate of 2 percent for the AM peak hour and 1 percent for the PM peak hour. These growth rates were used to estimate the 2028 Build volumes.

In addition to historic growth, the 2050 forecast assumed buildout for the master plan for the PSIC, as well as additional development in the Belfair UGA from future Kitsap County connections to the SR 3 Freight Corridor. With these assumptions, 2050 average annual growth in the SR 3 Freight Corridor is forecast to exceed 3 percent in the AM peak hour and would average nearly 5 percent annual growth in the PM peak hour. Figures 4-1 through 4-4 illustrate the 2028 and 2050 AM and PM peak hour forecasted volumes.


[^7]Figure 4-1. 2028 AM Peak Hour No-Build Volumes


Figure 4-2. 2028 PM Peak Hour No-Build Volumes


[^8]Figure 4-3. 2050 AM Peak Hour No-Build Volumes


[^9]Figure 4-4. 2050 PM Peak Hour No-Build Volumes

Figure 4-5 illustrates the forecast percentage of AM and PM peak hour traffic that is expected to use the SR 3 Freight Corridor during both the 2028 and 2050 years. The percentages are based on output from the travel demand models. The percentage of traffic using the SR 3 Freight Corridor is expected to increase over time to a forecast of approximately 45-68 percent by the 2050 AM and PM peak hours, depending on direction. Trip distribution is expected to change compared to existing patterns based on forecasted in-fill development around the new freight corridor.


[^10]Figure 4-5. Forecasted Peak Hour Travel Patterns

Table 4-1 shows the forecast change in traffic volumes for the existing mainline SR 3 at selected locations for the No-Build and Project Action alternatives. The forecast shows there is a significant reduction in 2050 bi-directional PM peak hour traffic volumes on the existing SR 3 corridor with the construction of the SR 3 Freight Corridor when compared to the No-Build conditions. This reduction in traffic volumes along the existing SR 3 corridor would help reduce future traffic congestion and queuing through Belfair.

Table 4-1. Change in SR 3 Bi-Directional Volumes - 2050 PM Peak Hour Traffic Forecast

| Location | SR 3 No-Build | SR 3 with Freight Corridor | \% Change |
| :--- | :---: | :---: | :---: |
| SR 3, South of Lake Flora Rd | 2,085 | 1,455 | $-43 \%$ |
| SR 3, North of NE Old Clifton <br> Rd | 2,500 | 1,845 | $-36 \%$ |
| SR 3, South of Old Belfair Hwy | 2,610 | 1,845 | $-41 \%$ |
| SR 3, North of SR 106 | 2,650 | 1,950 | $-36 \%$ |

### 4.1.2.2 Forecast Route Travel Times

Future travel times on the existing SR 3 and the proposed SR 3 Freight Corridor were estimated for both the 2028 and 2050 future analysis years. Synchro travel times are calculated using signal delay and the link travel time (link distance divided by posted speed limit). For the Project Action alternative, roundabouts were assumed at the north and south end connections. Delay for roundabouts was included in the estimates of the Project Action alternative.

As shown in Figure 4-6, the estimated travel time on the new SR 3 Freight Corridor is expected to be six minutes in either direction, cutting travel times for regional through-traffic by half or more. Additionally, with the SR 3 Freight Corridor removing traffic from existing SR 3, travel times on the existing SR 3 corridor are expected to be five minutes faster in the 2028 PM peak hour and 8 minutes faster by the 2050 PM peak hour, as compared with No-Build conditions.

### 4.1.3 Intersection Traffic Operations

WSDOT screens and evaluates intersection control alternatives to determine the best possible intersection type and design for a given location. The evaluation considers multiple factors, including project needs, feasibility (e.g. available right-of way, environmental concerns, etc.), operations, safety, and context.

Future traffic operations for the intersections along the SR 3 existing corridor were forecast and intersection control alternatives evaluated for the north and south endpoints of the proposed SR 3 Freight Corridor. The new end connections were evaluated for signalized and roundabout operations. Operations for the signalized alternative utilized the software program Synchro 10. Operations for the roundabout alternatives used Sidra 8, consistent with WSDOT Sidra Policy.

PSRC's standard for Highways of Statewide and Regional Significance is LOS D for signalized operations. Roundabout operation standards are based on WSDOT Sidra Policy. Roundabouts with a $\mathrm{v} / \mathrm{c}$ ratio between 0.85 to 0.90 range are considered to operate within WSDOT standards.



Figure 4-6. Future Travel Times

### 4.1.3.1 Local Intersection Operations

Tables 4-2 and 4-3 show the forecast LOS at intersections in the study area, with the exception of intersections at SR 302 and Lake Flora Road, where the SR 3 Freight Corridor would reconnect with the existing SR 3. Alternatives and LOS for those connections are discussed in the following sections.

Redistribution of traffic to the SR 3 Freight Corridor would reduce traffic volumes along the existing SR 3, improving both LOS and congestion at study area intersections. The intersections of SR 3/OId Belfair Highway and SR 3/NE Clifton Lane are still forecast to operate below standard in the Project Action alternative, but with considerably less delay than under the No-Build alternative.

Table 4-2. 2028 AM and PM Peak Hour Intersection Operations

| Peak Hour | Intersection on SR 3 | Traffic Control | 2028 No-Build |  |  | 2028 Build |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | LOS ${ }^{\text {a }}$ | Delay (sec/veh) | $\begin{gathered} \text { V/C } \\ \text { Ratiob } \end{gathered}$ | LOS | Delay (sec/veh) | $\mathrm{V} / \mathrm{C}$ Ratio |
| AM | SR 3 and Log Yard Road | Roundabout ${ }^{\text {c }}$ | A | 6 | 0.89 | A | 6 | 0.53 |
|  | SR 3 and NE Clifton Lane | Signal | E | 60 | - | D | 40 | - |
|  | SR 3 and Old Belfair Highway | Stop Signd | F | 85 | - | C | 25 | - |
|  | SR 3 and SR 106 | Signal | B | 19 | - | B | 17 | - |
| PM | SR 3 and Log Yard Road | Roundabout | A | 6 | 0.75 | A | 6 | 0.52 |
|  | SR 3 and NE Clifton Lane | Signal | F | 106 | - | D | 42 | - |
|  | SR 3 and Old Belfair Highway | Stop Sign | F | >180 | - | F | 58 | - |
|  | SR 3 and SR 106 | Signal | E | 73 | - | C | 21 | - |

a For unsignalized intersections, the LOS and delay are reported for the worst movement. For signalized intersections, LOS and delay are reported for the intersections as a whole.
b V/C ratio provided represents $\mathrm{V} / \mathrm{c}$ ratio of the worst approach at the intersection
c Plans for roundabout to be constructed at SR 3 and Log Yard Road prior to 2028
d Stop controlled on minor leg(s)
Table 4-3. 2050 AM and PM Peak Hour Intersection Operations

| Peak Hour | Intersection on SR 3 | Traffic Controla | 2050 No-Build |  |  | 2050 Build |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | LOS ${ }^{\text {b }}$ | Delay (sec/veh) | V/C Ratioc | LOS | Delay (sec/veh) | V/C <br> Ratio |
| AM | SR 3 and Log Yard Road | Roundabout ${ }^{\text {d }}$ | D | 39 | 1.11 | A | 6 | 0.68 |
|  | SR 3 and NE Clifton Lane | Signal | F | 128 | - | E | 79 | - |
|  | SR 3 and Old Belfair Highway | Stop Sign | F | >180 | - | F | 61 | - |
|  | SR 3 and SR 106 | Signal | C | 31 | - | B | 20 | - |
| PM | SR 3 and Log Yard Road | Roundabout | C | 29 | 1.08 | A | 9 | 0.72 |
|  | SR 3 and NE Clifton Lane | Signal | F | >180 | - | F | 158 | - |
|  | SR 3 and Old Belfair Highway | Stop Sign | F | >180 | - | F | >180 | - |
|  | SR 3 and SR 106 | Signal | F | >180 | - | D | 43 | - |

a Stop-sign= stop sign controlled on minor leg(s).
b For unsignalized intersections, the LOS and delay are reported for the worst movement. For signalized intersections, LOS and delay are reported for the intersections as a whole.
c V/C ratio provided represents v/c ratio of the worst approach at the intersection.
d Plans for roundabout to be constructed at SR 3 and Log Yard Road prior to 2028.

### 4.1.3.2 North and South End Connections

The north end connection of the SR 3 Freight Corridor to SR 3 would be a single-lane roundabout near the intersection of Lake Flora Road. The new connection would consist of four legs: SR 3 connecting north to Gorst, SR 3 connecting west to Belfair, the new SR 3 Freight Corridor, and Lake Flora Road, as shown in Figure 4-7. Local access connections would be provided at Lake Flora Road, northwest of the new intersection. The design includes a slip lane that avoids the roundabout and provides direct access to the business loop. This design incorporates a footprint able to expand to a multi-lane roundabout to accommodate future growth. Operation results for 2028 and 2050 conditions are shown in Table 4-4.

Table 4-4. Future Peak Hour Operations - North end Connection at Lake Flora Road Intersection

|  | AM Peak Hour |  |  |  |  |  | PM Peak Hour |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2028 Build |  |  | 2050 Build |  |  | 2028 Build |  |  | 2050 Build |  |  |
| Intersection Control | LOS | Delay (sec/veh ) | V/C <br> Ratio | LOS | Delay (sec/veh ) | V/C <br> Ratio | LOS | Delay (sec/veh) | V/C Ratio | LOS | Delay (sec/veh) | V/C <br> Ratio |
| Roundabout | B | 9 | 0.62 | E | 61 | 1.37 | A | 9 | 0.69 | E | 70 | 1.25 |

The south end connection would include two single-lane roundabouts as shown in Figure 4-8. The two single-lane roundabouts would provide improved connections to SR 3 and local roadways as compared to No-Build conditions while minimizing potential impacts to adjacent 4(f) properties, stream crossings and wetlands. They would provide access to North Mason High School and E Belwood Lane and improve the connections southbound connection on SR 3 toward Allyn. The design also incorporates separated multi-use pathways. Operation results for 2028 and 2050 conditions are shown in Table 4-5.

Table 4-5. Future Peak Hour Operations - Southern Endpoint

| Intersection Control | AM Peak Hour |  |  |  |  |  | PM Peak Hour |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2028 Build |  |  | 2050 Build |  |  | 2028 Build |  |  | 2050 Build |  |  |
|  | LOS | Delay (sec/veh) | $\mathrm{V} / \mathrm{C}$ <br> Ratio | LOS | Delay (sec/veh) | V/C Ratio | LOS | Delay (sec/veh) | V/C Ratio | LOS | Delay (sec/veh) | $\mathrm{V} / \mathrm{C}$ <br> Ratio |
| Split RAB - <br> West RAB | A | 6 | 0.56 | A | 7 | 0.71 | A | 8 | 0.68 | B | 11 | 0.85 |
| Split RAB - <br> East RAB | A | 7 | 0.43 | A | 8 | 0.55 | A | 6 | 0.33 | A | 7 | 0.47 |



Figure 4-7. North End Connection at Lake Flora Road


Figure 4-8. South End Connection at SR 302

### 4.1.4 Future Highway Traffic Operations

Consistent with the previous EA published in 2013, a mainline level of service analysis for the entire SR 3 Freight Corridor was performed. The software program HCS 7 was used to evaluate both the existing one-mile highway segment north of Lake Flora Road and the proposed SR 3 Freight Corridor south of Lake Flora Road. Table 4-6 shows the highway operations for the proposed Freight Corridor.

Table 4-6. Future Conditions PM Peak Hour Highway Operations

|  | SR 3 without Freight Corridor |  | Future SR 3 Freight Corridor |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Percent Time <br> Spent Following <br> (PTSF)a | LOS | V/C <br> Reatio | Percent Time Spent <br> Following <br> (PTSF) $)^{1}$ | Delay <br> (sec/veh) | V/C <br> Ratio |
| 2019 | $77 \%$ | D | 0.44 | - | - | - |
| 2028 | $79 \%$ | D | 0.47 | $46 \%$ | B | 0.14 |
| 2050 | $84 \%$ | E | 0.55 | $78 \%$ | D | 0.44 |

a Average time percent of total travel time that vehicles must travel in platoons behind slower vehicles due to inability to pass on a twolane highway (HCM 6th Edition, 2016).

In the Project Action alternative, the SR 3 Freight Corridor would operate at LOS B in 2028 and would operate at LOS D in 2050, with a similar v/c ratio as the existing SR 3 corridor through Belfair. Based on results of the operations analysis, a two-lane highway meets WSDOT standards for the mainline of the proposed SR 3 Freight Corridor.

### 4.1.5 The No-Build Future

The 2050 No-Build travel demand modeling show intersection and roadway congestion at several intersections in the study corridor. NE Clifton Lane and Old Belfair Highway are forecast to operate at LOS F during the AM peak and PM peaks. Additionally, SR 106 is forecast to operate at LOS F during the PM peak. The forecast delay for these intersections exceeds 180 seconds during both peaks, except NE Clifton Lane, where delay is forecast to be 128 seconds during the AM peak.

By 2050, the entire SR 3 corridor is forecast to operate at LOS E during the PM peak under the NoBuild condition.

Failure to construct improvements in the corridor would result in additional congestion, increased duration of delay, longer travel times, exacerbation of safety issues, and potential impacts to air quality precipitated by idling engines in very long queues at signalized and minor street unsignalized intersections. Access to and from business and other services would become difficult as gaps between vehicle platoons progressing through the corridor become nonexistent.

Under the No-Build alternative, the heavier traffic flow of passenger cars, trucks, and recreational vehicles through Belfair would have implications with respect to aesthetics, noise pollution, air quality, commercial and retail activities, as well other considerations. Presumably, with heavier traffic volumes, access to and from unsignalized intersections and businesses may be an issue over a longer period, as the peak hour is elongated and spreads congestion through longer periods of the day.

### 4.1.6 The Project Alternative Future

The SR 3 Freight Corridor would serve multiple purposes including reduced congestion and increased safety on SR 3, provision of an alternate route for regional traffic, and promotion of economic vitality. It would improve intermediate and long-term regional transportation mobility on the SR 3 corridor in northeast Mason and southwest Kitsap counites. The project would improve regional travel times between Shelton and Bremerton, provide safe and reliable regional access to jobs, goods, and services, and provide for the efficient movement of freight.

A two-lane highway would move regional traffic and meets the forecasted traffic demand through the year 2050. It would improve movement of freight, reduce commute travel times between Kitsap and Mason counties, accommodate seasonal changes in traffic, and help reduce traffic congestion and queuing through Belfair.

The Project Action alternative has safety benefits for users. With reduced traffic volume resulting from diversion of regional through traffic to the freight corridor, the existing SR 3 mainline would experience less congestion and delay and improved travel times. Lower volumes would lessen exposure and are likely to ease congestion related rear-end collisions. With lower volumes, left turning movement would find more gaps to turn safely.

The design section for the proposed SR 3 Freight Corridor states that it would be a limited access facility. The cross-section would include two 12 -foot lanes and two 8 -foot shoulders that can accommodate bicyclist and pedestrians. Separate pedestrian and bicycle paths would not be included along this facility as part of this project.

The Project Action alternative would provide an alternate route during emergencies and for emergency services. Regional response time would likely improve.

The anticipated effect of the Project Action on transit operations is beneficial. Reduced congestion and delay would improve transit operations. Additionally, the bypass provides alternate faster regional transit routes.

### 4.2 Indirect and Cumulative Effects

According to CFR 1508.8, indirect effects are caused by the project but can be later in time or farther removed in distance from the project. The SR 3 Freight Corridor project would provide greater vehicle capacity and better travel times for regional traffic through the Belfair vicinity. Improved travel times would allow for growth in activities and associated travel connected to businesses, commercial enterprises, and residences served by SR 3 outside of Belfair that are particularly dependent on regional traffic. However, both Mason and Kitsap Counties come under the state's Growth Management Act and have comprehensive planning in place to address the magnitude, form, and process associated with such land use changes. Therefore, no indirect impacts to traffic in or around the study area are predicted due to the Project Action.

According to CFR 1508.7, cumulative impacts are impacts on the environment which results from the incremental impact of the action when added to other past, present, and reasonably foreseeable future actions regardless of what agency (Federal or non-Federal) or person undertakes such other actions. Since no increase in total traffic as a result of the SR 3 Freight Corridor is predicted in or around the study area, beyond that which is already reflected in the forecast model, no contribution to cumulative traffic impacts in the area are predicted.

Further consideration about the indirect and cumulative impact of the SR 3 Freight Corridor project on land use changes can be found in the Land Use discipline report.

## 5. Mitigation and Conclusion

### 5.1 What the Required Project Would Achieve

### 5.1.1 What Existing and Future Transportation Needs Are Addressed

The proposed SR 3 Freight Corridor Project would provide a solution to the immediate and long-range regional transportation mobility and safety needs of the SR 3 corridor in northeast Mason and southwest Kitsap counties. It would provide a reliable regional route between Kitsap and Mason Counties. The SR 3 Freight Corridor would also reduce congestion and improve safety through Belfair and provide an alternate route for emergency vehicles. Implementation of this project would provide safe and reliable access to regional jobs, goods and services, and improve efficiencies for transit and other public service providers.

The two-lane facility on a new alignment would move regional traffic travelling between Shelton and Bremerton to a new roadway, bypassing Belfair. It would ensure efficient movement of freight, commute trips between Kitsap and Mason counties, accommodate seasonal influxes of tourist traffic, and serve general traffic needs through to the design year 2050. It would also serve as an alternate route during highway closures on existing SR 3 in Belfair.

### 5.2 Any Mitigation to Avoid or Minimize Adverse Effect

There are no significant transportation impacts due to the Project Action therefore mitigation measures for transportation are not necessary. However, due to growth forecast for the design year baseline conditions, transportation improvements would be necessary in the Belfair area to maintain service levels.

While mitigation measures are not necessary resulting from the Project Action, the following sections identify future improvements which may be required even with construction of the freight corridor.

### 5.2.1 SR 3 Freight Corridor Capacity

The horizon year (2050) identified for the project reflects the growth assumed in the local agency comprehensive plans and the growth (full build-out) assumed for the PSIC. Redistribution of traffic to the SR 3 Freight Corridor would reduce traffic volumes along the existing SR 3, improving both LOS and congestion at intersections along existing SR 3. The intersections at SR 3/OId Belfair Highway and SR 3/NE Clifton Lane are still forecast to operate below standard in the Project Action alternative, but with considerably less delay than under the No-Build alternative. The design for the north end connection at Lake Flora Road incorporates a footprint able to expand to a multi-lane roundabout to accommodate future growth.

### 5.2.2 Existing SR 3 Capacity

Depending on actual growth, highway segment LOS analysis for existing SR 3 through Belfair for 2050 baseline conditions (No-Build) show that the SR 3 corridor exhibits failing conditions. SR 3 mainline capacity increase may be needed to maintain service levels.

### 5.2.3 Intersection Control and Capacity

While the Project Action alternative has no significant impact on the existing SR 3 alignment through Belfair, intersection capacity improvements would be needed NE Clifton Lane and Old Belfair Highway to meet WSDOT LOS standards in the future. These needs are not due to the Project Action alternative, but by design year baseline (No-Build) forecast in the corridor. The Project Action alternative provides benefits through additional capacity and traffic volume reduction occurs at the existing SR 3 alignment through Belfair, as regional through traffic are diverted to the freight corridor.

Performance measures with the freight corridor such as traffic volume reduction through redistribution, reduced intersection delay and improved operating speeds, and improved travel time and LOS all are consistent with the purpose and need of the Project Action.

### 5.2.4 Local Connections

The Project Action would construct a new bypass highway around the Belfair community. It would be a limited access highway, however, the design would allow for two local connections between the Business Loop and the Freight Corridor, one at Romance Hill and one at the Kitsap County line, to facilitate local connections to Belfair and the Business Loop.

### 5.2.5 Findings and Conclusions

Analysis of the No-Build and the Project Action alternatives are documented in this report. Findings on the potential advantages and disadvantages for the No-Build and the Project Action alternatives are summarized below, followed by conclusions.

### 5.2.5.1 No-Build Alternative

Traffic volumes are forecast to grow through the design year (2050), resulting in congestion throughout the study corridor. Travel times would be greatly increased to a point where SR 3 would no longer be a viable freight route alternative. Intersection delay would be high and duration of congestion would last for hours.

Substantial and costly improvements would be needed to restore functional health of SR 3. Improvements could include widening the mainline and constructing capacity improvements at multiple intersections.

### 5.2.5.2 Project Action Alternative

Construction of the SR 3 Freight Corridor would meet the purpose and need of the Project Action. Improved travel time on the freight corridor and reduced delay at intersections on SR 3 would improve mobility and connectivity. The existing SR 3 alignment through Belfair would become a business loop with reduced traffic volumes, less delay, and improved travel times. Improved service levels would be achieved considering urban characteristics of the corridor, particularly through Belfair's commercial core. The freight corridor would perform at an improved operating speed through 2050.

Mason County should consider improving local road connectivity and improving parallel routes to maximize the benefits of the bypass.

### 5.2.6 Conclusions

Failure to construct improvements is not a realistic alternative for the SR 3 corridor in the Belfair vicinity. However, substantial and costly improvements will be needed in order for SR 3 to function reasonably well in the 2050 forecast year.

The SR 3 Freight Corridor would divert trips away from existing alignment of SR 3 through Belfair. Depending on the location, intersection volumes may be reduced on the business loop anywhere between 36 and 43 percent in the PM peak hour.

Past studies demonstrate that population and commercial growth in the SR 3 corridor would eventually overwhelm the transportation facility. These studies support the concept of the freight corridor. This report confirms and augments previous analyses that support the purpose and need for a two-lane freight corridor. This study finds no significant transportation impacts due to the Project Action alternative.

## 6. References

Bremerton Economic Development Study (BEDS), 2011, Washington State Department of Transportation.

Belfair Bypass 2010 Proviso Report, June 2010, Washington State Department of Transportation, Olympic Region.

Summary Report - Proposed SR 3 Belfair Bypass, June 30, 2009, Washington State Department of Transportation.

Draft SR 3, Belfair Bypass Transportation Discipline Report, June 2009, Washington State Department of Transportation, Eastern Region.

Belfair Bypass Traffic Analysis Report, September, 2008, The Transpo Group.
SR 3 Belfair Area Widening and Safety Improvements, Traffic Analysis Report, September, 2008, The Transpo Group.

SR 3 Belfair Bypass, Preferred Connection Alternatives Analysis, September 17, 2007, Washington State Department of Transportation.

Belfair Bypass, Environmental Assessment, November, 2001, Federal Highway Administration, Washington State Department of Transportation, Mason County.

## Appendix A

Existing Traffic Counts

|  |  |  | W L | AK <br> Pe <br> $\underset{7}{7}$ <br> 앙 <br> $\downarrow$ <br> TE <br> PH | V: 1 <br> F: 0 | OR <br> ur <br> ホ <br> 32 <br> 94 | R | SW L FLOR <br> 46 <br> 95 <br> 0 |  |  | C <br> V \%: <br> 2.1\% <br> 3.6\% <br> 6.1\% <br> 4.2\% | unt Pea <br> PHF <br> 0.88 <br> 0.96 <br> 0.87 <br> 0.94 | Dat eriod Hou |  | ed, M <br> 7:00 A <br> 7:00 A <br> dio <br> - <br> 1 <br> - | y 01 <br> to <br> to <br>  | 2019 <br> 9:00 A <br> 8:00 A |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Two-Hour Count Summaries |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Interval Start | 0 |  |  |  | SW LAKE FLORA RD |  |  |  | SR 3 |  |  |  | SR 3 |  |  |  | $\begin{gathered} \text { 15-min } \\ \text { Total } \end{gathered}$ | Rolling One Hour |
|  | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  |  |  |
|  | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT |  |  |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 24 | 0 | 9 | 0 | 0 | 185 | 27 | 0 | 3 | 73 | 0 | 321 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 25 | 0 | 14 | 0 | 0 | 196 | 27 | 0 | 2 | 117 | 0 | 381 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 29 | 0 | 11 | 0 | 0 | 202 | 26 | 0 | 2 | 102 | 0 | 372 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 17 | 0 | 12 | 0 | 0 | 195 | 21 | 0 | 5 | 108 | 0 | 358 | 1,432 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 18 | 0 | 7 | 0 | 0 | 159 | 14 | 0 | 3 | 74 | 0 | 275 | 1,386 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 17 | 0 | 4 | 0 | 0 | 163 | 26 | 0 | 7 | 77 | 0 | 294 | 1,299 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 21 | 0 | 9 | 0 | 0 | 166 | 24 | 0 | 2 | 97 | 0 | 319 | 1,246 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 15 | 0 | 3 | 0 | 0 | 150 | 11 | 0 | 6 | 104 | 0 | 289 | 1,177 |
| Count Total | 0 | 0 | 0 | 0 | 0 | 166 | 0 | 69 | 0 | 0 | 1,416 | 176 | 0 | 30 | 752 | 0 | 2,609 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 95 | 0 | 46 | 0 | 0 | 778 | 101 | 0 | 12 | 400 | 0 | 1,432 | 0 |
| Note: Two-hour count summary volumes include heavy vehicles but exclude bicycles in overall count. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Interval Start | Heavy Vehicle Totals |  |  |  |  |  | Bicycles |  |  |  |  |  | Pedestrians (Crossing Leg) |  |  |  |  |  |
|  | EB | WB | N | B | SB | Total | EB | WB |  |  | SB | Total | East |  | West | North | Sout | th Total |
| 7:00 AM | 0 | 0 | 1 | 1 | 2 | 13 | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 1 | 6 |  | 10 | 17 | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 2 |  |  | 6 | 16 | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 0 |  |  | 7 | 14 | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 1 |  |  | 12 | 24 | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 8:15 AM | 0 | 0 |  |  | 6 | 15 | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 8:30 AM | 0 | 0 |  |  | 10 | 18 | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 8:45 AM | 0 | 1 |  | 2 | 7 | 20 | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| Count Total | 0 | 5 |  | 2 | 60 | 137 | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| Peak Hr | 0 | 3 |  | 2 | 25 | 60 | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |


|  |  |  | W L | AK <br> Pe <br> © <br> 앙 <br> $\downarrow$ <br> TE <br> PH | ak ก <br> V: F: - |  | R |  | KE RD <br> $\leftarrow$ |  | C <br> V \%: <br> 4.4\% <br> 3.0\% <br> 3.6\% <br> 3.4\% | unt <br> Pea <br> PHF <br> 0.75 <br> 0.85 <br> 0.92 <br> 0.89 | Dat eriod Hou |  | ed, M <br> 4:00 P <br> 4:00 P <br> dio <br> i <br>  | 01 <br> to <br> to <br> $\rightarrow$ <br> O- | $\begin{aligned} & 2019 \\ & \text { 6:00 P } \\ & \text { 5:00 P } \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Two-Hour Count Summaries |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Interval Start | 0 |  |  |  | SW LAKE FLORA RD |  |  |  | SR 3 |  |  |  | SR 3 |  |  |  | $\begin{gathered} \text { 15-min } \\ \text { Total } \end{gathered}$ | Rolling One Hour |
|  | UT | Eastb | und TH | RT | UT | West | und | RT | Northbound |  |  |  | Southbound |  |  | RT |  |  |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 23 | 0 | 7 | 0 | 0 | 132 | 46 | 0 | 9 | 171 | 0 | 388 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 22 | 0 | 4 | 0 | 0 | 177 | 28 | 0 | 12 | 162 | 0 | 405 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 14 | 0 | 5 | 0 | 0 | 146 | 36 | 0 | 19 | 121 | 0 | 341 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 11 | 0 | 4 | 0 | 0 | 104 | 26 | 0 | 13 | 155 | 0 | 313 | 1,447 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 24 | 0 | 1 | 0 | 0 | 111 | 41 | 0 | 10 | 180 | 0 | 367 | 1,426 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 22 | 0 | 2 | 0 | 0 | 111 | 35 | 0 | 6 | 181 | 0 | 357 | 1,378 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 22 | 0 | 3 | 0 | 0 | 134 | 33 | 0 | 5 | 183 | 0 | 380 | 1,417 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 22 | 0 | 5 | 0 | 0 | 98 | 24 | 0 | 5 | 178 | 0 | 332 | 1,436 |
| Count Total | 0 | 0 | 0 | 0 | 0 | 160 | 0 | 31 | 0 | 0 | 1,013 | 269 | 0 | 79 | 1,331 | 0 | 2,883 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 70 | 0 | 20 | 0 | 0 | 559 | 136 | 0 | 53 | 609 | 0 | 1,447 | 0 |
| Note: Two-hour count summary volumes include heavy vehicles but exclude bicycles in overall count. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Interval Start | Heavy Vehicle Totals |  |  |  |  |  | Bicycles |  |  |  |  |  | Pedestrians (Crossing Leg) |  |  |  |  |  |
|  | EB | WB | N |  | SB | Total | EB | WB |  |  | SB | Total | East |  | West | North | Sou | Total |
| 4:00 PM | 0 | 2 | 4 |  | 5 | 11 | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 1 | 9 |  | 9 | 19 | 0 | 0 |  |  | 0 | 1 | 0 |  | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 1 | 6 |  | 3 | 10 | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 2 |  | 7 | 9 | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 0 |  |  | 1 | 8 | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 |  |  | 1 | 4 | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 |  |  | 1 | 2 | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | 0 |  |  | 0 | 0 | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| Count Total | 0 | 4 |  |  | 27 | 63 | 0 | 0 |  |  | 0 | 1 | 0 |  | 0 | 0 | 0 | 0 |
| Peak Hr | 0 | 4 |  |  | 24 | 49 | 0 | 0 |  |  | 0 | 1 | 0 |  | 0 | 0 | 0 | 0 |




Note: Two-hour count summary volumes include heavy vehicles but exclude bicycles in overall count.

| Interval Start | Heavy Vehicle Totals |  |  |  |  | Bicycles |  |  |  |  | Pedestrians (Crossing Leg) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EB | WB | NB | SB | Total | EB | WB | NB | SB | Total | East | West | North | South | Total |
| 7:00 AM | 6 | 5 | 0 | 3 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 1 | 8 | 0 | 7 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 |
| 7:30 AM | 2 | 5 | 0 | 5 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | 6 | 8 | 2 | 4 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 5 | 12 | 0 | 7 | 24 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 4 |
| 8:15 AM | 6 | 7 | 0 | 5 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 |
| 8:30 AM | 7 | 11 | 0 | 2 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 AM | 6 | 6 | 0 | 8 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 |
| Count Total | 39 | 62 | 2 | 41 | 144 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 2 | 2 | 9 |
| Peak Hour | 14 | 33 | 2 | 23 | 72 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 2 | 5 |




| $\stackrel{267}{\stackrel{267}{\leftarrow}}$ | N |  |  |  | R 3 FAIR <br> ak <br> : 1, <br> : 0 <br> N | H <br> our <br> - <br> 0 <br> 43 <br> 3 | Y $\qquad$ |  |  | $\xrightarrow[0]{1}$ | $\begin{aligned} & \text { V \%: } \\ & \hline 3.5 \% \\ & 0.0 \% \\ & .8 \% \\ & \hline .8 \% \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { iro } \\ & \text { PHF } \\ & \hline 0.87 \\ & 0.25 \\ & 0.91 \\ & 0.83 \\ & 0.93 \\ & \hline \end{aligned}$ | Ho | $\begin{gathered} \text { Tue, Oc } \\ 4: 00 \mathrm{P} \\ 5: 00 \mathrm{P} \end{gathered}$ | $\begin{aligned} & \text { to } \\ & \text { to } \\ & > \\ & 0 \\ & \hline 1 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | 6:00 P |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Two-Hour Count Summaries |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Interval Start | OLD BEFAIR HWY |  |  |  | DRIVEWAY |  |  |  | SR 3 |  |  |  | SR 3 |  |  | $\begin{gathered} \text { 15-min } \\ \text { Total } \end{gathered}$ | Rolling One Hour |
|  | Eastbound |  |  |  | Westbound |  |  | RT | Northbound |  |  |  | Southbound |  |  |  |  |
| 4:00 PM | 0 | 2 | 0 | 94 | 0 | 0 | 0 | 0 | 0 | 49 | 107 | 0 | 0 | 160 | 6 | 418 | 0 |
| 4:15 PM | 0 | 0 | 0 | 71 | 0 | 0 | 0 | 1 | 0 | 62 | 108 | 0 | 0 | 82 | 1 | 325 | 0 |
| 4:30 PM | 0 | 2 | 0 | 96 | 0 | 0 | 0 | 2 | 0 | 65 | 124 | 0 | 0 | 122 | 0 | 412 | 0 |
| 4:45 PM | 0 | 2 | 0 | 104 | 0 | 0 | 0 | 2 | 0 | 61 | 91 | 0 | 0 | 158 | 4 | 424 | 1,579 |
| 5:00 PM | 0 | 1 | 0 | 92 | 0 | 0 | 0 | 0 | 0 | 55 | 87 | 0 | 0 | 115 | 3 | 353 | 1,514 |
| 5:15 PM | 0 | 0 | 0 | 105 | 0 | 0 | 0 | 0 | 0 | 66 | 82 | 0 | 0 | 160 | 0 | 413 | 1,602 |
| 5:30 PM | 0 | 1 | 0 | 92 | 0 | 0 | 0 | 0 | 0 | 72 | 98 | 0 | 0 | 176 | 5 | 444 | 1,634 |
| 5:45 PM | 0 | 1 | 0 | 75 | 0 | 0 | 0 | 1 | 0 | 57 | 100 | 0 | 0 | 190 | 9 | 433 | 1,643 |
| Count Total | 0 | 9 | 0 | 729 | 0 | 0 | 0 | 6 | 0 | 487 | 797 | 0 | 0 | 1,163 | 28 | 3,222 | 0 |
| Peak Hour | 0 | 3 | 0 | 364 | 0 | 0 | 0 | 1 | 0 | 250 | 367 | 0 | 0 | 641 | 17 | 1,643 | 0 |
| Note: Two-hour count summary volumes include heavy vehicles but exclude bicycles in overall count. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Interval Start | Heavy Vehicle Totals |  |  |  |  |  | Bicycles |  |  |  |  |  | Pedestrians (Crossing Leg) |  |  |  |  |
|  | EB | WB |  | NB | SB | Total | EB | WB |  |  | SB | Total | East | West | North | Sou | h Total |
| 4:00 PM | 5 | 0 |  | 8 | 1 | 14 | 0 | 0 |  |  | 0 | 0 | 1 | 0 | 0 | 0 | 1 |
| 4:15 PM | 3 | 1 |  | 10 | 1 | 15 | 0 | 0 |  |  | 0 | 0 | 3 | 0 | 0 | 0 | 3 |
| 4:30 PM | 7 | 1 |  | 5 | 4 | 17 | 0 | 0 |  |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 9 | 1 |  | 6 | 5 | 21 | 0 | 0 |  |  | 0 | 0 | 2 | 2 | 0 | 0 | 4 |
| 5:00 PM | 4 | 0 |  | 1 | 4 | 9 | 0 | 0 |  |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 3 | 0 |  | 3 | 2 | 8 | 0 | 0 |  |  | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| 5:30 PM | 5 | 0 |  | 3 | 5 | 13 | 0 | 0 |  |  | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| 5:45 PM | 1 | 1 |  | 4 | 1 | 7 | 0 | 0 |  |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Count Total | 37 | 4 |  | 40 | 23 | 104 | 0 | 0 |  |  | 0 | 0 | 6 | 4 | 0 | 0 | 10 |
| Peak Hour | 13 | 1 |  | 11 | 12 | 37 | 0 | 0 |  |  | 0 | 0 | 0 | 2 | 0 | 0 | 2 |


|  |  | $\begin{aligned} & \infty \\ & \sim \\ & \infty \end{aligned}$ <br> 0 <br> 38 <br> 72 <br> 106 |  |  | R 3 <br> 10 <br> ak H <br> $\uparrow$ <br> : 1,3 <br> 0. | ur <br> N <br> 63 <br> 4 <br> $\begin{array}{r}1 \\ \stackrel{4}{4} \\ \hline\end{array}$ <br> ก |  |  |  | EB <br> WB <br> NB <br> SB <br> OTAL | $\begin{gathered} \frac{H V}{4.2 \%} \\ - \\ 3.0 \% \\ 6.9 \% \\ 4.8 \% \end{gathered}$ | unt |  |  |  | $\begin{aligned} & y \text { 01, } \\ & 1 \text { to } \\ & 1 \text { to } \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & \text { 0 } \end{aligned}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Two-Hour Count Summaries |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Interval Start | SR 106 |  |  |  | 0 |  |  |  | SR 3 |  |  |  | SR 3 |  |  |  | $\begin{gathered} \text { 15-min } \\ \text { Total } \end{gathered}$ | Rolling One Hour |
|  | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  |  |  |
| 7:00 AM | 0 | 52 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 3 | 104 | 0 | 0 | 0 | 61 | 20 | 246 | 0 |
| 7:15 AM | 0 | 64 | 0 | 21 | 0 | 0 | 0 | 0 | 0 | 1 | 112 | 0 | 0 | 0 | 89 | 25 | 312 | 0 |
| 7:30 AM | 0 | 70 | 0 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 132 | 0 | 0 | 0 | 147 | 26 | 407 | 0 |
| 7:45 AM |  | 64 | 0 | 16 | 0 | 0 | 0 | 0 | 0 | 1 | 140 | 0 | 0 | 0 | 127 | 32 | 380 | 1,345 |
| 8:00 AM | 0 | 40 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 12 | 130 | 0 | 0 | 0 | 59 | 20 | 264 | 1,363 |
| 8:15 AM | 0 | 51 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 1 | 132 | 0 | 0 | 0 | 60 | 26 | 277 | 1,328 |
| 8:30 AM | 0 | 58 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 6 | 122 | 0 | 0 | 0 | 69 | 30 | 292 | 1,213 |
| 8:45 AM | 0 | 75 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 5 | 118 | 0 | 0 | 0 | 58 | 28 | 289 | 1,122 |
| Count Total | 0 | 474 | 0 | 97 | 0 | 0 | 0 | 0 | 0 | 29 | 990 | 0 | 0 | 0 | 670 | 207 | 2,467 | 0 |
| Peak Hour | 0 | 238 | 0 | 72 | 0 | 0 | 0 | 0 | 0 | 14 | 514 | 0 | 0 | 0 | 422 | 103 | 1,363 | 0 |
| Note: Two-hour count summary volumes include heavy vehicles but exclude bicycles in overall count. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Interval Start | Heavy Vehicle Totals |  |  |  |  |  | Bicycles |  |  |  |  |  | Pedestrians (Crossing Leg) |  |  |  |  |  |
|  | EB | WB | N |  | SB | Total | EB | WB |  | NB | SB | Total | East |  | West | North | Sout | h Total |
| 7:00 AM | 1 | 0 | 1 |  | 5 | 16 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 7:15 AM | 2 | 0 | 2 |  | 6 | 10 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 7:30 AM | 8 | 0 | 3 |  | 22 | 33 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 7:45 AM | 1 | 0 |  |  | 4 | 9 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 8:00 AM | 2 | 0 |  |  | 4 | 13 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 8:15 AM | 1 | 0 |  |  | 13 | 21 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 8:30 AM | 2 | 0 |  |  | 6 | 21 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 8:45 AM | 0 | 0 |  |  | 5 | 11 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| Count Total | 17 | 0 |  |  | 65 | 134 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| Peak Hr | 13 | 0 |  |  | 36 | 65 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |


| $\stackrel{375}{\stackrel{381}{\longleftarrow}}$ |  |  |  |  | ak |  |  |  |  | $\begin{aligned} & \mathrm{EB} \\ & \mathrm{VB} \\ & \mathrm{NB} \\ & \mathrm{SB} \\ & \mathrm{TAL} \end{aligned}$ | HV \%: <br> 2.8\% <br> 1.7\% <br> 2.8\% <br> 2.5\% | unt Pea <br> oío <br> PHF <br> 0.82 <br> 0.85 <br> 0.95 <br> 0.97 | Dat eriod Hou |  | ue, Oc <br> :00 P <br> 5:00 P | 17, <br> to <br> to | 017 <br> 6:00 P <br> 6:00 P |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Two-Hour Count Summaries |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Interval Start | SR 106 |  |  |  | 0 |  |  |  | SR 3 |  |  |  | SR 3 |  |  |  | $\begin{gathered} \text { 15-min } \\ \text { Total } \end{gathered}$ | Rolling One Hour |
|  | UT | Eastb | Tund | RT | Westbound |  |  | RT | Northbound |  |  |  | Southbound |  |  |  |  |  |
| 4:00 PM | 0 | 31 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 7 | 84 | 0 | 0 | 0 | 135 | 64 | 323 | 0 |
| 4:15 PM |  | 38 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 9 | 113 | 0 | 0 | 0 | 172 | 74 | 410 | 0 |
| 4:30 PM |  | 38 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 15 | 111 | 0 | 0 | 0 | 186 | 79 | 436 | 0 |
| 4:45 PM | 0 | 40 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 9 | 81 | 0 | 0 | 0 | 186 | 76 | 400 | 1,569 |
| 5:00 PM | 0 | 30 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 10 | 83 | 0 | 0 | 0 | 170 | 87 | 387 | 1,633 |
| 5:15 PM | 0 | 40 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 19 | 80 | 0 | 0 | 0 | 181 | 86 | 418 | 1,641 |
| 5:30 PM | 0 | 46 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 12 | 110 | 0 | 0 | 0 | 170 | 79 | 426 | 1,631 |
| 5:45 PM | 0 | 29 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 9 | 93 | 0 | 0 | 0 | 203 | 73 | 415 | 1,646 |
| Count Total | 0 | 292 | 0 | 57 | 0 | 0 | 0 | 0 | 0 | 90 | 755 | 0 | 0 | 0 | 1,403 | 618 | 3,215 | 0 |
| Peak Hour | 0 | 145 | 0 | 36 | 0 | 0 | 0 | 0 | 0 | 50 | 366 | 0 | 0 | 0 | 724 | 325 | 1,646 | 0 |
| Note: Two-hour count summary volumes include heavy vehicles but exclude bicycles in overall count. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Interval Start | Heavy Vehicle Totals |  |  |  |  |  | Bicycles |  |  |  |  |  | Pedestrians (Crossing Leg) |  |  |  |  |  |
|  | EB | WB | N |  | SB | Total | EB | WB |  | B | SB | Total | East |  | West | North | Sou | h Total |
| 4:00 PM | 2 | 0 | 2 |  | 13 | 17 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 4:15 PM | 2 | 0 | 1 |  | 5 | 18 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 4:30 PM | 1 | 0 |  |  | 8 | 11 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 4:45 PM | 4 | 0 |  |  | 10 | 16 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 5:00 PM | 2 | 0 |  |  | 11 | 14 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 |  |  | 4 | 7 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 5:30 PM | 1 | 0 |  |  | 9 | 11 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 1 | 0 | 0 | 1 |
| 5:45 PM | 2 | 0 |  |  | 5 | 9 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| Count Total | 14 | 0 |  |  | 65 | 103 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 1 | 0 | 0 | 1 |
| Peak Hr | 5 | 0 |  |  | 29 | 41 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 1 | 0 | 0 | 1 |


|  |  |  |  |  | ak <br> S <br> $\rightarrow$ <br> V: <br> F: | 2 <br> our <br> $\underset{7}{7}$ <br> נ <br> 8 <br> 84 <br> $\stackrel{\infty}{8}$ |  | SR 3 <br> 85 <br> 9 <br> 0 |  |  | HV \%: <br> 4.3\% <br> 2.6\% <br> 4.9\% <br> 3.6\% |  | Da erio Ho |  |  | y 01 <br> to <br> to <br> ( | $\begin{aligned} & 2019 \\ & 9: 00 \text { A } \\ & 8: 15 \text { A } \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Two-Hour Count Summaries |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Interval Start | 0 |  |  |  | SR 302 |  |  |  | SR 3 |  |  |  | SR 3 |  |  |  | $\begin{gathered} \text { 15-min } \\ \text { Total } \end{gathered}$ | Rolling One Hour |
|  | Eastbound |  |  |  | UT | Westbound |  | RT | Northbound |  |  |  | Southbound |  |  |  |  |  |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 15 | 0 | 0 | 92 | 3 | 0 | 4 | 49 | 0 | 164 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 19 | 0 | 0 | 105 | 4 | 0 | 12 | 52 | 0 | 194 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 22 | 0 | 0 | 122 | 8 | 0 | 24 | 65 | 0 | 243 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 31 | 0 | 0 | 109 | 11 | 0 | 44 | 60 | 0 | 260 | 861 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 0 | 0 | 98 | 1 | 0 | 11 | 58 | 0 | 181 | 878 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 11 | 0 | 0 | 103 | 1 | 0 | 6 | 49 | 0 | 171 | 855 |
| 8:30 AM |  | 0 | 0 | 0 |  | 0 | 0 | 18 |  | 0 | 100 | 1 |  | 13 | 61 | 0 | 193 | 805 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 13 | 0 | 0 | 98 | 0 | 0 | 8 | 43 | 0 | 166 | 711 |
| Count Total | 0 | 0 | 0 | 0 | 0 | 15 | 0 | 142 | 0 | 0 | 827 | 29 | 0 | 122 | 437 | 0 | 1,572 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 85 | 0 | 0 | 434 | 24 | 0 | 91 | 235 | 0 | 878 | 0 |
| Note: Two-hour count summary volumes include heavy vehicles but exclude bicycles in overall count. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Interval Start | Heavy Vehicle Totals |  |  |  |  |  | Bicycles |  |  |  |  |  | Pedestrians (Crossing Leg) |  |  |  |  |  |
|  | EB | WB |  | NB | SB | Total | EB | WB |  |  | SB | Total | East |  | West | North | Sou | h Total |
| 7:00 AM | 0 | 1 |  | 2 | 7 | 10 | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 1 |  | 3 | 2 | 6 | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 3 |  | 4 | 3 | 10 | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 0 |  | 4 | 6 | 10 | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 |  | 1 | 5 | 6 | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 8:15 AM | 0 | 0 |  | 4 | 10 | 14 | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 8:30 AM | 0 | 0 |  | 7 | 7 | 14 | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 8:45 AM | 0 | 0 |  | 2 | 5 | 7 | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| Count Total | 0 | 5 |  | 27 | 45 | 77 | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| Peak Hr | 0 | 4 |  | 12 | 16 | 32 | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |



# Appendix B 

Traffic Operations
Modeling Output

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.2 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | 1 | $\mathbf{7}$ | $\mathbf{F}$ |  | - | 4 |
| Traffic Vol, veh/h | 95 | 45 | 780 | 100 | 10 | 400 |
| Future Vol, veh/h | 95 | 45 | 780 | 100 | 10 | 400 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 275 | 0 | - | - | 300 | - |
| Veh in Median Storage, $\#$ | 1 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 94 | 94 | 94 | 94 | 94 | 94 |
| Heavy Vehicles, \% | 2 | 2 | 4 | 4 | 6 | 6 |
| Mvmt Flow | 101 | 48 | 830 | 106 | 11 | 426 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.7 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | $\mathbf{1}$ | $\mathbf{7}$ | 1 | 4 | 个 | $\mathbf{7}$ |
| Traffic Vol, veh/h | 35 | 15 | 5 | 775 | 355 | 5 |
| Future Vol, veh/h | 35 | 15 | 5 | 775 | 355 | 5 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | Free |
| Storage Length | 150 | 0 | 200 | - | - | 475 |
| Veh in Median Storage, $\#$ | 1 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 9 | 9 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 35 | 15 | 5 | 775 | 355 | 5 |


HCM LOS C

| Minor Lane/Major Mvmt | NBL | NBT EBLn1 EBLn2 | SBT |  |
| :--- | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 1204 | -332 | 673 | - |
| HCM Lane V/C Ratio | 0.004 | -0.105 | 0.022 | - |
| HCM Control Delay (s) | 8 | -17.1 | 10.5 | - |
| HCM Lane LOS | A | - | C | B |
| HCM 95th \%tile Q(veh) | 0 | - | 0.3 | 0.1 |
| (ven | - |  |  |  |

Timings
3: SR 3 \& NE Clifton Lane/Rite Aid Driveway


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 4.3 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | 1 | $\mathbf{7}$ |  | $\mathbf{1}$ | $\mathbf{F}$ |  |
| Traffic Vol, veh/h | 10 | 245 | 185 | 545 | 355 | 15 |
| Future Vol, veh/h | 10 | 245 | 185 | 545 | 355 | 15 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 300 | 0 | 100 | - | - | - |
| Veh in Median Storage, $\#$ | 1 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 88 | 88 | 88 | 88 | 88 | 88 |
| Heavy Vehicles, \% | 9 | 9 | 3 | 3 | 7 | 7 |
| Mvmt Flow | 11 | 278 | 210 | 619 | 403 | 17 |



Timings
5: SR 3 \& SR 106

|  | 4 |  | 4 | $\dagger$ | $\frac{1}{1}$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ${ }^{1}$ | 「 | ${ }^{7}$ | 4 | 4 | 「 |
| Traffic Volume (vph) | 240 | 70 | 15 | 515 | 420 | 105 |
| Future Volume (vph) | 240 | 70 | 15 | 515 | 420 | 105 |
| Turn Type | Prot | Perm | Prot | NA | NA | pm+ov |
| Protected Phases | 4 |  | 5 | 2 | 6 | 4 |
| Permitted Phases |  | 4 |  |  |  | 6 |
| Detector Phase | 4 | 4 | 5 | 2 | 6 | 4 |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial (s) | 10.0 | 10.0 | 6.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split (s) | 27.7 | 27.7 | 11.7 | 22.5 | 40.7 | 27.7 |
| Total Split (s) | 50.0 | 50.0 | 40.0 | 50.0 | 50.0 | 50.0 |
| Total Split (\%) | 35.7\% | 35.7\% | 28.6\% | 35.7\% | 35.7\% | 35.7\% |
| Yellow Time (s) | 3.9 | 3.9 | 4.7 | 4.7 | 4.7 | 3.9 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.9 | 4.9 | 5.7 | 5.7 | 5.7 | 4.9 |
| Lead/Lag |  |  | Lead |  | Lag |  |
| Lead-Lag Optimize? |  |  | Yes |  | Yes |  |
| Recall Mode | None | None | None | Min | Min | None |
| Act Effct Green (s) | 19.1 | 19.1 | 7.1 | 34.5 | 30.7 | 60.0 |
| Actuated g/C Ratio | 0.29 | 0.29 | 0.11 | 0.53 | 0.47 | 0.92 |
| v/c Ratio | 0.60 | 0.17 | 0.10 | 0.66 | 0.63 | 0.09 |
| Control Delay | 29.0 | 7.2 | 37.6 | 15.0 | 19.5 | 0.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 29.0 | 7.2 | 37.6 | 15.0 | 19.5 | 0.6 |
| LOS | C | A | D | B | B | A |
| Approach Delay | 24.1 |  |  | 15.6 | 15.7 |  |
| Approach LOS | C |  |  | B | B |  |

## Intersection Summary

Cycle Length: 140
Actuated Cycle Length: 65.3
Natural Cycle: 85
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.66
Intersection Signal Delay: 17.6
Intersection LOS: B
Intersection Capacity Utilization 51.5\% ICU Level of Service A
Analysis Period (min) 15
Splits and Phases: 5: SR 3 \& SR 106


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.5 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | $\mathbf{Y}$ |  | 1 |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 10 | 85 | 435 | 25 | 90 | 235 |
| Future Vol, veh/h | 10 | 85 | 435 | 25 | 90 | 235 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 84 | 84 | 84 | 84 | 84 | 84 |
| Heavy Vehicles, \% | 4 | 4 | 3 | 3 | 5 | 5 |
| Mvmt Flow | 12 | 101 | 518 | 30 | 107 | 280 |


| Major/Minor M | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1027 | 533 | 0 | 0 | 548 | 0 |
| Stage 1 | 533 | - | - | - | - | - |
| Stage 2 | 494 | - | - | - | - | - |
| Critical Hdwy | 6.44 | 6.24 | - | - | 4.15 | - |
| Critical Hdwy Stg 1 | 5.44 |  | - | - | - | - |
| Critical Hdwy Stg 2 | 5.44 | - | - | - | - | - |
| Follow-up Hdwy | 3.536 | 3.336 | - | - | 2.245 | - |
| Pot Cap-1 Maneuver | 257 | 543 | - | - | 1007 | - |
| Stage 1 | 584 | - | - | - | - | - |
| Stage 2 | 609 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 225 | 543 | - | - | 1007 | - |
| Mov Cap-2 Maneuver | 225 | - | - | - | - | - |
| Stage 1 | 510 | - | - | - | - | - |
| Stage 2 | 609 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |
| HCM Control Delay, s | 15 |  | 0 |  | 2.5 |  |
| HCM LOS | C |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT | NBRWBLn1 |  | SBL | SBT |
| Capacity (veh/h) |  | - | - | 473 | 1007 | - |
| HCM Lane V/C Ratio |  | - | - | 0.239 | 0.106 | - |
| HCM Control Delay (s) |  | - | - | 15 | 9 | 0 |
| HCM Lane LOS |  | - | - | C | A | A |
| HCM 95th \%tile Q(veh) |  | - | - | 0.9 | 0.4 | - |

## Arterial Level of Service: NB SR 3

| Cross Street | Arterial Class | $\begin{array}{r} \text { Flow } \\ \text { Speed } \end{array}$ | Running Time | Signal Delay | $\begin{array}{r} \text { Travel } \\ \text { Time (s) } \\ \hline \end{array}$ | $\begin{aligned} & \text { Dist } \\ & \text { (mi) } \end{aligned}$ | Arterial Speed | Arterial LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SR 106 | II | 49 | 119.7 | 15.0 | 134.7 | 1.64 | 43.7 | A |
| Rite Aid Driveway | II | 35 | 166.6 | 14.4 | 181.0 | 1.64 | 32.6 | B |
| Total | II |  | 286.3 | 29.4 | 315.7 | 3.27 | 37.3 | A |

Arterial Level of Service: SB SR 3

|  | Arterial <br> Class | Flow <br> Speed | Running <br> Time | Signal <br> Delay | Travel <br> Time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed | Arterial <br> LOS |
| :--- | :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Cross Street | II Clifton Lane | 43 | 203.8 | 43.1 | 246.9 | 2.46 | 35.8 | A |
| SR 106 | II | 35 | 168.2 | 19.5 | 187.7 | 1.64 | 31.4 | B |
| Total | II |  | 372.0 | 62.6 | 434.6 | 4.10 | 33.9 | B |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.9 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | 1 | $\mathbf{7}$ | $\mathbf{F}$ |  | 1 | 4 |
| Traffic Vol, veh/h | 70 | 20 | 560 | 135 | 55 | 610 |
| Future Vol, veh/h | 70 | 20 | 560 | 135 | 55 | 610 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 275 | 0 | - | - | 300 | - |
| Veh in Median Storage, $\#$ | 1 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 89 | 89 | 89 | 89 | 89 | 89 |
| Heavy Vehicles, \% | 4 | 4 | 3 | 3 | 4 | 4 |
| Mvmt Flow | 79 | 22 | 629 | 152 | 62 | 685 |




| Major/Minor | Minor2 | Major1 |  | Major2 |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Conflicting Flow All | 1217 | 686 | 686 | 0 | - |
| $\quad$ Stage 1 | 686 | - | - | - | - |
| $\quad$ Stage 2 | 531 | - | - | - |  |
| Critical Hdwy | 6.49 | 6.29 | 4.11 | - | - |

HCM LOS B

| Minor Lane/Major Mvmt | NBL | NBT EBLn1 EBLn2 | SBT |  |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 912 | -326 | 436 | - |  |
| HCM Lane V/C Ratio | 0.006 | -0.032 | 0.059 | - |  |
| HCM Control Delay (s) | 9 | -16.4 | 13.8 | - |  |
| HCM Lane LOS | A | - | C | B | - |
| HCM 95th \%tile Q(veh) | 0 | - | 0.1 | 0.2 | - |

Timings
3: SR 3 \& NE Clifton Lane/Rite Aid Driveway


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 13.7 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | i | $\mathbf{7}$ |  | $\mathbf{4}$ | $\mathbf{F}$ |  |
| Traffic Vol, veh/h | 5 | 365 | 250 | 365 | 640 | 15 |
| Future Vol, veh/h | 5 | 365 | 250 | 365 | 640 | 15 |
| Conflicting Peds, \#/hr | 2 | 2 | 2 | 0 | 0 | 2 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 300 | 0 | 100 | - | - | - |
| Veh in Median Storage, $\#$ | 1 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 93 | 93 | 93 | 93 | 93 | 93 |
| Heavy Vehicles, \% | 4 | 4 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 5 | 392 | 269 | 392 | 688 | 16 |


| Major/Minor | Minor2 | Major1 |  |  | Major2 |  |
| :--- | ---: | ---: | ---: | :--- | :--- | :--- |
| Conflicting Flow All | 1630 | 700 | 706 | 0 | - | 0 |
| $\quad$ Stage 1 | 698 | - | - | - | - | - |
| Stage 2 | 932 | - | - | - | - | - |
| Critical Hdwy | 6.44 | 6.24 | 4.12 | - | - | - |
| Critical Hdwy Stg 1 | 5.44 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.44 | - | - | - | - | - |
| Follow-up Hdwy | 3.536 | 3.336 | 2.218 | - | - | - |
| Pot Cap-1 Maneuver | 111 | 436 | 892 | - | - | - |
| $\quad$ Stage 1 | 490 | - | - | - | - | - |
| Stage 2 | 380 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 77 | 434 | 890 | - | - | - |
| Mov Cap-2 Maneuver | 97 | - | - | - | - | - |
| Stage 1 | 342 | - | - | - | - | - |
| Stage 2 | 379 | - | - | - | - | - |
|  |  |  |  |  |  |  |


| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 53.6 | 4.4 | 0 |


| Minor Lane/Major Mvmt | NBL | NBT EBLn1 EBLn2 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 890 | - | 97 | 434 | - |

Timings
5: SR 3 \& SR 106

|  | 4 |  | 4 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 「 | ${ }^{*}$ | $\uparrow$ | 4 | 「 |
| Traffic Volume (vph) | 145 | 35 | 50 | 365 | 725 | 325 |
| Future Volume (vph) | 145 | 35 | 50 | 365 | 725 | 325 |
| Turn Type | Prot | Perm | Prot | NA | NA | $\mathrm{pm}+\mathrm{ov}$ |
| Protected Phases | 4 |  | 5 | 2 | 6 | 4 |
| Permitted Phases |  | 4 |  |  |  | 6 |
| Detector Phase | 4 | 4 | 5 | 2 | 6 | 4 |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial (s) | 10.0 | 10.0 | 6.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split (s) | 27.7 | 27.7 | 11.7 | 22.5 | 40.7 | 27.7 |
| Total Split (s) | 50.0 | 50.0 | 40.0 | 50.0 | 30.0 | 50.0 |
| Total Split (\%) | 41.7\% | 41.7\% | 33.3\% | 41.7\% | 25.0\% | 41.7\% |
| Yellow Time (s) | 3.9 | 3.9 | 4.7 | 4.7 | 4.7 | 3.9 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.9 | 4.9 | 5.7 | 5.7 | 5.7 | 4.9 |
| Lead/Lag |  |  | Lead |  | Lag |  |
| Lead-Lag Optimize? |  |  | Yes |  | Yes |  |
| Recall Mode | None | None | None | Min | Min | None |
| Act Effct Green (s) | 11.5 | 11.5 | 7.3 | 32.3 | 24.9 | 37.2 |
| Actuated g/C Ratio | 0.21 | 0.21 | 0.13 | 0.59 | 0.46 | 0.68 |
| v/c Ratio | 0.43 | 0.11 | 0.23 | 0.36 | 0.94 | 0.30 |
| Control Delay | 24.9 | 8.8 | 26.5 | 6.9 | 41.0 | 1.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 24.9 | 8.8 | 26.5 | 6.9 | 41.0 | 1.3 |
| LOS | C | A | C | A | D | A |
| Approach Delay | 21.8 |  |  | 9.3 | 28.7 |  |
| Approach LOS | C |  |  | A | C |  |
| Intersection Summary |  |  |  |  |  |  |
| Cycle Length: 120 |  |  |  |  |  |  |
| Actuated Cycle Length: 54.6 |  |  |  |  |  |  |
| Natural Cycle: 85 |  |  |  |  |  |  |
| Control Type: Actuated-Uncoordinated |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.94 |  |  |  |  |  |  |
| Intersection Signal Delay: 23.0 |  |  |  | Intersection LOS: C |  |  |
| Intersection Capacity Utilization 61.2\% |  |  |  | ICU Level of Service B |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |
| Splits and Phases: 5: SR 3 \& SR 106 |  |  |  |  |  |  |
| 402 |  |  |  |  |  | $1^{4} 04$ |
| 50 s |  |  |  |  |  | 50 s |
| 405 |  |  | $\dagger \square 6$ |  |  |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.3 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | $\mathbf{Y}$ |  | 1 |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 10 | 130 | 335 | 15 | 110 | 575 |
| Future Vol, veh/h | 10 | 130 | 335 | 15 | 110 | 575 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 2 | 2 | 4 | 4 | 2 | 2 |
| Mvmt Flow | 10 | 130 | 335 | 15 | 110 | 575 |


| Major/Minor | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1138 | 343 | 0 | 0 | 350 | 0 |
| Stage 1 | 343 | - | - | - | - | - |
| Stage 2 | 795 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |
| Critical Hdwy Stg 1 | 5.42 |  | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.218 | - |
| Pot Cap-1 Maneuver | 223 | 700 | - | - | 1209 | - |
| Stage 1 | 719 | - | - | - | - | - |
| Stage 2 | 445 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 193 | 700 | - | - | 1209 | - |
| Mov Cap-2 Maneuver | 193 | - | - | - | - | - |
| Stage 1 | 623 | - | - | - | - | - |
| Stage 2 | 445 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |
| HCM Control Delay, s | S 13 |  | 0 |  | 1.3 |  |
| HCM LOS | B |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT | NBRWBLn1 |  | SBL | SBT |
| Capacity (veh/h) |  | - | - | 589 | 1209 | - |
| HCM Lane V/C Ratio |  | - |  | 0.238 | 0.091 | - |
| HCM Control Delay (s) |  | - | - | 13 | 8.3 | 0 |
| HCM Lane LOS |  | - | - | B | A | A |
| HCM 95th \%tile Q(veh) |  | - | - | 0.9 | 0.3 | - |

## Arterial Level of Service: NB SR 3

|  | Arterial <br> Class | Flow <br> Speed | Running <br> Time | Signal <br> Delay | Travel <br> Time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed | Arterial <br> LOS |
| :--- | :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Cross Street | II | 49 | 119.7 | 6.9 | 126.6 | 1.64 | 46.5 | A |
| SR 106 | II | 35 | 166.6 | 8.9 | 175.5 | 1.64 | 33.6 | B |
| Tite Aid Driveway | II | II |  | 286.3 | 15.8 | 302.1 | 3.27 | 39.0 |
| A |  |  |  |  |  |  |  |  |

Arterial Level of Service: SB SR 3

|  | Arterial <br> Class | Flow <br> Speed | Running <br> Time | Signal <br> Delay | Travel <br> Time $(s)$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed | Arterial <br> LOS |
| :--- | :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Cross Street | II | 43 | 203.8 | 163.9 | 367.7 | 2.46 | 24.1 | C |
| NE Clifton Lane | II | 35 | 168.2 | 41.0 | 209.2 | 1.64 | 28.2 | B |
| SR 106 | II |  | 372.0 | 204.9 | 576.9 | 4.10 | 25.6 | C |

MOVEMENT SUMMARY
Site: 200 [SR 3/SR 302-2025 AM Build - West RAB]
的审 Network: N101 [SR 3/SR 302
2025 AM Build]
Build - Opening Year
2025 AM Peak Hour
Double RAB
Site Category: -
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | Demand Flows Arrival Flows Total HV Total HV |  |  |  | Deg. <br> Satn <br> v/c | Average Delay sec | Level of Service | Aver. Back of Queue Prop. Vehicles Distance Queued$\qquad$ veh ft |  |  | Effective Aver. No.Average Stop Cycles Speed Rate |  |  |
|  | veh/h |  | veh/h | \% |  |  |  |  |  |  |  |  | mph |
| South: SR 3 Les |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 226 | 3.0 | 226 | 3.0 | 0.548 | 4.9 | LOS A | 1.8 | 44.9 | 0.41 | 0.49 | 0.41 | 36.6 |
| 18 R2 | 417 | 3.0 | 417 | 3.0 | 0.548 | 4.9 | LOS A | 1.8 | 44.9 | 0.41 | 0.49 | 0.41 | 33.0 |
| Approach | 643 | 3.0 | 643 | 3.0 | 0.548 | 4.9 | LOS A | 1.8 | 44.9 | 0.41 | 0.49 | 0.41 | 34.8 |
| East: SR 302 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 186 | 4.0 | 186 | 4.0 | 0.270 | 10.9 | LOS B | 0.6 | 15.4 | 0.44 | 0.65 | 0.44 | 32.6 |
| 16 R2 | 96 | 4.0 | 96 | 4.0 | 0.270 | 5.3 | LOS A | 0.6 | 15.4 | 0.44 | 0.65 | 0.44 | 31.4 |
| Approach | 282 | 4.0 | 282 | 4.0 | 0.270 | 9.0 | LOS A | 0.6 | 15.4 | 0.44 | 0.65 | 0.44 | 32.2 |
| North: SR 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $7 \quad$ L2 | 95 | 5.0 | 95 | 5.0 | 0.241 | 10.7 | LOS B | 0.5 | 13.5 | 0.40 | 0.58 | 0.40 | 31.5 |
| 4 T1 | 161 | 5.0 | 161 | 5.0 | 0.241 | 5.1 | LOS A | 0.5 | 13.5 | 0.40 | 0.58 | 0.40 | 35.5 |
| Approach | 256 | 5.0 | 256 | 5.0 | 0.241 | 7.2 | LOS A | 0.5 | 13.5 | 0.40 | 0.58 | 0.40 | 34.5 |
| All Vehicles | 1181 | 3.7 | 1181 | 3.7 | 0.548 | 6.4 | LOS A | 1.8 | 44.9 | 0.42 | 0.55 | 0.42 | 34.1 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Network Data dialog (Network tab). Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

SIDRA INTERSECTION 8.0 | Copyright © 2000-2019 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: PARAMETRIX | Processed: Wednesday, September 4, 2019 2:24:46 PM
Project: U:IPSOIProjectsIClients11631-WSDOT1234-1631-130 SR3FreightCorr TOAAIO2WBSI07_OperationsAnalysis\SR3_RBTs_v3.sip8

Build - Opening Year
2025 AM Peak Hour
Double RAB
Site Category: -
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Demand Total veh/h | Flows HV \% | Arrival FlowsTotal HV |  | Deg. Satn v/c | Average Delay sec | Level of Service | Aver. Back of Queue Prop. Vehicles Distance Queued |  |  | Effective Aver. No.Average Stop Cycles Speed |  |  |
| South: Bellwood Lane sec |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 1 | 3.0 | 1 | 3.0 | 0.006 | 12.2 | LOS B | 0.0 | 0.3 | 0.54 | 0.59 | 0.54 | 30.5 |
| 3 a | L1 | 1 | 3.0 | 1 | 3.0 | 0.006 | 11.0 | LOS B | 0.0 | 0.3 | 0.54 | 0.59 | 0.54 | 34.5 |
| 8 | T1 | 1 | 3.0 | 1 | 3.0 | 0.006 | 6.6 | LOS A | 0.0 | 0.3 | 0.54 | 0.59 | 0.54 | 34.8 |
| 18 | R2 | 1 | 3.0 | 1 | 3.0 | 0.006 | 6.6 | LOS A | 0.0 | 0.3 | 0.54 | 0.59 | 0.54 | 33.9 |
| Appro | ach | 5 | 3.0 | 5 | 3.0 | 0.006 | 9.1 | LOS A | 0.0 | 0.3 | 0.54 | 0.59 | 0.54 | 33.7 |
| East: SR 302 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 1 | 4.0 | 1 | 4.0 | 0.139 | 11.8 | LOS B | 0.3 | 7.0 | 0.50 | 0.60 | 0.50 | 36.1 |
| 6 | T1 | 89 | 4.0 | 89 | 4.0 | 0.139 | 6.2 | LOS A | 0.3 | 7.0 | 0.50 | 0.60 | 0.50 | 32.4 |
| 16a | R1 | 1 | 4.0 | 1 | 4.0 | 0.139 | 5.8 | LOS A | 0.3 | 7.0 | 0.50 | 0.60 | 0.50 | 35.8 |
| 16 | R2 | 36 | 4.0 | 36 | 4.0 | 0.139 | 6.1 | LOS A | 0.3 | 7.0 | 0.50 | 0.60 | 0.50 | 35.0 |
| Appro | ach | 127 | 4.0 | 127 | 4.0 | 0.139 | 6.2 | LOS A | 0.3 | 7.0 | 0.50 | 0.60 | 0.50 | 33.5 |
| North: SR 3 Bypass |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 24 | 5.0 | 24 | 5.0 | 0.189 | 10.2 | LOS B | 0.4 | 10.3 | 0.28 | 0.51 | 0.28 | 36.7 |
| 4 | T1 | 1 | 5.0 | 1 | 5.0 | 0.189 | 4.5 | LOS A | 0.4 | 10.3 | 0.28 | 0.51 | 0.28 | 36.7 |
| 14 | R2 | 190 | 5.0 | 190 | 5.0 | 0.189 | 4.5 | LOS A | 0.4 | 10.3 | 0.28 | 0.51 | 0.28 | 33.3 |
| 14b | R3 | 1 | 5.0 | 1 | 5.0 | 0.189 | 4.7 | LOS A | 0.4 | 10.3 | 0.28 | 0.51 | 0.28 | 35.2 |
| Appro | ach | 217 | 5.0 | 217 | 5.0 | 0.189 | 5.2 | LOS A | 0.4 | 10.3 | 0.28 | 0.51 | 0.28 | 33.9 |
| NorthWest: School Driveway |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7bx | L3 | 1 | 3.0 | 1 | 3.0 | 0.005 | 12.4 | LOS B | 0.0 | 0.2 | 0.45 | 0.55 | 0.45 | 35.6 |
| 7 ax | L1 | 1 | 3.0 | 1 | 3.0 | 0.005 | 10.0 | LOS B | 0.0 | 0.2 | 0.45 | 0.55 | 0.45 | 34.8 |
| 14ax | R1 | 1 | 3.0 | 1 | 3.0 | 0.005 | 5.2 | LOS A | 0.0 | 0.2 | 0.45 | 0.55 | 0.45 | 34.9 |
| 14bx | R3 | 1 | 3.0 | 1 | 3.0 | 0.005 | 5.7 | LOS A | 0.0 | 0.2 | 0.45 | 0.55 | 0.45 | 31.0 |
| Appro | ach | 5 | 3.0 | 5 | 3.0 | 0.005 | 8.3 | LOS A | 0.0 | 0.2 | 0.45 | 0.55 | 0.45 | 34.4 |
| West: SR 302 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5b | L3 | 1 | 4.0 | 1 | 4.0 | 0.426 | 11.1 | LOS B | 1.3 | 33.4 | 0.21 | 0.58 | 0.21 | 33.4 |
| 5 | L2 | 404 | 4.0 | 404 | 4.0 | 0.426 | 9.9 | LOS A | 1.3 | 33.4 | 0.21 | 0.58 | 0.21 | 32.9 |
| 2 | T1 | 118 | 4.0 | 118 | 4.0 | 0.426 | 4.3 | LOS A | 1.3 | 33.4 | 0.21 | 0.58 | 0.21 | 32.9 |
| 12 | R2 | 1 | 4.0 | 1 | 4.0 | 0.426 | 4.3 | LOS A | 1.3 | 33.4 | 0.21 | 0.58 | 0.21 | 31.6 |
| Approach |  | 524 | 4.0 | 524 | 4.0 | 0.426 | 8.7 | LOS A | 1.3 | 33.4 | 0.21 | 0.58 | 0.21 | 32.9 |
| All Ve | icles | 877 | 4.2 | 877 | 4.2 | 0.426 | 7.4 | LOS A | 1.3 | 33.4 | 0.27 | 0.56 | 0.27 | 33.2 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Network Data dialog (Network tab). Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

SIDRA INTERSECTION 8.0 | Copyright © 2000-2019 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: PARAMETRIX | Processed: Wednesday, September 4, 2019 2:24:46 PM
Project: U:IPSOIProjectsIClients11631-WSDOT\234-1631-130 SR3FreightCorr TOAAIO2WBSI07_OperationsAnalysisISR3_RBTs_v3.sip8

MOVEMENT SUMMARY
Site: 200 [SR 3/SR 302-2025 PM Build - West RAB]
嘾 Network: N101 [SR 3/ SR 302 2025 PM Build]
Build - Opening Year
2025 AM Peak Hour
Double RAB
Site Category: -
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | Demand Total | Flows HV | Arrival Total | Fows HV | Deg. Satn | Average Delay | Level of Service | Aver. Back Vehicles | k of Queue Distance | Prop. Queued | Effective Stop Rate | Aver. No.A Cycles | erage peed |
|  | veh/h |  | veh/h | \% | v/c | sec |  | veh | ft |  |  |  | mph |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 180 | 3.0 | 180 | 3.0 | 0.337 | 4.8 | LOS A | 0.9 | 22.2 | 0.39 | 0.50 | 0.39 | 36.6 |
| 18 R2 | 200 | 3.0 | 200 | 3.0 | 0.337 | 4.8 | LOS A | 0.9 | 22.2 | 0.39 | 0.50 | 0.39 | 33.1 |
| Approach | 380 | 3.0 | 380 | 3.0 | 0.337 | 4.8 | LOS A | 0.9 | 22.2 | 0.39 | 0.50 | 0.39 | 35.2 |
| East: SR 302 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 246 | 4.0 | 246 | 4.0 | 0.352 | 10.8 | LOS B | 0.8 | 21.7 | 0.43 | 0.64 | 0.43 | 32.7 |
| 16 R2 | 136 | 4.0 | 136 | 4.0 | 0.352 | 5.2 | LOS A | 0.8 | 21.7 | 0.43 | 0.64 | 0.43 | 31.4 |
| Approach | 382 | 4.0 | 382 | 4.0 | 0.352 | 8.8 | LOS A | 0.8 | 21.7 | 0.43 | 0.64 | 0.43 | 32.2 |
| North: SR 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 130 | 5.0 | 130 | 5.0 | 0.676 | 13.1 | LOS B | 2.7 | 71.0 | 0.72 | 0.73 | 0.79 | 30.5 |
| 4 T1 | 555 | 5.0 | 555 | 5.0 | 0.676 | 7.5 | LOS A | 2.7 | 71.0 | 0.72 | 0.73 | 0.79 | 34.8 |
| Approach | 685 | 5.0 | 685 | 5.0 | 0.676 | 8.5 | LOS A | 2.7 | 71.0 | 0.72 | 0.73 | 0.79 | 34.3 |
| All Vehicles | 1447 | 4.2 | 1447 | 4.2 | 0.676 | 7.6 | LOS A | 2.7 | 71.0 | 0.56 | 0.65 | 0.59 | 34.0 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Network Data dialog (Network tab). Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

SIDRA INTERSECTION 8.0 | Copyright © 2000-2019 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: PARAMETRIX | Processed: Wednesday, August 21, 2019 4:33:04 PM
Project: U:IPSOIProjectsIClients11631-WSDOT1234-1631-130 SR3FreightCorr TOAAIO2WBSI07_OperationsAnalysis\SR3_RBTs_v3.sip8

Build - Opening Year
2025 AM Peak Hour
Double RAB
Site Category: -
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \text { ID } \end{gathered}$ | Turn | Demand Total veh/h | Flows HV \% | Arriva Total veh/h | lows <br> HV <br> \% | Deg. <br> Satn <br> v/c | Average Delay sec | Level of Service | Aver. Back of Queue Prop. Vehicles Distance Queued |  |  | Effective Aver. No.Average Stop Cycles Speed |  |  |
| South: Bellwood Lane sec |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 1 | 3.0 | 1 | 3.0 | 0.005 | 11.5 | LOS B | 0.0 | 0.2 | 0.48 | 0.57 | 0.48 | 30.9 |
| 3 a | L1 | 1 | 3.0 | 1 | 3.0 | 0.005 | 10.4 | LOS B | 0.0 | 0.2 | 0.48 | 0.57 | 0.48 | 34.8 |
| 8 | T1 | 1 | 3.0 | 1 | 3.0 | 0.005 | 5.9 | LOS A | 0.0 | 0.2 | 0.48 | 0.57 | 0.48 | 35.1 |
| 18 | R2 | 1 | 3.0 | 1 | 3.0 | 0.005 | 5.9 | LOS A | 0.0 | 0.2 | 0.48 | 0.57 | 0.48 | 34.2 |
| Appro | ach | 5 | 3.0 | 5 | 3.0 | 0.005 | 8.4 | LOS A | 0.0 | 0.2 | 0.48 | 0.57 | 0.48 | 34.1 |
| East: SR 302 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 1 | 4.0 | 1 | 4.0 | 0.180 | 10.9 | LOS B | 0.4 | 9.1 | 0.40 | 0.52 | 0.40 | 36.4 |
| 6 | T1 | 155 | 4.0 | 155 | 4.0 | 0.180 | 5.3 | LOS A | 0.4 | 9.1 | 0.40 | 0.52 | 0.40 | 32.8 |
| 16a | R1 | 1 | 4.0 | 1 | 4.0 | 0.180 | 4.9 | LOS A | 0.4 | 9.1 | 0.40 | 0.52 | 0.40 | 36.1 |
| 16 | R2 | 30 | 4.0 | 30 | 4.0 | 0.180 | 5.3 | LOS A | 0.4 | 9.1 | 0.40 | 0.52 | 0.40 | 35.3 |
| Appro | ach | 187 | 4.0 | 187 | 4.0 | 0.180 | 5.3 | LOS A | 0.4 | 9.1 | 0.40 | 0.52 | 0.40 | 33.5 |
| North: SR 3 Bypass |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 42 | 5.0 | 42 | 5.0 | 0.315 | 10.7 | LOS B | 0.7 | 18.8 | 0.39 | 0.56 | 0.39 | 36.3 |
| 4 | T1 | 1 | 5.0 | 1 | 5.0 | 0.315 | 5.0 | LOS A | 0.7 | 18.8 | 0.39 | 0.56 | 0.39 | 36.4 |
| 14 | R2 | 298 | 5.0 | 298 | 5.0 | 0.315 | 5.0 | LOS A | 0.7 | 18.8 | 0.39 | 0.56 | 0.39 | 32.8 |
| 14b | R3 | 1 | 5.0 | 1 | 5.0 | 0.315 | 5.2 | LOS A | 0.7 | 18.8 | 0.39 | 0.56 | 0.39 | 34.9 |
| Appro | ach | 342 | 5.0 | 342 | 5.0 | 0.315 | 5.7 | LOS A | 0.7 | 18.8 | 0.39 | 0.56 | 0.39 | 33.5 |
| NorthWest: School Driveway |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 bx | L3 | 1 | 3.0 | 1 | 3.0 | 0.006 | 13.6 | LOS B | 0.0 | 0.3 | 0.57 | 0.59 | 0.57 | 35.0 |
| 7 ax | L1 | 1 | 3.0 | 1 | 3.0 | 0.006 | 11.2 | LOS B | 0.0 | 0.3 | 0.57 | 0.59 | 0.57 | 34.3 |
| 14ax | R1 | 1 | 3.0 | 1 | 3.0 | 0.006 | 6.4 | LOS A | 0.0 | 0.3 | 0.57 | 0.59 | 0.57 | 34.4 |
| 14bx | R3 | 1 | 3.0 | 1 | 3.0 | 0.006 | 6.9 | LOS A | 0.0 | 0.3 | 0.57 | 0.59 | 0.57 | 30.2 |
| Appro | ach | 5 | 3.0 | 5 | 3.0 | 0.006 | 9.5 | LOS A | 0.0 | 0.3 | 0.57 | 0.59 | 0.57 | 33.9 |
| West: SR 302 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5b | L3 | 1 | 4.0 | 1 | 4.0 | 0.326 | 11.2 | LOS B | 0.9 | 22.9 | 0.24 | 0.55 | 0.24 | 33.9 |
| 5 | L2 | 231 | 4.0 | 231 | 4.0 | 0.326 | 10.0 | LOS B | 0.9 | 22.9 | 0.24 | 0.55 | 0.24 | 33.4 |
| 2 | T1 | 160 | 4.0 | 160 | 4.0 | 0.326 | 4.4 | LOS A | 0.9 | 22.9 | 0.24 | 0.55 | 0.24 | 33.4 |
| 12 | R2 | 1 | 4.0 | 1 | 4.0 | 0.326 | 4.4 | LOS A | 0.9 | 22.9 | 0.24 | 0.55 | 0.24 | 32.1 |
| Approach |  | 393 | 4.0 | 393 | 4.0 | 0.326 | 7.7 | LOS A | 0.9 | 22.9 | 0.24 | 0.55 | 0.24 | 33.4 |
| All Ve | hicles | 931 | 4.4 | 931 | 4.4 | 0.326 | 6.5 | LOS A | 0.9 | 22.9 | 0.33 | 0.55 | 0.33 | 33.5 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Network Data dialog (Network tab). Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

SIDRA INTERSECTION 8.0 | Copyright © 2000-2019 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: PARAMETRIX | Processed: Wednesday, August 21, 2019 4:33:04 PM
Project: U:IPSOIProjectsIClients11631-WSDOT1234-1631-130 SR3FreightCorr TOAAIO2WBSI07_OperationsAnalysis\SR3_RBTs_v3.sip8

MOVEMENT SUMMARY
Site: 221 [SR 3/SR 302-2040 AM Three Connector Build -
West RAB]
堭卓 Network: N101 [SR3 3/SR 3022040 AM Build Three Connectors]
Build - Opening Year
2025 AM Peak Hour
Double RAB
Site Category: -
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID <br> South: SR 3 | Demand Flows Arrival Flows Total HV Total HV |  |  |  | Deg. Satn <br> v/c | Average Delay sec | Level of Service | Aver. Back of Queue Prop. Vehicles Distance Queued veh ft |  |  | Effective Aver. No.Average <br> Stop Cycles Speed Rate <br> mph |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 292 | 3.0 | 292 | 3.0 | 0.711 | 5.2 | LOS A | 3.1 | 80.1 | 0.59 | 0.54 | 0.59 | 36.1 |
| 18 R2 | 613 | 3.0 | 613 | 3.0 | 0.711 | 5.2 | LOS A | 3.1 | 80.1 | 0.59 | 0.54 | 0.59 | 32.2 |
| Approach | 905 | 3.0 | 905 | 3.0 | 0.711 | 5.2 | LOS A | 3.1 | 80.1 | 0.59 | 0.54 | 0.59 | 34.0 |
| East: SR 302 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 329 | 4.0 | 329 | 4.0 | 0.396 | 11.3 | LOS B | 1.0 | 27.0 | 0.56 | 0.70 | 0.56 | 31.9 |
| 16 R2 | 108 | 4.0 | 108 | 4.0 | 0.396 | 5.6 | LOS A | 1.0 | 27.0 | 0.56 | 0.70 | 0.56 | 30.7 |
| Approach | 437 | 4.0 | 437 | 4.0 | 0.396 | 9.9 | LOS A | 1.0 | 27.0 | 0.56 | 0.70 | 0.56 | 31.6 |
| North: SR 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 119 | 5.0 | 119 | 5.0 | 0.298 | 11.3 | LOS B | 0.7 | 18.6 | 0.54 | 0.64 | 0.54 | 30.9 |
| 4 T1 | 196 | 5.0 | 196 | 5.0 | 0.298 | 5.7 | LOS A | 0.7 | 18.6 | 0.54 | 0.64 | 0.54 | 35.1 |
| Approach | 315 | 5.0 | 315 | 5.0 | 0.298 | 7.8 | LOS A | 0.7 | 18.6 | 0.54 | 0.64 | 0.54 | 34.0 |
| All Vehicles | 1657 | 3.6 | 1657 | 3.6 | 0.711 | 7.0 | LOS A | 3.1 | 80.1 | 0.57 | 0.60 | 0.57 | 33.3 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Network Data dialog (Network tab). Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

SIDRA INTERSECTION 8.0 | Copyright © 2000-2019 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: PARAMETRIX | Processed: Wednesday, September 4, 2019 2:28:37 PM
Project: U:IPSO\ProjectsIClients11631-WSDOT\234-1631-130 SR3FreightCorr TOAA102WBSI07_OperationsAnalysis\SR3_RBTs_v3.sip8

MOVEMENT SUMMARY
$\theta$ Site: 2 [SR 3/SR 302-2040 AM Three Connector Build - East RAB]

蟿 Network: N101 [SR3 3/SR 3022040 AM Build Three Connectors]
Build - Opening Year
2025 AM Peak Hour
Double RAB
Site Category: -
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Demand Flows Arrival Flows Total HV Total HV |  |  |  | Deg. Satn v/c | Average Delay sec | Level of Service | Aver. Back of Queue Vehicles Distance |  | Prop. Queued | Effective Aver. No.Average Stop Cycles Speed |  |  |
| South: Bellwood Lane |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 1 | 3.0 | 1 | 3.0 | 0.006 | 13.4 | LOS B | 0.0 | 0.4 | 0.68 | 0.61 | 0.68 | 29.6 |
| 3 a | L1 | 1 | 3.0 | 1 | 3.0 | 0.006 | 12.3 | LOS B | 0.0 | 0.4 | 0.68 | 0.61 | 0.68 | 33.9 |
| 8 | T1 | 1 | 3.0 | 1 | 3.0 | 0.006 | 7.8 | LOS A | 0.0 | 0.4 | 0.68 | 0.61 | 0.68 | 34.2 |
| 18 | R2 | 1 | 3.0 | 1 | 3.0 | 0.006 | 7.8 | LOS A | 0.0 | 0.4 | 0.68 | 0.61 | 0.68 | 33.3 |
| Appr | ach | 5 | 3.0 | 5 | 3.0 | 0.006 | 10.3 | LOS B | 0.0 | 0.4 | 0.68 | 0.61 | 0.68 | 33.1 |
| East: SR 302 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 1 | 4.0 | 1 | 4.0 | 0.170 | 12.7 | LOS B | 0.4 | 9.8 | 0.63 | 0.68 | 0.63 | 35.6 |
| 6 | T1 | 101 | 4.0 | 101 | 4.0 | 0.170 | 7.1 | LOS A | 0.4 | 9.8 | 0.63 | 0.68 | 0.63 | 31.7 |
| 16a | R1 | 1 | 4.0 | 1 | 4.0 | 0.170 | 6.7 | LOS A | 0.4 | 9.8 | 0.63 | 0.68 | 0.63 | 35.4 |
| 16 | R2 | 48 | 4.0 | 48 | 4.0 | 0.170 | 7.1 | LOS A | 0.4 | 9.8 | 0.63 | 0.68 | 0.63 | 34.6 |
| Appr | ach | 151 | 4.0 | 151 | 4.0 | 0.170 | 7.1 | LOS A | 0.4 | 9.8 | 0.63 | 0.68 | 0.63 | 33.1 |
| North: SR 3 Bypass |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 42 | 5.0 | 42 | 5.0 | 0.301 | 10.2 | LOS B | 0.7 | 19.3 | 0.32 | 0.52 | 0.32 | 36.6 |
| 4 | T1 | 1 | 5.0 | 1 | 5.0 | 0.301 | 4.6 | LOS A | 0.7 | 19.3 | 0.32 | 0.52 | 0.32 | 36.6 |
| 14 | R2 | 333 | 5.0 | 333 | 5.0 | 0.301 | 4.6 | LOS A | 0.7 | 19.3 | 0.32 | 0.52 | 0.32 | 33.1 |
| 14b | R3 | 1 | 5.0 | 1 | 5.0 | 0.301 | 4.8 | LOS A | 0.7 | 19.3 | 0.32 | 0.52 | 0.32 | 35.1 |
| Appr | ach | 377 | 5.0 | 377 | 5.0 | 0.301 | 5.2 | LOS A | 0.7 | 19.3 | 0.32 | 0.52 | 0.32 | 33.7 |
| NorthWest: School Driveway |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7bx | L3 | 1 | 3.0 | 1 | 3.0 | 0.005 | 13.0 | LOS B | 0.0 | 0.3 | 0.55 | 0.57 | 0.55 | 35.3 |
| 7 ax | L1 | 1 | 3.0 | 1 | 3.0 | 0.005 | 10.7 | LOS B | 0.0 | 0.3 | 0.55 | 0.57 | 0.55 | 34.5 |
| 14ax | R1 | 1 | 3.0 | 1 | 3.0 | 0.005 | 5.9 | LOS A | 0.0 | 0.3 | 0.55 | 0.57 | 0.55 | 34.6 |
| 14bx | R3 | 1 | 3.0 | 1 | 3.0 | 0.005 | 6.4 | LOS A | 0.0 | 0.3 | 0.55 | 0.57 | 0.55 | 30.6 |
| Appr |  | 5 | 3.0 | 5 | 3.0 | 0.005 | 9.0 | LOS A | 0.0 | 0.3 | 0.55 | 0.57 | 0.55 | 34.1 |
| West: SR 302 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5b | L3 | 1 | 4.0 | 1 | 4.0 | 0.550 | 11.3 | LOS B | 2.0 | 52.6 | 0.31 | 0.57 | 0.31 | 32.9 |
| 5 | L2 | 594 | 4.0 | 594 | 4.0 | 0.550 | 10.1 | LOS B | 2.0 | 52.6 | 0.31 | 0.57 | 0.31 | 32.4 |
| 2 | T1 | 136 | 4.0 | 136 | 4.0 | 0.550 | 4.5 | LOS A | 2.0 | 52.6 | 0.31 | 0.57 | 0.31 | 32.4 |
| 12 | R2 | 1 | 4.0 | 1 | 4.0 | 0.550 | 4.5 | LOS A | 2.0 | 52.6 | 0.31 | 0.57 | 0.31 | 31.2 |
| Appr | ach | 732 | 4.0 | 732 | 4.0 | 0.550 | 9.1 | LOS A | 2.0 | 52.6 | 0.31 | 0.57 | 0.31 | 32.4 |
| All Ve | icles | 1270 | 4.3 | 1270 | 4.3 | 0.550 | 7.7 | LOS A | 2.0 | 52.6 | 0.35 | 0.57 | 0.35 | 32.8 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Network Data dialog (Network tab). Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements ( $\mathrm{v} / \mathrm{c}$ not used as specified in HCM 6).

Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

SIDRA INTERSECTION 8.0 | Copyright © 2000-2019 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: PARAMETRIX | Processed: Wednesday, September 4, 2019 2:28:37 PM
Project: U:IPSO\Projects\Clients\1631-WSDOT\234-1631-130 SR3FreightCorr TOAAI02WBSI07_OperationsAnalysisISR3_RBTs_v3.sip8

Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

SIDRA INTERSECTION 8.0 | Copyright © 2000-2019 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: PARAMETRIX | Processed: Wednesday, August 21, 2019 4:26:34 PM
Project: U:IPSO\Projects\Clients\1631-WSDOT\234-1631-130 SR3FreightCorr TOAAIO2WBSI07_OperationsAnalysis\SR3_RBTs_v3.sip8

## MOVEMENT SUMMARY

Site: 200 [SR 3/SR 302-2040 PM Build - West RAB]
Build - Horizon Year
2040 PM Peak Hour
Split RAB
Site Category: -
Roundabout

Movement Performance - Vehicles

| Mov Turn ID | Demand Total veh/h | $\begin{array}{r} \text { lows } \\ \text { HV } \\ \% \end{array}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Average Cycles Speed mph |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| South: SR 3 |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 190 | 3.0 | 0.447 | 4.6 | LOS A | 3.5 | 89.3 | 0.49 | 0.52 | 0.49 | 36.6 |
| 18 R2 | 350 | 3.0 | 0.447 | 4.8 | LOS A | 3.5 | 89.3 | 0.49 | 0.52 | 0.49 | 33.5 |
| Approach | 540 | 3.0 | 0.447 | 4.7 | LOS A | 3.5 | 89.3 | 0.49 | 0.52 | 0.49 | 34.8 |
| East: SR 302 |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 492 | 4.0 | 0.542 | 11.0 | LOS B | 4.2 | 107.2 | 0.53 | 0.66 | 0.53 | 32.1 |
| 16 R2 | 150 | 4.0 | 0.542 | 5.2 | LOS A | 4.2 | 107.2 | 0.53 | 0.66 | 0.53 | 30.8 |
| Approach | 642 | 4.0 | 0.542 | 9.7 | LOS A | 4.2 | 107.2 | 0.53 | 0.66 | 0.53 | 31.8 |
| North: SR 3 |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 150 | 5.0 | 0.848 | 21.4 | LOS C | 14.2 | 368.4 | 1.00 | 1.18 | 1.57 | 23.8 |
| 4 T1 | 630 | 5.0 | 0.848 | 15.4 | LOS B | 14.2 | 368.4 | 1.00 | 1.18 | 1.57 | 31.4 |
| Approach | 780 | 5.0 | 0.848 | 16.6 | LOS B | 14.2 | 368.4 | 1.00 | 1.18 | 1.57 | 30.1 |
| All Vehicles | 1962 | 4.1 | 0.848 | 11.1 | LOS B | 14.2 | 368.4 | 0.71 | 0.83 | 0.93 | 31.7 |

Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
Intersection and Approach LOS values are based on average delay for all movements (v/c not used).
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

SIDRA INTERSECTION 8.0 | Copyright © 2000-2019 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: PARAMETRIX | Processed: Wednesday, July 15, 2020 8:33:31 AM
Project: U:IPSO\Projects\Clients\1631-WSDOT\234-1631-132 SR3FreightCorridorTOAC\02WBSITraffic Analysis\05Analysis\Ops\Sidra
ISR3_RBTs_UPDATED_SR302.sip8

## MOVEMENT SUMMARY

Site: 222 [SR 3/SR 302-2040 PM Build - East RAB]
Build - Horizon Year
2040 PM Peak Hour
Split RAB
Site Category: -
Roundabout

Movement Performance - Vehicles

| Mov Turn ID | Demand <br> Total veh/h | $\begin{array}{r} \text { lows } \\ \text { HV } \\ \% \end{array}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back of Queue <br> Vehicles Distance veh $\qquad$ |  | Prop. Queued | Effective Stop Rate | Aver. No. Average Cycles Speed mph |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| East: SR 302 ( 0.50 .51 |  |  |  |  |  |  |  |  |  |  |  |
| 6 T1 | 151 | 4.0 | 0.202 | 5.4 | LOS A | 1.1 | 28.2 | 0.51 | 0.57 | 0.51 | 34.7 |
| 16 R2 | 70 | 4.0 | 0.202 | 5.6 | LOS A | 1.1 | 28.2 | 0.51 | 0.57 | 0.51 | 35.2 |
| Approach | 221 | 4.0 | 0.202 | 5.5 | LOS A | 1.1 | 28.2 | 0.51 | 0.57 | 0.51 | 34.9 |
| North: SR 3 Bypass |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 75 | 5.0 | 0.467 | 10.7 | LOS B | 3.3 | 87.0 | 0.45 | 0.56 | 0.45 | 36.3 |
| 14 R2 | 491 | 5.0 | 0.467 | 4.9 | LOS A | 3.3 | 87.0 | 0.45 | 0.56 | 0.45 | 33.1 |
| Approach | 566 | 5.0 | 0.467 | 5.7 | LOS A | 3.3 | 87.0 | 0.45 | 0.56 | 0.45 | 33.7 |
| West: SR 302 |  |  |  |  |  |  |  |  |  |  |  |
| 5 L2 | 382 | 4.0 | 0.411 | 10.2 | LOS B | 3.1 | 81.0 | 0.33 | 0.58 | 0.33 | 32.8 |
| 2 T1 | 151 | 4.0 | 0.411 | 4.3 | LOS A | 3.1 | 81.0 | 0.33 | 0.58 | 0.33 | 32.8 |
| Approach | 533 | 4.0 | 0.411 | 8.6 | LOS A | 3.1 | 81.0 | 0.33 | 0.58 | 0.33 | 32.8 |
| All Vehicles | 1320 | 4.4 | 0.467 | 6.8 | LOS A | 3.3 | 87.0 | 0.41 | 0.57 | 0.41 | 33.5 |

Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
Intersection and Approach LOS values are based on average delay for all movements (v/c not used).
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

SIDRA INTERSECTION 8.0 | Copyright © 2000-2019 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: PARAMETRIX | Processed: Wednesday, July 15, 2020 8:36:49 AM
Project: U:IPSO\Projects\Clients\1631-WSDOT\234-1631-132 SR3FreightCorridorTOAC\02WBSITraffic Analysis\05Analysis\Ops\Sidra
ISR3_RBTs_UPDATED_SR302.sip8

## MOVEMENT SUMMARY

Site: 2 [SR 3/Lake Flora Road - 2025 AM Build - No PSIC Vols]
Build - Opening Year
2025 AM Peak Hour
No PSIC Volumes
Site Category: -
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID |  | Demand <br> Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \hline \% \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: SR 3 Bypass |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 10 | 4.0 | 0.513 | 16.2 | LOS B | 4.1 | 104.5 | 0.85 | 0.95 | 0.99 | 34.0 |
| 8 | T1 | 310 | 4.0 | 0.513 | 10.6 | LOS B | 4.1 | 104.5 | 0.85 | 0.95 | 0.99 | 34.0 |
| 18 | R2 | 30 | 4.0 | 0.513 | 10.6 | LOS B | 4.1 | 104.5 | 0.85 | 0.95 | 0.99 | 33.1 |
| Appr |  | 350 | 4.0 | 0.513 | 10.7 | LOS B | 4.1 | 104.5 | 0.85 | 0.95 | 0.99 | 34.0 |
| East: Lake Flora Road |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 25 | 2.0 | 0.274 | 16.4 | LOS B | 1.7 | 43.6 | 0.82 | 0.88 | 0.82 | 33.6 |
| 6 | T1 | 85 | 2.0 | 0.274 | 10.8 | LOS B | 1.7 | 43.6 | 0.82 | 0.88 | 0.82 | 33.6 |
| 16 | R2 | 50 | 2.0 | 0.274 | 10.8 | LOS B | 1.7 | 43.6 | 0.82 | 0.88 | 0.82 | 32.7 |
| Appr |  | 160 | 2.0 | 0.274 | 11.6 | LOS B | 1.7 | 43.6 | 0.82 | 0.88 | 0.82 | 33.3 |
| North: SR 3 |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 15 | 6.0 | 0.428 | 10.5 | LOS B | 3.0 | 79.8 | 0.42 | 0.52 | 0.42 | 36.4 |
| 4 | T1 | 145 | 6.0 | 0.428 | 4.9 | LOS A | 3.0 | 79.8 | 0.42 | 0.52 | 0.42 | 36.4 |
| 14 | R2 | 310 | 6.0 | 0.428 | 4.9 | LOS A | 3.0 | 79.8 | 0.42 | 0.52 | 0.42 | 35.3 |
| Approach |  | 470 | 6.0 | 0.428 | 5.1 | LOS A | 3.0 | 79.8 | 0.42 | 0.52 | 0.42 | 35.7 |
| West: SR 3 |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 565 | 4.0 | 0.616 | 11.4 | LOS B | 5.0 | 128.7 | 0.59 | 0.68 | 0.59 | 33.8 |
| 2 | T1 | 85 | 4.0 | 0.616 | 5.8 | LOS A | 5.0 | 128.7 | 0.59 | 0.68 | 0.59 | 33.8 |
| 12 | R2 | 10 | 4.0 | 0.616 | 5.8 | LOS A | 5.0 | 128.7 | 0.59 | 0.68 | 0.59 | 32.9 |
| Appr |  | 660 | 4.0 | 0.616 | 10.6 | LOS B | 5.0 | 128.7 | 0.59 | 0.68 | 0.59 | 33.8 |
| All V | icles | 1640 | 4.4 | 0.616 | 9.2 | LOS A | 5.0 | 128.7 | 0.62 | 0.71 | 0.65 | 34.3 |

Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
Intersection and Approach LOS values are based on average delay for all movements (v/c not used).
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^11]
## MOVEMENT SUMMARY

Site: 2 [SR 3/Lake Flora Road - 2025 PM Build - No PSIC Vols]
Build - Opening Year
2025 PM Peak Hour
No PSIC Volumes
Site Category: -
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov | Turn | Demand <br> Total veh/h | $\begin{array}{r} \text { lows } \\ \text { HV } \\ \% \end{array}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: SR 3 Bypass |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 11 | 3.0 | 0.350 | 14.1 | LOS B | 2.3 | 58.0 | 0.79 | 0.83 | 0.79 | 34.9 |
| 8 | T1 | 191 | 3.0 | 0.350 | 8.5 | LOS A | 2.3 | 58.0 | 0.79 | 0.83 | 0.79 | 34.9 |
| 18 | R2 | 34 | 3.0 | 0.350 | 8.5 | LOS A | 2.3 | 58.0 | 0.79 | 0.83 | 0.79 | 33.9 |
| Appr |  | 236 | 3.0 | 0.350 | 8.8 | LOS A | 2.3 | 58.0 | 0.79 | 0.83 | 0.79 | 34.8 |
| East: Lake Flora Road |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 22 | 4.0 | 0.156 | 13.8 | LOS B | 0.9 | 23.0 | 0.71 | 0.76 | 0.71 | 34.7 |
| 6 | T1 | 62 | 4.0 | 0.156 | 8.1 | LOS A | 0.9 | 23.0 | 0.71 | 0.76 | 0.71 | 34.7 |
| 16 | R2 | 22 | 4.0 | 0.156 | 8.1 | LOS A | 0.9 | 23.0 | 0.71 | 0.76 | 0.71 | 33.7 |
| Appr |  | 107 | 4.0 | 0.156 | 9.3 | LOS A | 0.9 | 23.0 | 0.71 | 0.76 | 0.71 | 34.5 |
| North: SR 3 |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 62 | 4.0 | 0.688 | 10.8 | LOS B | 7.4 | 191.3 | 0.56 | 0.53 | 0.56 | 36.0 |
| 4 | T1 | 225 | 4.0 | 0.688 | 5.2 | LOS A | 7.4 | 191.3 | 0.56 | 0.53 | 0.56 | 36.0 |
| 14 | R2 | 506 | 4.0 | 0.688 | 5.2 | LOS A | 7.4 | 191.3 | 0.56 | 0.53 | 0.56 | 34.9 |
| Approach |  | 792 | 4.0 | 0.688 | 5.6 | LOS A | 7.4 | 191.3 | 0.56 | 0.53 | 0.56 | 35.3 |
| West: SR 3 |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 483 | 3.0 | 0.641 | 13.4 | LOS B | 6.0 | 154.3 | 0.73 | 0.82 | 0.82 | 33.4 |
| 2 | T1 | 129 | 3.0 | 0.641 | 7.8 | LOS A | 6.0 | 154.3 | 0.73 | 0.82 | 0.82 | 33.4 |
| 12 | R2 | 11 | 3.0 | 0.641 | 7.7 | LOS A | 6.0 | 154.3 | 0.73 | 0.82 | 0.82 | 32.5 |
| Appr |  | 624 | 3.0 | 0.641 | 12.1 | LOS B | 6.0 | 154.3 | 0.73 | 0.82 | 0.82 | 33.4 |
| All V | icles | 1758 | 3.5 | 0.688 | 8.6 | LOS A | 7.4 | 191.3 | 0.66 | 0.69 | 0.69 | 34.5 |

Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
Intersection and Approach LOS values are based on average delay for all movements (v/c not used).
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^12]
## MOVEMENT SUMMARY

Site: 2 [Single Lane - SR 3/Lake Flora Road - 2040 AM Build - Three Connectors]
Three Connectors Build - Horizon Year
2040 AM Peak Hour
Site Category: -
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | Turn | Demand <br> Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: SR 3 Bypass |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 10 | 4.0 | 1.373 | 199.3 | LOS F | 72.6 | 1873.1 | 1.00 | 3.02 | 6.34 | 9.0 |
| 8 | T1 | 530 | 4.0 | 1.373 | 193.7 | LOS F | 72.6 | 1873.1 | 1.00 | 3.02 | 6.34 | 9.0 |
| 18 | R2 | 105 | 4.0 | 1.373 | 193.7 | LOS F | 72.6 | 1873.1 | 1.00 | 3.02 | 6.34 | 8.9 |
| Approad | ach | 645 | 4.0 | 1.373 | 193.8 | LOS F | 72.6 | 1873.1 | 1.00 | 3.02 | 6.34 | 9.0 |
| East: Lake Flora Road |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 40 | 2.0 | 0.537 | 27.6 | LOS C | 5.0 | 127.9 | 1.00 | 1.12 | 1.32 | 28.8 |
| 6 | T1 | 115 | 2.0 | 0.537 | 22.0 | LOS C | 5.0 | 127.9 | 1.00 | 1.12 | 1.32 | 28.8 |
| 16 | R2 | 65 | 2.0 | 0.537 | 22.0 | LOS C | 5.0 | 127.9 | 1.00 | 1.12 | 1.32 | 28.1 |
| Approad |  | 220 | 2.0 | 0.537 | 23.0 | LOS C | 5.0 | 127.9 | 1.00 | 1.12 | 1.32 | 28.6 |
| North: SR 3 |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 15 | 6.0 | 0.578 | 10.9 | LOS B | 5.2 | 135.9 | 0.58 | 0.55 | 0.58 | 35.9 |
| 4 | T1 | 285 | 6.0 | 0.578 | 5.3 | LOS A | 5.2 | 135.9 | 0.58 | 0.55 | 0.58 | 35.9 |
| 14 | R2 | 375 | 6.0 | 0.578 | 5.3 | LOS A | 5.2 | 135.9 | 0.58 | 0.55 | 0.58 | 34.9 |
| Approach |  | 675 | 6.0 | 0.578 | 5.4 | LOS A | 5.2 | 135.9 | 0.58 | 0.55 | 0.58 | 35.3 |
| West: SR 3 |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 745 | 4.0 | 0.872 | 19.1 | LOS D | 16.2 | 417.3 | 1.00 | 1.05 | 1.43 | 30.8 |
| 2 | T1 | 165 | 4.0 | 0.872 | 13.5 | LOS D | 16.2 | 417.3 | 1.00 | 1.05 | 1.43 | 30.8 |
| 12 | R2 | 10 | 4.0 | 0.872 | 13.5 | LOS D | 16.2 | 417.3 | 1.00 | 1.05 | 1.43 | 30.1 |
| Approad | ach | 920 | 4.0 | 0.872 | 18.1 | LOS B | 16.2 | 417.3 | 1.00 | 1.05 | 1.43 | 30.8 |
| All Ve | icles | 2460 | 4.4 | 1.373 | 61.1 | LOS E | 72.6 | 1873.1 | 0.88 | 1.44 | 2.47 | 19.2 |

Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
Intersection and Approach LOS values are based on average delay for all movements (v/c not used).
Roundabout Capacity Model: SIDRA Standard
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^13]
## MOVEMENT SUMMARY

Site: 2 [Single Lane - SR 3/Lake Flora Road - 2040 PM Build - Three Connectors]
Three Connectors Build - Horizon Year
2040 PM Peak Hour
Site Category: -
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | Turn | Demand Total veh/h |  | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: SR 3 Bypass |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 11 | 3.0 | 0.756 | 25.4 | LOS C | 9.5 | 244.2 | 1.00 | 1.21 | 1.54 | 29.9 |
| 8 | T1 | 326 | 3.0 | 0.756 | 19.8 | LOS B | 9.5 | 244.2 | 1.00 | 1.21 | 1.54 | 29.9 |
| 18 | R2 | 96 | 3.0 | 0.756 | 19.8 | LOS B | 9.5 | 244.2 | 1.00 | 1.21 | 1.54 | 29.2 |
| Appr |  | 433 | 3.0 | 0.756 | 20.0 | LOS B | 9.5 | 244.2 | 1.00 | 1.21 | 1.54 | 29.7 |
| East: Lake Flora Road |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 219 | 4.0 | 0.893 | 40.9 | LOS D | 16.3 | 419.9 | 1.00 | 1.48 | 2.27 | 24.3 |
| 6 | T1 | 270 | 4.0 | 0.893 | 35.3 | LOS D | 16.3 | 419.9 | 1.00 | 1.48 | 2.27 | 24.3 |
| 16 | R2 | 28 | 4.0 | 0.893 | 35.3 | LOS D | 16.3 | 419.9 | 1.00 | 1.48 | 2.27 | 23.9 |
| Appr |  | 517 | 4.0 | 0.893 | 37.7 | LOS D | 16.3 | 419.9 | 1.00 | 1.48 | 2.27 | 24.3 |
| North: SR 3 |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 73 | 4.0 | 1.247 | 131.9 | LOS F | 88.2 | 2274.8 | 1.00 | 3.22 | 6.24 | 12.3 |
| 4 | T1 | 444 | 4.0 | 1.247 | 126.2 | LOS F | 88.2 | 2274.8 | 1.00 | 3.22 | 6.24 | 12.3 |
| 14 | R2 | 562 | 4.0 | 1.247 | 126.2 | LOS F | 88.2 | 2274.8 | 1.00 | 3.22 | 6.24 | 12.1 |
| Appr |  | 1079 | 4.0 | 1.247 | 126.6 | LOS F | 88.2 | 2274.8 | 1.00 | 3.22 | 6.24 | 12.2 |
| West: SR 3 |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 579 | 3.0 | 0.988 | 43.2 | LOS E | 27.8 | 712.1 | 1.00 | 1.71 | 2.77 | 23.4 |
| 2 | T1 | 202 | 3.0 | 0.988 | 37.6 | LOS E | 27.8 | 712.1 | 1.00 | 1.71 | 2.77 | 23.4 |
| 12 | R2 | 11 | 3.0 | 0.988 | 37.6 | LOS E | 27.8 | 712.1 | 1.00 | 1.71 | 2.77 | 23.0 |
| Approach |  | 792 | 3.0 | 0.988 | 41.7 | LOS D | 27.8 | 712.1 | 1.00 | 1.71 | 2.77 | 23.4 |
| All V | icles | 2820 | 3.6 | 1.247 | 70.1 | LOS E | 88.2 | 2274.8 | 1.00 | 2.17 | 3.81 | 17.9 |

Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
Intersection and Approach LOS values are based on average delay for all movements (v/c not used).
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^14]
## MOVEMENT SUMMARY

## Site: 2 [SR 3/Log Yard Road - 2025 AM No Build]

No Build - Opening Year
2025 AM Peak Hour
Site Category: -
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | Turn | Demand Total veh/h | Flows HV \% | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 5 | 2.0 | 0.888 | 11.4 | LOS D | 17.9 | 455.4 | 0.87 | 0.51 | 0.87 | 34.9 |
| 8 | T1 | 975 | 2.0 | 0.888 | 5.8 | LOS D | 17.9 | 455.4 | 0.87 | 0.51 | 0.87 | 34.9 |
| 18 | R2 | 95 | 2.0 | 0.888 | 5.8 | LOS D | 17.9 | 455.4 | 0.87 | 0.51 | 0.87 | 33.9 |
| Appr |  | 1075 | 2.0 | 0.888 | 5.8 | LOS A | 17.9 | 455.4 | 0.87 | 0.51 | 0.87 | 34.8 |
| East: Park and Ride |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 50 | 2.0 | 0.287 | 18.1 | LOS B | 2.0 | 51.3 | 0.95 | 0.96 | 0.95 | 32.1 |
| 6 | T1 | 5 | 2.0 | 0.287 | 12.5 | LOS B | 2.0 | 51.3 | 0.95 | 0.96 | 0.95 | 32.1 |
| 16 | R2 | 60 | 2.0 | 0.287 | 12.4 | LOS B | 2.0 | 51.3 | 0.95 | 0.96 | 0.95 | 31.3 |
| Appr |  | 115 | 2.0 | 0.287 | 14.9 | LOS B | 2.0 | 51.3 | 0.95 | 0.96 | 0.95 | 31.6 |
| North: SR 3 |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 30 | 2.0 | 0.446 | 10.1 | LOS B | 3.5 | 89.8 | 0.31 | 0.43 | 0.31 | 36.6 |
| 4 | T1 | 505 | 2.0 | 0.446 | 4.4 | LOS A | 3.5 | 89.8 | 0.31 | 0.43 | 0.31 | 36.6 |
| 14 | R2 | 5 | 2.0 | 0.446 | 4.4 | LOS A | 3.5 | 89.8 | 0.31 | 0.43 | 0.31 | 35.5 |
| Appr |  | 540 | 2.0 | 0.446 | 4.8 | LOS A | 3.5 | 89.8 | 0.31 | 0.43 | 0.31 | 36.6 |
| West: Log Yard Road |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 35 | 9.0 | 0.081 | 13.0 | LOS B | 0.4 | 10.6 | 0.59 | 0.72 | 0.59 | 34.0 |
| 2 | T1 | 5 | 9.0 | 0.081 | 7.4 | LOS A | 0.4 | 10.6 | 0.59 | 0.72 | 0.59 | 34.1 |
| 12 | R2 | 20 | 9.0 | 0.081 | 7.3 | LOS A | 0.4 | 10.6 | 0.59 | 0.72 | 0.59 | 33.1 |
| Appr |  | 60 | 9.0 | 0.081 | 10.6 | LOS B | 0.4 | 10.6 | 0.59 | 0.72 | 0.59 | 33.7 |
| All V | icles | 1790 | 2.2 | 0.888 | 6.2 | LOS A | 17.9 | 455.4 | 0.70 | 0.52 | 0.70 | 35.0 |

Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
Intersection and Approach LOS values are based on average delay for all movements (v/c not used).
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^15]
## MOVEMENT SUMMARY

## Site: 2 [SR 3/Log Yard Road - 2025 PM No Build]

No Build - Opening Year
2025 PM Peak Hour
Site Category: -
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | Demand Total veh/h |  | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles <br> veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: SR 3 |  |  |  |  |  |  |  |  |  |  |  |
| 3 L2 | 5 | 1.0 | 0.610 | 10.4 | LOS B | 5.6 | 140.1 | 0.43 | 0.46 | 0.43 | 36.4 |
| 8 T1 | 665 | 1.0 | 0.610 | 4.8 | LOS A | 5.6 | 140.1 | 0.43 | 0.46 | 0.43 | 36.3 |
| 18 R2 | 65 | 1.0 | 0.610 | 4.8 | LOS A | 5.6 | 140.1 | 0.43 | 0.46 | 0.43 | 35.3 |
| Approach | 735 | 1.0 | 0.610 | 4.9 | LOS A | 5.6 | 140.1 | 0.43 | 0.46 | 0.43 | 36.2 |
| East: Park and Ride |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 90 | 1.0 | 0.204 | 13.6 | LOS B | 1.2 | 29.6 | 0.70 | 0.80 | 0.70 | 33.8 |
| 6 T1 | 5 | 1.0 | 0.204 | 8.0 | LOS A | 1.2 | 29.6 | 0.70 | 0.80 | 0.70 | 33.8 |
| 16 R2 | 55 | 1.0 | 0.204 | 8.0 | LOS A | 1.2 | 29.6 | 0.70 | 0.80 | 0.70 | 32.9 |
| Approach | 150 | 1.0 | 0.204 | 11.4 | LOS B | 1.2 | 29.6 | 0.70 | 0.80 | 0.70 | 33.5 |
| North: SR 3 |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 65 | 1.0 | 0.747 | 10.9 | LOS B | 9.3 | 233.9 | 0.63 | 0.52 | 0.63 | 35.5 |
| 4 T1 | 815 | 1.0 | 0.747 | 5.3 | LOS A | 9.3 | 233.9 | 0.63 | 0.52 | 0.63 | 35.5 |
| 14 R2 | 5 | 1.0 | 0.747 | 5.3 | LOS A | 9.3 | 233.9 | 0.63 | 0.52 | 0.63 | 34.5 |
| Approach | 885 | 1.0 | 0.747 | 5.7 | LOS A | 9.3 | 233.9 | 0.63 | 0.52 | 0.63 | 35.5 |
| West: Log Yard Road |  |  |  |  |  |  |  |  |  |  |  |
| 5 L2 | 15 | 9.0 | 0.099 | 17.1 | LOS B | 0.6 | 16.0 | 0.83 | 0.84 | 0.83 | 32.6 |
| 2 T1 | 5 | 9.0 | 0.099 | 11.5 | LOS B | 0.6 | 16.0 | 0.83 | 0.84 | 0.83 | 32.7 |
| 12 R 2 | 25 | 9.0 | 0.099 | 11.5 | LOS B | 0.6 | 16.0 | 0.83 | 0.84 | 0.83 | 31.8 |
| Approach | 45 | 9.0 | 0.099 | 13.4 | LOS B | 0.6 | 16.0 | 0.83 | 0.84 | 0.83 | 32.1 |
| All Vehicles | 1815 | 1.2 | 0.747 | 6.0 | LOS A | 9.3 | 233.9 | 0.56 | 0.53 | 0.56 | 35.5 |

Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
Intersection and Approach LOS values are based on average delay for all movements (v/c not used).
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^16]
## MOVEMENT SUMMARY

## $\nabla$ Site: 2 [SR 3/Log Yard Road - 2025 AM Build]

Build - Opening Year
2025 AM Peak Hour
Site Category: -
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Deman Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: SR 3 |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 5 | 2.0 | 0.527 | 10.2 | LOS B | 4.0 | 100.9 | 0.33 | 0.44 | 0.33 | 36.7 |
| 8 | T1 | 540 | 2.0 | 0.527 | 4.6 | LOSA | 4.0 | 100.9 | 0.33 | 0.44 | 0.33 | 36.7 |
| 18 | R2 | 95 | 2.0 | 0.527 | 4.6 | LOSA | 4.0 | 100.9 | 0.33 | 0.44 | 0.33 | 35.6 |
| Appr |  | 640 | 2.0 | 0.527 | 4.7 | LOS A | 4.0 | 100.9 | 0.33 | 0.44 | 0.33 | 36.5 |
| East: Park and Ride |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 50 | 2.0 | 0.141 | 12.7 | LOS B | 0.7 | 18.8 | 0.61 | 0.73 | 0.61 | 34.7 |
| 6 | T1 | 5 | 2.0 | 0.141 | 7.1 | LOSA | 0.7 | 18.8 | 0.61 | 0.73 | 0.61 | 34.7 |
| 16 | R2 | 60 | 2.0 | 0.141 | 7.1 | LOSA | 0.7 | 18.8 | 0.61 | 0.73 | 0.61 | 33.7 |
| Appr |  | 115 | 2.0 | 0.141 | 9.6 | LOS A | 0.7 | 18.8 | 0.61 | 0.73 | 0.61 | 34.2 |
| North: SR 3 |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 30 | 2.0 | 0.213 | 9.9 | LOSA | 1.2 | 30.0 | 0.22 | 0.44 | 0.22 | 36.8 |
| 4 | T1 | 225 | 2.0 | 0.213 | 4.3 | LOSA | 1.2 | 30.0 | 0.22 | 0.44 | 0.22 | 36.7 |
| 14 | R2 | 5 | 2.0 | 0.213 | 4.3 | LOSA | 1.2 | 30.0 | 0.22 | 0.44 | 0.22 | 35.7 |
| Appr |  | 260 | 2.0 | 0.213 | 5.0 | LOS A | 1.2 | 30.0 | 0.22 | 0.44 | 0.22 | 36.7 |
| West: Log Yard Road |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 35 | 9.0 | 0.064 | 11.2 | LOS B | 0.3 | 7.5 | 0.42 | 0.63 | 0.42 | 34.8 |
| 2 | T1 | 5 | 9.0 | 0.064 | 5.6 | LOSA | 0.3 | 7.5 | 0.42 | 0.63 | 0.42 | 34.9 |
| 12 | R2 | 20 | 9.0 | 0.064 | 5.6 | LOSA | 0.3 | 7.5 | 0.42 | 0.63 | 0.42 | 33.9 |
| Approach |  | 60 | 9.0 | 0.064 | 8.9 | LOS A | 0.3 | 7.5 | 0.42 | 0.63 | 0.42 | 34.5 |
| All Vehicles |  | 1075 | 2.4 | 0.527 | 5.5 | LOS A | 4.0 | 100.9 | 0.34 | 0.48 | 0.34 | 36.2 |

Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
Intersection and Approach LOS values are based on average delay for all movements (v/c not used).
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^17]
## MOVEMENT SUMMARY

## $\square$ Site: 2 [SR 3/Log Yard Road - 2025 PM Build]

Build - Opening Year
2025 PM Peak Hour
Site Category: -
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Deman Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: SR 3 |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 5 | 1.0 | 0.433 | 10.2 | LOS B | 2.9 | 72.3 | 0.32 | 0.44 | 0.32 | 36.8 |
| 8 | T1 | 455 | 1.0 | 0.433 | 4.6 | LOSA | 2.9 | 72.3 | 0.32 | 0.44 | 0.32 | 36.7 |
| 18 | R2 | 65 | 1.0 | 0.433 | 4.6 | LOSA | 2.9 | 72.3 | 0.32 | 0.44 | 0.32 | 35.7 |
| Appr |  | 525 | 1.0 | 0.433 | 4.7 | LOS A | 2.9 | 72.3 | 0.32 | 0.44 | 0.32 | 36.6 |
| East: Park and Ride |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 90 | 1.0 | 0.166 | 12.0 | LOS B | 0.9 | 21.6 | 0.55 | 0.72 | 0.55 | 34.6 |
| 6 | T1 | 5 | 1.0 | 0.166 | 6.4 | LOSA | 0.9 | 21.6 | 0.55 | 0.72 | 0.55 | 34.6 |
| 16 | R2 | 55 | 1.0 | 0.166 | 6.4 | LOSA | 0.9 | 21.6 | 0.55 | 0.72 | 0.55 | 33.7 |
| Appr |  | 150 | 1.0 | 0.166 | 9.8 | LOS A | 0.9 | 21.6 | 0.55 | 0.72 | 0.55 | 34.3 |
| North: SR 3 |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 65 | 1.0 | 0.516 | 10.4 | LOS B | 4.0 | 101.9 | 0.40 | 0.48 | 0.40 | 36.2 |
| 4 | T1 | 545 | 1.0 | 0.516 | 4.8 | LOSA | 4.0 | 101.9 | 0.40 | 0.48 | 0.40 | 36.2 |
| 14 | R2 | 5 | 1.0 | 0.516 | 4.8 | LOSA | 4.0 | 101.9 | 0.40 | 0.48 | 0.40 | 35.1 |
| Appr |  | 615 | 1.0 | 0.516 | 5.4 | LOS A | 4.0 | 101.9 | 0.40 | 0.48 | 0.40 | 36.2 |
| West: Log Yard Road |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 15 | 9.0 | 0.067 | 13.8 | LOS B | 0.3 | 9.3 | 0.65 | 0.73 | 0.65 | 34.2 |
| 2 | T1 | 5 | 9.0 | 0.067 | 8.2 | LOSA | 0.3 | 9.3 | 0.65 | 0.73 | 0.65 | 34.3 |
| 12 | R2 | 25 | 9.0 | 0.067 | 8.2 | LOSA | 0.3 | 9.3 | 0.65 | 0.73 | 0.65 | 33.3 |
| Approach |  | 45 | 9.0 | 0.067 | 10.1 | LOS B | 0.3 | 9.3 | 0.65 | 0.73 | 0.65 | 33.7 |
| All Vehicles |  | 1335 | 1.3 | 0.516 | 5.7 | LOS A | 4.0 | 101.9 | 0.40 | 0.50 | 0.40 | 36.0 |

Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
Intersection and Approach LOS values are based on average delay for all movements (v/c not used).
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^18]
## MOVEMENT SUMMARY

## Site: 2 [SR 3/Log Yard Road - 2040 AM No Build]

No Build - Horizon Year
2040 AM Peak Hour
Site Category: -
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: SR 3 |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 5 | 2.0 | 1.106 | 63.4 | LOS F | 88.6 | 2250.3 | 1.00 | 1.33 | 2.14 | 19.9 |
| 8 | T1 | 1295 | 2.0 | 1.106 | 57.8 | LOS F | 88.6 | 2250.3 | 1.00 | 1.33 | 2.14 | 19.9 |
| 18 | R2 | 145 | 2.0 | 1.106 | 57.8 | LOS F | 88.6 | 2250.3 | 1.00 | 1.33 | 2.14 | 19.5 |
| Appr |  | 1445 | 2.0 | 1.106 | 57.8 | LOS E | 88.6 | 2250.3 | 1.00 | 1.33 | 2.14 | 19.8 |
| East: Park and Ride |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 80 | 2.0 | 0.573 | 34.4 | LOS C | 5.6 | 141.4 | 1.00 | 1.12 | 1.33 | 26.0 |
| 6 | T1 | 5 | 2.0 | 0.573 | 28.8 | LOS C | 5.6 | 141.4 | 1.00 | 1.12 | 1.33 | 26.0 |
| 16 | R2 | 85 | 2.0 | 0.573 | 28.8 | LOS C | 5.6 | 141.4 | 1.00 | 1.12 | 1.33 | 25.4 |
| Appr |  | 170 | 2.0 | 0.573 | 31.5 | LOS C | 5.6 | 141.4 | 1.00 | 1.12 | 1.33 | 25.7 |
| North: SR 3 |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 60 | 2.0 | 0.553 | 10.3 | LOS B | 5.2 | 132.0 | 0.43 | 0.47 | 0.43 | 36.1 |
| 4 | T1 | 655 | 2.0 | 0.553 | 4.7 | LOSA | 5.2 | 132.0 | 0.43 | 0.47 | 0.43 | 36.1 |
| 14 | R2 | 5 | 2.0 | 0.553 | 4.6 | LOSA | 5.2 | 132.0 | 0.43 | 0.47 | 0.43 | 35.1 |
| Appr |  | 720 | 2.0 | 0.553 | 5.1 | LOS A | 5.2 | 132.0 | 0.43 | 0.47 | 0.43 | 36.1 |
| West: Log Yard Road |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 40 | 9.0 | 0.094 | 14.3 | LOS B | 0.5 | 14.5 | 0.72 | 0.77 | 0.72 | 33.3 |
| 2 | T1 | 5 | 9.0 | 0.094 | 8.6 | LOS A | 0.5 | 14.5 | 0.72 | 0.77 | 0.72 | 33.4 |
| 12 | R2 | 20 | 9.0 | 0.094 | 8.6 | LOSA | 0.5 | 14.5 | 0.72 | 0.77 | 0.72 | 32.4 |
| Approach |  | 65 | 9.0 | 0.094 | 12.1 | LOS B | 0.5 | 14.5 | 0.72 | 0.77 | 0.72 | 33.0 |
| All Vehicles |  | 2400 | 2.2 | 1.106 | 38.9 | LOS D | 88.6 | 2250.3 | 0.82 | 1.04 | 1.53 | 23.7 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS $F$ will result if $v / c>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^19]
## MOVEMENT SUMMARY

## Site: 2 [SR 3/Log Yard Road - 2040 PM No Build]

No Build - Design Year
2040 PM Peak Hour
Site Category: -
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov | Turn | Demand <br> Total veh/h |  | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: SR 3 |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 10 | 1.0 | 0.811 | 11.7 | LOS B | 11.8 | 298.0 | 0.81 | 0.61 | 0.83 | 35.2 |
| 8 | T1 | 755 | 1.0 | 0.811 | 6.1 | LOS A | 11.8 | 298.0 | 0.81 | 0.61 | 0.83 | 35.2 |
| 18 | R2 | 255 | 1.0 | 0.811 | 6.1 | LOS A | 11.8 | 298.0 | 0.81 | 0.61 | 0.83 | 34.2 |
| Appr |  | 1020 | 1.0 | 0.811 | 6.1 | LOS A | 11.8 | 298.0 | 0.81 | 0.61 | 0.83 | 34.9 |
| East: Park and Ride |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 280 | 1.0 | 0.620 | 18.4 | LOS B | 6.3 | 159.8 | 0.98 | 1.07 | 1.25 | 31.5 |
| 6 | T1 | 10 | 1.0 | 0.620 | 12.8 | LOS B | 6.3 | 159.8 | 0.98 | 1.07 | 1.25 | 31.4 |
| 16 | R2 | 135 | 1.0 | 0.620 | 12.8 | LOS B | 6.3 | 159.8 | 0.98 | 1.07 | 1.25 | 30.7 |
| Appr |  | 425 | 1.0 | 0.620 | 16.5 | LOS B | 6.3 | 159.8 | 0.98 | 1.07 | 1.25 | 31.2 |
| North: SR 3 |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 130 | 1.0 | 1.081 | 58.9 | LOS F | 57.1 | 1438.7 | 1.00 | 1.87 | 3.10 | 20.7 |
| 4 | T1 | 1050 | 1.0 | 1.081 | 53.3 | LOS F | 57.1 | 1438.7 | 1.00 | 1.87 | 3.10 | 20.6 |
| 14 | R2 | 10 | 1.0 | 1.081 | 53.2 | LOS F | 57.1 | 1438.7 | 1.00 | 1.87 | 3.10 | 20.3 |
| Appr |  | 1190 | 1.0 | 1.081 | 53.9 | LOS D | 57.1 | 1438.7 | 1.00 | 1.87 | 3.10 | 20.6 |
| West: Log Yard Road |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 15 | 9.0 | 0.242 | 28.9 | LOS C | 1.8 | 48.5 | 1.00 | 0.98 | 1.00 | 27.9 |
| 2 | T1 | 10 | 9.0 | 0.242 | 23.3 | LOS C | 1.8 | 48.5 | 1.00 | 0.98 | 1.00 | 28.0 |
| 12 | R2 | 30 | 9.0 | 0.242 | 23.3 | LOS C | 1.8 | 48.5 | 1.00 | 0.98 | 1.00 | 27.3 |
| Approach |  | 55 | 9.0 | 0.242 | 24.8 | LOS C | 1.8 | 48.5 | 1.00 | 0.98 | 1.00 | 27.6 |
| All Vehicles |  | 2690 | 1.2 | 1.081 | 29.3 | LOS C | 57.1 | 1438.7 | 0.92 | 1.25 | 1.90 | 26.2 |

Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
Intersection and Approach LOS values are based on average delay for all movements (v/c not used).
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^20]
## MOVEMENT SUMMARY

## F Site: 2 [SR 3/Log Yard Road - 2040 AM Build - Three Connectors]

Three Connector Build - Horizon Year
2040 AM Peak Hour
Site Category: -
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | Demand <br> Total veh/h | $\begin{array}{r} \text { lows } \\ \text { HV } \\ \% \end{array}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles veh | of Queue Distance ft | Prop. Queued $\qquad$ | Effective Stop Rate | Aver. No. Cycles | Average <br> Speed <br> mph |
| South: SR 3 |  |  |  |  |  |  |  |  |  |  |  |
| 3 L2 | 5 | 2.0 | 0.683 | 11.0 | LOS B | 6.3 | 160.5 | 0.56 | 0.54 | 0.56 | 36.0 |
| 8 T1 | 700 | 2.0 | 0.683 | 5.4 | LOS A | 6.3 | 160.5 | 0.56 | 0.54 | 0.56 | 35.9 |
| 18 R2 | 165 | 2.0 | 0.683 | 5.3 | LOS A | 6.3 | 160.5 | 0.56 | 0.54 | 0.56 | 34.9 |
| Approach | 870 | 2.0 | 0.683 | 5.4 | LOS A | 6.3 | 160.5 | 0.56 | 0.54 | 0.56 | 35.7 |
| East: Park and Ride |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 80 | 2.0 | 0.262 | 13.9 | LOS B | 1.7 | 43.6 | 0.78 | 0.82 | 0.78 | 34.2 |
| 6 T1 | 10 | 2.0 | 0.262 | 8.3 | LOS A | 1.7 | 43.6 | 0.78 | 0.82 | 0.78 | 34.2 |
| 16 R 2 | 110 | 2.0 | 0.262 | 8.2 | LOS A | 1.7 | 43.6 | 0.78 | 0.82 | 0.78 | 33.2 |
| Approach | 200 | 2.0 | 0.262 | 10.5 | LOS B | 1.7 | 43.6 | 0.78 | 0.82 | 0.78 | 33.7 |
| North: SR 3 |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 85 | 2.0 | 0.245 | 10.0 | LOS B | 1.5 | 37.7 | 0.29 | 0.49 | 0.29 | 36.1 |
| 4 T1 | 230 | 2.0 | 0.245 | 4.4 | LOS A | 1.5 | 37.7 | 0.29 | 0.49 | 0.29 | 36.1 |
| 14 R2 | 5 | 2.0 | 0.245 | 4.4 | LOS A | 1.5 | 37.7 | 0.29 | 0.49 | 0.29 | 35.1 |
| Approach | 320 | 2.0 | 0.245 | 5.9 | LOS A | 1.5 | 37.7 | 0.29 | 0.49 | 0.29 | 36.1 |
| West: Log Yard Road |  |  |  |  |  |  |  |  |  |  |  |
| 5 L2 | 40 | 9.0 | 0.076 | 11.4 | LOS B | 0.4 | 9.5 | 0.47 | 0.64 | 0.47 | 34.8 |
| $2 \quad \mathrm{~T} 1$ | 20 | 9.0 | 0.076 | 5.8 | LOS A | 0.4 | 9.5 | 0.47 | 0.64 | 0.47 | 34.8 |
| 12 R 2 | 15 | 9.0 | 0.076 | 5.8 | LOS A | 0.4 | 9.5 | 0.47 | 0.64 | 0.47 | 33.8 |
| Approach | 75 | 9.0 | 0.076 | 8.8 | LOS A | 0.4 | 9.5 | 0.47 | 0.64 | 0.47 | 34.6 |
| All Vehicles | 1465 | 2.4 | 0.683 | 6.4 | LOS A | 6.3 | 160.5 | 0.52 | 0.57 | 0.52 | 35.5 |

Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
Intersection and Approach LOS values are based on average delay for all movements (v/c not used).
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^21]
## MOVEMENT SUMMARY

## G Site: 2 [SR 3/Log Yard Road - 2040 PM Build - Three Connectors]

Three Connectors Build - Horizon Year
2040 PM Peak Hour
Site Category: -
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | Turn | Demand Total veh/h | $\begin{gathered} \text { Iows } \\ \text { HV } \\ \hline \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: SR 3 |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 10 | 1.0 | 0.656 | 11.4 | LOS B | 6.2 | 157.0 | 0.67 | 0.60 | 0.68 | 35.8 |
| 8 | T1 | 460 | 1.0 | 0.656 | 5.8 | LOS A | 6.2 | 157.0 | 0.67 | 0.60 | 0.68 | 35.7 |
| 18 | R2 | 315 | 1.0 | 0.656 | 5.8 | LOS A | 6.2 | 157.0 | 0.67 | 0.60 | 0.68 | 34.7 |
| Appr |  | 785 | 1.0 | 0.656 | 5.8 | LOS A | 6.2 | 157.0 | 0.67 | 0.60 | 0.68 | 35.3 |
| East: Park and Ride |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 315 | 1.0 | 0.545 | 13.3 | LOS B | 4.6 | 115.4 | 0.77 | 0.84 | 0.84 | 34.0 |
| 6 | T1 | 30 | 1.0 | 0.545 | 7.7 | LOS A | 4.6 | 115.4 | 0.77 | 0.84 | 0.84 | 34.0 |
| 16 | R2 | 185 | 1.0 | 0.545 | 7.6 | LOS A | 4.6 | 115.4 | 0.77 | 0.84 | 0.84 | 33.1 |
| Appro |  | 530 | 1.0 | 0.545 | 11.0 | LOS B | 4.6 | 115.4 | 0.77 | 0.84 | 0.84 | 33.7 |
| North: SR 3 |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 175 | 1.0 | 0.738 | 14.4 | LOS B | 9.2 | 231.7 | 0.86 | 0.86 | 1.03 | 34.3 |
| 4 | T1 | 605 | 1.0 | 0.738 | 8.8 | LOS A | 9.2 | 231.7 | 0.86 | 0.86 | 1.03 | 34.3 |
| 14 | R2 | 10 | 1.0 | 0.738 | 8.8 | LOS A | 9.2 | 231.7 | 0.86 | 0.86 | 1.03 | 33.4 |
| Appror |  | 790 | 1.0 | 0.738 | 10.1 | LOS B | 9.2 | 231.7 | 0.86 | 0.86 | 1.03 | 34.3 |
| West: Log Yard Road |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 15 | 9.0 | 0.160 | 18.7 | LOS B | 1.1 | 29.4 | 0.92 | 0.89 | 0.92 | 32.2 |
| 2 | T1 | 25 | 9.0 | 0.160 | 13.1 | LOS B | 1.1 | 29.4 | 0.92 | 0.89 | 0.92 | 32.2 |
| 12 | R2 | 30 | 9.0 | 0.160 | 13.1 | LOS B | 1.1 | 29.4 | 0.92 | 0.89 | 0.92 | 31.4 |
| Approach |  | 70 | 9.0 | 0.160 | 14.3 | LOS B | 1.1 | 29.4 | 0.92 | 0.89 | 0.92 | 31.8 |
| All Vehicles |  | 2175 | 1.3 | 0.738 | 8.9 | LOS A | 9.2 | 231.7 | 0.77 | 0.76 | 0.85 | 34.4 |

Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
Intersection and Approach LOS values are based on average delay for all movements (v/c not used).
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^22]3: SR 3 \& NE Clifton Lane/Rite Aid Driveway

| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | F | ${ }^{7}$ | $\hat{\beta}$ | \% | F | * | 4 | 「 |
| Traffic Volume (vph) | 445 | 25 | 5 | 5 | 65 | 580 | 5 | 370 | 140 |
| Future Volume (vph) | 445 | 25 | 5 | 5 | 65 | 580 | 5 | 370 | 140 |
| Turn Type | Perm | NA | Perm | NA | Prot | NA | Prot | NA | Perm |
| Protected Phases |  | 8 |  | 4 | 5 | 2 | 1 | 6 |  |
| Permitted Phases | 8 |  | 4 |  |  |  |  |  | 6 |
| Detector Phase | 8 | 8 | 4 | 4 | 5 | 2 | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 10.0 | 6.0 | 10.0 | 10.0 |
| Minimum Split (s) | 29.5 | 29.5 | 29.5 | 29.5 | 10.5 | 27.6 | 10.5 | 27.6 | 27.6 |
| Total Split (s) | 30.0 | 30.0 | 30.0 | 30.0 | 20.0 | 60.0 | 11.0 | 60.0 | 60.0 |
| Total Split (\%) | 27.3\% | 27.3\% | 27.3\% | 27.3\% | 18.2\% | 54.5\% | 10.0\% | 54.5\% | 54.5\% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.6 | 3.5 | 3.6 | 3.6 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.6 | 4.5 | 4.6 | 4.6 |
| Lead/Lag |  |  |  |  | Lead | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? |  |  |  |  | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | Min | None | Min | Min |
| Act Effct Green (s) | 27.0 | 27.0 | 27.0 | 27.0 | 9.3 | 50.9 | 6.5 | 41.9 | 41.9 |
| Actuated g/C Ratio | 0.30 | 0.30 | 0.30 | 0.30 | 0.10 | 0.57 | 0.07 | 0.47 | 0.47 |
| v/c Ratio | 1.23 | 0.14 | 0.01 | 0.06 | 0.39 | 0.62 | 0.08 | 0.89 | 0.33 |
| Control Delay | 158.6 | 16.3 | 30.8 | 15.7 | 49.3 | 15.2 | 49.8 | 45.4 | 4.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 158.6 | 16.3 | 30.8 | 15.7 | 49.3 | 15.2 | 49.8 | 45.4 | 4.6 |
| LOS | F | B | C | B | D | B | D | D | A |
| Approach Delay |  | 140.6 |  | 18.1 |  | 18.6 |  | 34.3 |  |
| Approach LOS |  | F |  | B |  | B |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |
| Cycle Length: 110 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 89.3 |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 100 |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Uncoordinated |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.23 |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 59.8 |  |  |  | Intersection LOS: E |  |  |  |  |  |
| Intersection Capacity Utilization 86.0\% |  |  |  | ICU Level of Service E |  |  |  |  |  |

Analysis Period (min) 15
Splits and Phases: 3: SR 3 \& NE Clifton Lane/Rite Aid Driveway


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 4.7 | 4.7 |  |  |  |  |  |
| Movement E | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 「' | ${ }^{*}$ | 4 | $\hat{\dagger}$ |  |
| Traffic Vol, veh/h | 10 | 260 | 195 | 640 | 400 | 15 |
| Future Vol, veh/h | 10 | 260 | 195 | 640 | 400 | 15 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control Stop | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None |  | None |
| Storage Length 300 | 300 | 0 | 100 | - | - | - |
| Veh in Median Storage, \# |  | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 88 | 88 | 88 | 88 | 88 | 88 |
| Heavy Vehicles, \% | 9 | 9 | 3 | 3 | 7 | 7 |
| Mvmt Flow | 11 | 295 | 222 | 727 | 455 | 17 |


| Major/Minor | Minor2 | Major1 |  |  | Major2 |  |
| :--- | ---: | ---: | ---: | :--- | :--- | :--- |
| Conflicting Flow All | 1635 | 464 | 472 | 0 | - | 0 |
| $\quad$ Stage 1 | 464 | - | - | - | - | - |
| $\quad$ Stage 2 | 1171 | - | - | - | - | - |
| Critical Hdwy | 6.49 | 6.29 | 4.13 | - | - | - |
| Critical Hdwy Stg 1 | 5.49 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.49 | - | - | - | - | - |
| Follow-up Hdwy | 3.581 | 3.381 | 2.227 | - | - | - |
| Pot Cap-1 Maneuver | 107 | 584 | 1085 | - | - | - |
| $\quad$ Stage 1 | 619 | - | - | - | - | - |
| Stage 2 | 285 | - | - | - | - | - |

Platoon blocked, \%
Mov Cap-1 Maneuver $85 \quad 5841085$

| Mov Cap-2 Maneuver | 56 | - | - | - | - | - |
| :---: | ---: | ---: | ---: | ---: | ---: | :--- |
| Stage 1 | 492 | - | - | - | - | - |
| Stage 2 | 285 | - | - | - | - | - |


| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 19.8 | 2.1 | 0 |
| HCM LOS | C |  |  |


| Minor Lane/Major Mvmt | NBL | NBTEBLn1EBLn2 | SBT | SBR |  |  |
| :--- | ---: | ---: | ---: | ---: | :--- | :--- |
| Capacity (veh/h) | 1085 | - | 56 | 584 | - | - |
| HCM Lane V/C Ratio | 0.204 | -0.203 | 0.506 | - | - |  |
| HCM Control Delay (s) | 9.2 | - | 85 | 17.3 | - | - |
| HCM Lane LOS | A | - | F | C | - | - |
| HCM 95th \%tile Q(veh) | 0.8 | - | 0.7 | 2.8 | - | - |


| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | 「 | ${ }^{*}$ | 4 | 4 | 「 |
| Traffic Volume (vph) | 260 | 75 | 15 | 595 | 475 | 110 |
| Future Volume (vph) | 260 | 75 | 15 | 595 | 475 | 110 |
| Turn Type | Prot | Perm | Prot | NA | NA | $\mathrm{pm}+\mathrm{ov}$ |
| Protected Phases | 4 |  | 5 | 2 | 6 | 4 |
| Permitted Phases |  | 4 |  |  |  | 6 |
| Detector Phase | 4 | 4 | 5 | 2 | 6 | 4 |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial (s) | 10.0 | 10.0 | 6.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split (s) | 27.7 | 27.7 | 11.7 | 22.5 | 40.7 | 27.7 |
| Total Split (s) | 50.0 | 50.0 | 40.0 | 50.0 | 50.0 | 50.0 |
| Total Split (\%) | 35.7\% | 35.7\% | 28.6\% | 35.7\% | 35.7\% | 35.7\% |
| Yellow Time (s) | 3.9 | 3.9 | 4.7 | 4.7 | 4.7 | 3.9 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.9 | 4.9 | 5.7 | 5.7 | 5.7 | 4.9 |
| Lead/Lag |  |  | Lead |  | Lag |  |
| Lead-Lag Optimize? |  |  | Yes |  | Yes |  |
| Recall Mode | None | None | None | Min | Min | None |
| Act Effct Green (s) | 20.3 | 20.3 | 6.7 | 47.7 | 43.4 | 73.0 |
| Actuated g/C Ratio | 0.26 | 0.26 | 0.08 | 0.60 | 0.55 | 0.92 |
| v/c Ratio | 0.73 | 0.20 | 0.13 | 0.67 | 0.61 | 0.10 |
| Control Delay | 38.5 | 7.1 | 41.4 | 15.3 | 19.1 | 0.5 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 38.5 | 7.1 | 41.4 | 15.3 | 19.1 | 0.5 |
| LOS | D | A | D | B | B | A |
| Approach Delay | 31.5 |  |  | 16.0 | 15.6 |  |
| Approach LOS | C |  |  | B | B |  |

## Intersection Summary

Cycle Length: 140
Actuated Cycle Length: 79
Natural Cycle: 85
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.73
Intersection Signal Delay: 19.2 Intersection LOS: B
Intersection Capacity Utilization $57.1 \% \quad$ ICU Level of Service B
Analysis Period (min) 15
Splits and Phases: 5: SR 3 \& SR 106


3: SR 3 \& NE Clifton Lane/Rite Aid Driveway

| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | $\hat{F}$ | ${ }^{*}$ | $\hat{\beta}$ | ${ }^{*}$ | $\uparrow$ | ${ }^{*}$ | 4 | 「 |
| Traffic Volume (vph) | 335 | 20 | 15 | 25 | 95 | 370 | 5 | 620 | 430 |
| Future Volume (vph) | 335 | 20 | 15 | 25 | 95 | 370 | 5 | 620 | 430 |
| Turn Type | Perm | NA | Perm | NA | Prot | NA | Prot | NA | Perm |
| Protected Phases |  | 8 |  | 4 | 5 | 2 | 1 | 6 |  |
| Permitted Phases | 8 |  | 4 |  |  |  |  |  | 6 |
| Detector Phase | 8 | 8 | 4 | 4 | 5 | 2 | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 10.0 | 6.0 | 10.0 | 10.0 |
| Minimum Split (s) | 29.5 | 29.5 | 29.5 | 29.5 | 10.5 | 27.6 | 10.5 | 27.6 | 27.6 |
| Total Split (s) | 30.0 | 30.0 | 30.0 | 30.0 | 20.0 | 60.0 | 11.0 | 60.0 | 60.0 |
| Total Split (\%) | 27.3\% | 27.3\% | 27.3\% | 27.3\% | 18.2\% | 54.5\% | 10.0\% | 54.5\% | 54.5\% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.6 | 3.5 | 3.6 | 3.6 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.6 | 4.5 | 4.6 | 4.6 |
| Lead/Lag |  |  |  |  | Lead | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? |  |  |  |  | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | Min | None | Min | Min |
| Act Effct Green (s) | 25.5 | 25.5 | 25.5 | 25.5 | 11.8 | 69.6 | 6.2 | 55.4 | 55.4 |
| Actuated g/C Ratio | 0.24 | 0.24 | 0.24 | 0.24 | 0.11 | 0.65 | 0.06 | 0.52 | 0.52 |
| v/c Ratio | 1.29 | 0.42 | 0.09 | 0.10 | 0.60 | 0.39 | 0.11 | 1.43 | 0.76 |
| Control Delay | 188.0 | 9.9 | 34.3 | 25.9 | 58.8 | 10.3 | 53.4 | 229.1 | 10.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 188.0 | 9.9 | 34.3 | 25.9 | 58.8 | 10.3 | 53.4 | 229.1 | 10.3 |
| LOS | F | A | C | C | E | B | D | F | B |
| Approach Delay |  | 125.7 |  | 28.4 |  | 20.0 |  | 139.1 |  |
| Approach LOS |  | F |  | C |  | B |  | F |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |
| Cycle Length: 110 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 106.4 |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 150 |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Uncoordinated |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.43 |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 106.1 |  |  |  | Intersection LOS: F |  |  |  |  |  |
| Intersection Capacity Utilization 105.1\% |  |  |  | ICU Level of Service G |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |

Splits and Phases: 3: SR 3 \& NE Clifton Lane/Rite Aid Driveway


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 43 |  |  |  |  |  |
| Movement EBL | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations |  | 「 | ${ }^{7}$ | 4 | $\uparrow$ |  |
| Traffic Vol, veh/h |  | 385 | 265 | 490 | 890 | 20 |
| Future Vol, veh/h | 5 | 385 | 265 | 490 | 890 | 20 |
| Conflicting Peds, \#/hr |  | 2 | 2 | 0 | 0 | 2 |
| Sign Control Stop |  | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length 300 | 300 | 0 | 100 | - | - | - |
| Veh in Median Storage, \# |  | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 93 | 93 | 93 | 93 | 93 | 93 |
| Heavy Vehicles, \% |  | 4 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 5 | 414 | 285 | 527 | 957 | 22 |


| Major/Minor | Minor2 | Major1 | Major2 |  |  |  |
| :--- | ---: | ---: | ---: | ---: | :--- | :--- |
| Conflicting Flow All | 2069 | 972 | 981 | 0 | - | 0 |
| $\quad$ Stage 1 | 970 | - | - | - | - | - |
| $\quad$ Stage 2 | 1099 | - | - | - | - | - |
| Critical Hdwy | 6.44 | 6.24 | 4.12 | - | - | - |
| Critical Hdwy Stg 1 | 5.44 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.44 | - | - | - | - | - |
| Follow-up Hdwy | 3.536 | 3.336 | 2.218 | - | - | - |
| Pot Cap-1 Maneuver | 59 | $\sim 304$ | 704 | - | - | - |
| $\quad$ Stage 1 | 365 | - | - | - | - | - |
| Stage 2 | 316 | - | - | - | - | - |

Platoon blocked, \%
Mov Cap-1 Maneuver 35 ~ 303703
Mov Cap-2 Maneuver

| Stage 1 | 217 |
| :--- | :--- |
| Stage | 315 |


| Approach | EB | NB |
| :--- | ---: | :---: |
| HCM Control Delay, s217.4 | 4.8 | 0 |
| HCM LOS | F |  |


| Minor Lane/Major Mvmt | NBL | NBTEBLn1EBLn2 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 703 | - | 27 | 303 | - |
| HCM Lane V/C Ratio | 0.405 | -0.199 | 1.366 | - | - |
| HCM Control Delay (s) | 13.6 | -168.9 | 218 | - | - |
| HCM Lane LOS | B | - | F | F | - |
| HCM 95th \%tile Q(veh) | 2 | - | 0.6 | 21.2 | - |

Notes
$\sim$ : Volume exceeds capacity $\$$ : Delay exceeds 300s + : Computation Not Defined $\quad$ : All major volume in platoon

| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | 「 | \％ | 个 | 4 | 「゙ |
| Traffic Volume（vph） | 180 | 40 | 55 | 460 | 985 | 440 |
| Future Volume（vph） | 180 | 40 | 55 | 460 | 985 | 440 |
| Turn Type | Prot | Perm | Prot | NA | NA | pm＋ov |
| Protected Phases | 4 |  | 5 | 2 | 6 | 4 |
| Permitted Phases |  | 4 |  |  |  | 6 |
| Detector Phase | 4 | 4 | 5 | 2 | 6 | 4 |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial（s） | 10.0 | 10.0 | 6.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split（s） | 27.7 | 27.7 | 11.7 | 22.5 | 40.7 | 27.7 |
| Total Split（s） | 50.0 | 50.0 | 40.0 | 50.0 | 30.0 | 50.0 |
| Total Split（\％） | 41．7\％ | 41．7\％ | 33．3\％ | 41．7\％ | 25．0\％ | 41．7\％ |
| Yellow Time（s） | 3.9 | 3.9 | 4.7 | 4.7 | 4.7 | 3.9 |
| All－Red Time（s） | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 4.9 | 4.9 | 5.7 | 5.7 | 5.7 | 4.9 |
| Lead／Lag |  |  | Lead |  | Lag |  |
| Lead－Lag Optimize？ |  |  | Yes |  | Yes |  |
| Recall Mode | None | None | None | Min | Min | None |
| Act Effct Green（s） | 12.6 | 12.6 | 7.5 | 32.5 | 25.0 | 38.4 |
| Actuated g／C Ratio | 0.22 | 0.22 | 0.13 | 0.58 | 0.45 | 0.69 |
| v／c Ratio | 0.48 | 0.11 | 0.24 | 0.45 | 1.26 | 0.39 |
| Control Delay | 25.4 | 8.2 | 27.5 | 8.5 | 149.6 | 2.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 25.4 | 8.2 | 27.5 | 8.5 | 149.6 | 2.0 |
| LOS | C | A | C | A | F | A |
| Approach Delay | 22.3 |  |  | 10.5 | 104.0 |  |
| Approach LOS | C |  |  | B | F |  |

## Intersection Summary

Cycle Length： 120
Actuated Cycle Length： 56
Natural Cycle： 105
Control Type：Actuated－Uncoordinated
Maximum v／c Ratio： 1.26

| Intersection Signal Delay： 73.4 | Intersection LOS：E |
| :--- | :--- |
| Intersection Capacity Utilization $74.1 \%$ | ICU Level of Service D |

Analysis Period（min） 15
Splits and Phases：5：SR 3 \＆SR 106


| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | $\uparrow$ | \% | $\uparrow$ | ${ }^{*}$ | $\uparrow$ | ${ }^{*}$ | 4 | 「 |
| Traffic Volume (vph) | 465 | 25 | 5 | 5 | 65 | 240 | 5 | 220 | 145 |
| Future Volume (vph) | 465 | 25 | 5 | 5 | 65 | 240 | 5 | 220 | 145 |
| Turn Type | Perm | NA | Perm | NA | Prot | NA | Prot | NA | Perm |
| Protected Phases |  | 8 |  | 4 | 5 | 2 | 1 | 6 |  |
| Permitted Phases | 8 |  | 4 |  |  |  |  |  | 6 |
| Detector Phase | 8 | 8 | 4 | 4 | 5 | 2 | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 10.0 | 6.0 | 10.0 | 10.0 |
| Minimum Split (s) | 29.5 | 29.5 | 29.5 | 29.5 | 10.5 | 27.6 | 10.5 | 27.6 | 27.6 |
| Total Split (s) | 30.0 | 30.0 | 30.0 | 30.0 | 20.0 | 60.0 | 11.0 | 60.0 | 60.0 |
| Total Split (\%) | 27.3\% | 27.3\% | 27.3\% | 27.3\% | 18.2\% | 54.5\% | 10.0\% | 54.5\% | 54.5\% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.6 | 3.5 | 3.6 | 3.6 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.6 | 4.5 | 4.6 | 4.6 |
| Lead/Lag |  |  |  |  | Lead | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? |  |  |  |  | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | Min | None | Min | Min |
| Act Effct Green (s) | 26.8 | 26.8 | 26.8 | 26.8 | 8.5 | 31.3 | 6.4 | 23.0 | 23.0 |
| Actuated g/C Ratio | 0.39 | 0.39 | 0.39 | 0.39 | 0.12 | 0.45 | 0.09 | 0.33 | 0.33 |
| v/c Ratio | 1.01 | 0.11 | 0.01 | 0.04 | 0.33 | 0.33 | 0.06 | 0.75 | 0.43 |
| Control Delay | 72.5 | 11.3 | 20.6 | 11.1 | 36.8 | 12.7 | 37.8 | 37.0 | 7.1 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 72.5 | 11.3 | 20.6 | 11.1 | 36.8 | 12.7 | 37.8 | 37.0 | 7.1 |
| LOS | E | B | C | B | D | B | D | D | A |
| Approach Delay |  | 65.0 |  | 12.6 |  | 17.7 |  | 25.2 |  |
| Approach LOS |  | E |  | B |  | B |  | C |  |

## Intersection Summary

Cycle Length: 110
Actuated Cycle Length: 69.4
Natural Cycle: 80
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 1.01

| Intersection Signal Delay: 40.1 | Intersection LOS: D |
| :--- | :--- |
| Intersection Capacity Utilization $72.2 \%$ | ICU Level of Service C |

Analysis Period (min) 15
Splits and Phases: 3: SR 3 \& NE Clifton Lane/Rite Aid Driveway


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 5.2 | 5.2 |  |  |  |  |  |
| Movement E | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | 「 | ${ }^{7}$ | 4 | $\uparrow$ |  |
| Traffic Vol, veh/h | 10 | 260 | 195 | 300 | 250 | 15 |
| Future Vol, veh/h | 10 | 260 | 195 | 300 | 250 | 15 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control Stop | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length 300 | 300 | 0 | 100 | - | - | - |
| Veh in Median Storage, \# | \# 1 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 88 | 88 | 88 | 88 | 88 | 88 |
| Heavy Vehicles, \% | 9 | 9 | 3 | 3 | 7 | 7 |
| Mvmt Flow | 11 | 295 | 222 | 341 | 284 | 17 |



| Minor Lane/Major Mvmt | NBL | NBTEBLn1EBLn2 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 1254 | - | 195 | 730 | - |
| HCM Lane V/C Ratio | 0.177 | -0.058 | 0.405 | - | - |
| HCM Control Delay (s) | 8.5 | -24.6 | 13.2 | - | - |
| HCM Lane LOS | A | - | C | B | - |
| HCM 95th \%tile Q(veh) | 0.6 | - | 0.2 | 2 | - |


| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | * | 7 | \% | 4 | 4 | F |
| Traffic Volume (vph) | 270 | 75 | 15 | 250 | 325 | 110 |
| Future Volume (vph) | 270 | 75 | 15 | 250 | 325 | 110 |
| Turn Type | Prot | Perm | Prot | NA | NA | $\mathrm{pm}+0 \mathrm{v}$ |
| Protected Phases | 4 |  | 5 | 2 | 6 | 4 |
| Permitted Phases |  | 4 |  |  |  | 6 |
| Detector Phase | 4 | 4 | 5 | 2 | 6 | 4 |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial (s) | 10.0 | 10.0 | 6.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split (s) | 27.7 | 27.7 | 11.7 | 22.5 | 40.7 | 27.7 |
| Total Split (s) | 50.0 | 50.0 | 40.0 | 50.0 | 50.0 | 50.0 |
| Total Split (\%) | 35.7\% | 35.7\% | 28.6\% | 35.7\% | 35.7\% | 35.7\% |
| Yellow Time (s) | 3.9 | 3.9 | 4.7 | 4.7 | 4.7 | 3.9 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.9 | 4.9 | 5.7 | 5.7 | 5.7 | 4.9 |
| Lead/Lag |  |  | Lead |  | Lag |  |
| Lead-Lag Optimize? |  |  | Yes |  | Yes |  |
| Recall Mode | None | None | None | Min | Min | None |
| Act Effct Green (s) | 19.5 | 19.5 | 7.4 | 24.6 | 20.9 | 51.4 |
| Actuated g/C Ratio | 0.35 | 0.35 | 0.13 | 0.44 | 0.37 | 0.91 |
| v/c Ratio | 0.57 | 0.16 | 0.08 | 0.39 | 0.62 | 0.10 |
| Control Delay | 22.3 | 5.7 | 33.5 | 12.2 | 21.9 | 0.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 22.3 | 5.7 | 33.5 | 12.2 | 21.9 | 0.6 |
| LOS | C | A | C | B | C | A |
| Approach Delay | 18.7 |  |  | 13.4 | 16.5 |  |
| Approach LOS | B |  |  | B | B |  |

## Intersection Summary

Cycle Length: 140
Actuated Cycle Length: 56.4
Natural Cycle: 85
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.62
Intersection Signal Delay: 16.5 Intersection LOS: B
Intersection Capacity Utilization 42.7\% ICU Level of Service A
Analysis Period (min) 15
Splits and Phases: 5: SR 3 \& SR 106


Timings

|  | $\rangle$ | $\rightarrow$ | 7 | 7 |  |  | 4 | $\dagger$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | $\hat{\beta}$ |  | \% | $\hat{\beta}$ |  | \% | $\uparrow$ |  | \% | 4 | F |
| Trafic Volume (vph) | 335 | 20 | 160 | 15 | 25 | 10 | 95 | 160 | 10 | 5 | 350 | 430 |
| Future Volume (vph) | 335 | 20 | 160 | 15 | 25 | 10 | 95 | 160 | 10 | 5 | 350 | 430 |
| Satd. Flow (prot) | 1660 | 1515 | 0 | 1710 | 1721 | 0 | 1676 | 1749 | 0 | 931 | 980 | 833 |
| FIt Permitted | 0.730 |  |  | 0.509 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (perm) | 1276 | 1515 | 0 | 916 | 1721 | 0 | 1674 | 1749 | 0 | 931 | 980 | 815 |
| Satd. Flow (RTOR) |  | 188 |  |  | 12 |  |  | 5 |  |  |  | 506 |
| Lane Group Flow (vph) | 394 | 212 | 0 | 18 | 41 | 0 | 112 | 200 | 0 | 6 | 412 | 506 |
| Turn Type | Perm | NA |  | Perm | NA |  | Prot | NA |  | Prot | NA | Perm |
| Protected Phases |  | 8 |  |  | 4 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 8 |  |  | 4 |  |  |  |  |  |  |  | 6 |
| Detector Phase | 8 | 8 |  | 4 | 4 |  | 5 | 2 |  | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 6.0 | 6.0 |  | 6.0 | 6.0 |  | 6.0 | 10.0 |  | 6.0 | 10.0 | 10.0 |
| Minimum Split (s) | 29.5 | 29.5 |  | 29.5 | 29.5 |  | 10.5 | 27.6 |  | 10.5 | 27.6 | 27.6 |
| Total Split (s) | 30.0 | 30.0 |  | 30.0 | 30.0 |  | 20.0 | 60.0 |  | 11.0 | 60.0 | 60.0 |
| Total Split (\%) | 27.3\% | 27.3\% |  | 27.3\% | 27.3\% |  | 18.2\% | 54.5\% |  | 10.0\% | 54.5\% | 54.5\% |
| Yellow Time (s) | 3.5 | 3.5 |  | 3.5 | 3.5 |  | 3.5 | 3.6 |  | 3.5 | 3.6 | 3.6 |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.5 | 4.5 |  | 4.5 | 4.5 |  | 4.5 | 4.6 |  | 4.5 | 4.6 | 4.6 |
| Lead/Lag |  |  |  |  |  |  | Lead | Lag |  | Lead | Lag | Lag |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes |  | Yes | Yes | Yes |
| Recall Mode | None | None |  | None | None |  | None | Min |  | None | Min | Min |
| Act Effct Green (s) | 26.7 | 26.7 |  | 26.7 | 26.7 |  | 11.5 | 56.3 |  | 6.5 | 45.4 | 45.4 |
| Actuated g/C Ratio | 0.28 | 0.28 |  | 0.28 | 0.28 |  | 0.12 | 0.60 |  | 0.07 | 0.48 | 0.48 |
| v/c Ratio | 1.09 | 0.38 |  | 0.07 | 0.08 |  | 0.55 | 0.19 |  | 0.10 | 0.87 | 0.77 |
| Control Delay | 112.3 | 9.5 |  | 33.1 | 25.2 |  | 53.6 | 8.6 |  | 52.0 | 43.9 | 11.1 |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Delay | 112.3 | 9.5 |  | 33.1 | 25.2 |  | 53.6 | 8.6 |  | 52.0 | 43.9 | 11.1 |
| LOS | F | A |  | C | C |  | D | A |  | D | D | B |
| Approach Delay |  | 76.3 |  |  | 27.6 |  |  | 24.8 |  |  | 26.0 |  |
| Approach LOS |  | E |  |  | C |  |  | C |  |  | C |  |

## Intersection Summary

Cycle Length: 110
Actuated Cycle Length: 94.4
Natural Cycle: 90
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 1.09
Intersection Signal Delay: 41.9
Intersection LOS: D
Intersection Capacity Utilization 78.1\%
ICU Level of Service D
Analysis Period (min) 15
Splits and Phases: 3: SR 3 \& NE Clifton Lane/Rite Aid Driveway


5: SR 3 \& SR 106

|  | 4 |  | 4 | $\dagger$ | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | \% | 「 | ${ }^{4}$ | 4 | 4 | 「 |
| Trafic Volume (vph) | 180 | 40 | 55 | 255 | 710 | 440 |
| Future Volume (vph) | 180 | 40 | 55 | 255 | 710 | 440 |
| Satd. Flow (prot) | 1660 | 1485 | 1676 | 1765 | 1748 | 1485 |
| Flt Permitted | 0.950 |  | 0.950 |  |  |  |
| Satd. Flow (perm) | 1660 | 1485 | 1675 | 1765 | 1748 | 1452 |
| Satd. Flow (RTOR) |  | 40 |  |  |  | 440 |
| Lane Group Flow (vph) | 180 | 40 | 55 | 255 | 710 | 440 |
| Turn Type | Prot | Perm | Prot | NA | NA | pm+ov |
| Protected Phases | 4 |  | 5 | 2 | 6 | 4 |
| Permitted Phases |  | 4 |  |  |  | 6 |
| Detector Phase | 4 | 4 | 5 | 2 | 6 | 4 |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial (s) | 10.0 | 10.0 | 6.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split (s) | 27.7 | 27.7 | 11.7 | 22.5 | 40.7 | 27.7 |
| Total Split (s) | 50.0 | 50.0 | 40.0 | 50.0 | 30.0 | 50.0 |
| Total Split (\%) | 41.7\% | 41.7\% | 33.3\% | 41.7\% | 25.0\% | 41.7\% |
| Yellow Time (s) | 3.9 | 3.9 | 4.7 | 4.7 | 4.7 | 3.9 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.9 | 4.9 | 5.7 | 5.7 | 5.7 | 4.9 |
| Lead/Lag |  |  | Lead |  | Lag |  |
| Lead-Lag Optimize? |  |  | Yes |  | Yes |  |
| Recall Mode | None | None | None | Min | Min | None |
| Act Effct Green (s) | 12.5 | 12.5 | 7.5 | 32.5 | 25.0 | 38.3 |
| Actuated g/C Ratio | 0.22 | 0.22 | 0.13 | 0.58 | 0.45 | 0.69 |
| $\mathrm{v} / \mathrm{c}$ Ratio | 0.49 | 0.11 | 0.24 | 0.25 | 0.91 | 0.39 |
| Control Delay | 25.5 | 8.2 | 27.5 | 6.6 | 37.4 | 1.5 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 25.5 | 8.2 | 27.5 | 6.6 | 37.4 | 1.5 |
| LOS | C | A | C | A | D | A |
| Approach Delay | 22.4 |  |  | 10.3 | 23.7 |  |
| Approach LOS | C |  |  | B | C |  |
| Intersection Summary |  |  |  |  |  |  |
| Cycle Length: 120 |  |  |  |  |  |  |
| Actuated Cycle Length: 55.9 |  |  |  |  |  |  |
| Natural Cycle: 85 |  |  |  |  |  |  |
| Control Type: Actuated-Uncoordinated |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.91 |  |  |  |  |  |  |
| Intersection Signal Delay: 21.0 |  |  |  | Intersection LOS: C |  |  |
| Intersection Capacity Utilization 67.6\% |  |  |  | ICU Level of Service C |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |
| Splits and Phases: 5: SR 3 \& SR 106 |  |  |  |  |  |  |
| 402 |  |  |  |  |  | ${ }^{14} 04$ |
| 505 |  |  |  |  |  | OE |
| 405 |  |  | $\pm \boxed{\square}$ |  |  |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 16.1 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | 1 | $\mathbf{r}$ |  | $\mathbf{4}$ | $\mathbf{b}$ |  |
| Traffic Vol, veh/h | 5 | 385 | 265 | 285 | 620 | 20 |
| Future Vol, veh/h | 5 | 385 | 265 | 285 | 620 | 20 |
| Conflicting Peds, \#/hr | 2 | 2 | 2 | 0 | 0 | 2 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 300 | 0 | 100 | - | - | - |
| Veh in Median Storage, \# | 1 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 93 | 93 | 93 | 93 | 93 | 93 |
| Heavy Vehicles, \% | 4 | 4 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 5 | 414 | 285 | 306 | 667 | 22 |



| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 57.7 | 5.2 | 0 |
| HCM LOS | F |  |  |


| Minor Lane/Major Mvmt | NBL | NBT EBLn1 EBLn2 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 902 | -206 | 444 | - | - |
| HCM Lane V/C Ratio | 0.316 | -0.026 | 0.932 | - | - |
| HCM Control Delay (s) | 10.8 | -22.9 | 58.2 | - | - |
| HCM Lane LOS | B | - | C | F | - |
| HCM 95th \%tile Q(veh) | 1.4 | - | 0.1 | 10.7 | - |

3: SR 3 \& NE Clifton Lane/Rite Aid Driveway

| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | * | $\uparrow$ | \% | $\uparrow$ | * | $\uparrow$ | ${ }^{7}$ | 4 | F |
| Traffic Volume (vph) | 540 | 30 | 5 | 10 | 75 | 790 | 5 | 495 | 170 |
| Future Volume (vph) | 540 | 30 | 5 | 10 | 75 | 790 | 5 | 495 | 170 |
| Turn Type | Perm | NA | Perm | NA | Prot | NA | Prot | NA | Perm |
| Protected Phases |  | 8 |  | 4 | 5 | 2 | 1 | 6 |  |
| Permitted Phases | 8 |  | 4 |  |  |  |  |  | 6 |
| Detector Phase | 8 | 8 | 4 | 4 | 5 | 2 | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 10.0 | 6.0 | 10.0 | 10.0 |
| Minimum Split (s) | 29.5 | 29.5 | 29.5 | 29.5 | 10.5 | 27.6 | 10.5 | 27.6 | 27.6 |
| Total Split (s) | 30.0 | 30.0 | 30.0 | 30.0 | 20.0 | 60.0 | 11.0 | 60.0 | 60.0 |
| Total Split (\%) | 27.3\% | 27.3\% | 27.3\% | 27.3\% | 18.2\% | 54.5\% | 10.0\% | 54.5\% | 54.5\% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.6 | 3.5 | 3.6 | 3.6 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.6 | 4.5 | 4.6 | 4.6 |
| Lead/Lag |  |  |  |  | Lead | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? |  |  |  |  | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | Min | None | Min | Min |
| Act Effct Green (s) | 25.6 | 25.6 | 25.6 | 25.6 | 10.0 | 65.8 | 6.2 | 55.7 | 55.7 |
| Actuated g/C Ratio | 0.25 | 0.25 | 0.25 | 0.25 | 0.10 | 0.64 | 0.06 | 0.54 | 0.54 |
| v/c Ratio | 1.83 | 0.20 | 0.02 | 0.09 | 0.49 | 0.75 | 0.09 | 1.03 | 0.36 |
| Control Delay | 412.1 | 16.5 | 31.8 | 16.7 | 54.8 | 18.8 | 52.0 | 74.0 | 4.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 412.1 | 16.5 | 31.8 | 16.7 | 54.8 | 18.8 | 52.0 | 74.0 | 4.4 |
| LOS | F | B | C | B | D | B | D | E | A |
| Approach Delay |  | 360.6 |  | 18.5 |  | 21.9 |  | 56.2 |  |
| Approach LOS |  | F |  | B |  | C |  | E |  |

## Intersection Summary

Cycle Length: 110
Actuated Cycle Length: 102.6
Natural Cycle: 150
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 1.83

| Intersection Signal Delay: 127.8 | Intersection LOS: F |
| :--- | :--- |
| Intersection Capacity Utilization 104.1\% | ICU Level of Service G |
| Analysis Period (min) 15 |  |

Splits and Phases: 3: SR 3 \& NE Clifton Lane/Rite Aid Driveway


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 12 | 1.2 |  |  |  |  |  |
| Movement E | BL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 「' | ${ }^{7}$ | 4 | 个 |  |
| Traffic Vol, veh/h | 10 | 300 | 225 | 870 | 535 | 15 |
| Future Vol, veh/h | 10 | 300 | 225 | 870 | 535 | 15 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control Stop | top | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None |  | None |
| Storage Length 300 | 300 | 0 | 100 | - | - | - |
| Veh in Median Storage, \# |  | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 88 | 88 | 88 | 88 | 88 | 88 |
| Heavy Vehicles, \% | 9 | 9 | 3 | 3 | 7 | 7 |
| Mvmt Flow | 11 | 341 | 256 | 989 | 608 | 17 |


| Major/Minor | Minor2 | Major1 | Major2 |  |  |  |
| :--- | ---: | ---: | ---: | ---: | :--- | :--- |
| Conflicting Flow All | 2118 | 617 | 625 | 0 | - | 0 |
| $\quad$ Stage 1 | 617 | - | - | - | - | - |
| $\quad$ Stage 2 | 1501 | - | - | - | - | - |
| Critical Hdwy | 6.49 | 6.29 | 4.13 | - | - | - |
| Critical Hdwy Stg 1 | 5.49 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.49 | - | - | - | - | - |
| Follow-up Hdwy | 3.581 | 3.381 | 2.227 | - | - | - |
| Pot Cap-1 Maneuver | 53 | 477 | 952 | - | - | - |
| $\quad$ Stage 1 | 525 | - | - | - | - | - |
| Stage 2 | 196 | - | - | - | - | - |

Platoon blocked, \%
Mov Cap-1 Maneuver $39 \quad 477 \quad 952$

Mov Cap-2 Maneuver ~ -91
Stage $1 \quad 384$

Stage 2196

| Approach | EB | NB | SB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | - | 2.1 | 0 |
| HCM LOS | - |  |  |


| Minor Lane/Major Mvmt | NBL | NBTEBLn1EBLn2 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 952 | - | +477 | - | - |
| HCM Lane V/C Ratio | 0.269 | - | -0.715 | - | - |
| HCM Control Delay (s) | 10.2 | - | -29.3 | - | - |
| HCM Lane LOS | B | - | - | D | - |
| HCM 95th \%tile Q(veh) | 1.1 | - | - | 5.6 | - |

Notes
~: Volume exceeds capacity $\$$ : Delay exceeds 300s + : Computation Not Defined $\quad$ : All major volume in platoon

| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | 「 | ${ }^{7}$ | 4 | 4 | 「' |
| Traffic Volume (vph) | 310 | 90 | 15 | 805 | 625 | 130 |
| Future Volume (vph) | 310 | 90 | 15 | 805 | 625 | 130 |
| Turn Type | Prot | Perm | Prot | NA | NA | pm+ov |
| Protected Phases | 4 |  | 5 | 2 | 6 | 4 |
| Permitted Phases |  | 4 |  |  |  | 6 |
| Detector Phase | 4 | 4 | 5 | 2 | 6 | 4 |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial (s) | 10.0 | 10.0 | 6.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split (s) | 27.7 | 27.7 | 11.7 | 22.5 | 40.7 | 27.7 |
| Total Split (s) | 50.0 | 50.0 | 40.0 | 50.0 | 50.0 | 50.0 |
| Total Split (\%) | 35.7\% | 35.7\% | 28.6\% | 35.7\% | 35.7\% | 35.7\% |
| Yellow Time (s) | 3.9 | 3.9 | 4.7 | 4.7 | 4.7 | 3.9 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.9 | 4.9 | 5.7 | 5.7 | 5.7 | 4.9 |
| Lead/Lag |  |  | Lead |  | Lag |  |
| Lead-Lag Optimize? |  |  | Yes |  | Yes |  |
| Recall Mode | None | None | None | Min | Min | None |
| Act Effct Green (s) | 23.9 | 23.9 | 6.8 | 50.0 | 45.5 | 78.7 |
| Actuated g/C Ratio | 0.28 | 0.28 | 0.08 | 0.59 | 0.54 | 0.93 |
| v/c Ratio | 0.80 | 0.22 | 0.14 | 0.93 | 0.82 | 0.12 |
| Control Delay | 42.0 | 6.1 | 44.5 | 34.3 | 30.1 | 0.5 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 42.0 | 6.1 | 44.5 | 34.3 | 30.1 | 0.5 |
| LOS | D | A | D | C | C | A |
| Approach Delay | 34.0 |  |  | 34.5 | 25.0 |  |
| Approach LOS | C |  |  | C | C |  |

## Intersection Summary

Cycle Length: 140
Actuated Cycle Length: 84.8
Natural Cycle: 85
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.93

| Intersection Signal Delay: 30.7 | Intersection LOS: C |
| :--- | :--- |
| Intersection Capacity Utilization $71.7 \%$ | ICU Level of Service C |

Analysis Period (min) 15
Splits and Phases: 5: SR 3 \& SR 106


3: SR 3 \& NE Clifton Lane/Rite Aid Driveway

| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | $\uparrow$ | \% | $\hat{\beta}$ | ${ }^{*}$ | $\uparrow$ | * | 4 | 「' |
| Traffic Volume (vph) | 465 | 20 | 20 | 25 | 110 | 515 | 10 | 895 | 600 |
| Future Volume (vph) | 465 | 20 | 20 | 25 | 110 | 515 | 10 | 895 | 600 |
| Turn Type | Perm | NA | Perm | NA | Prot | NA | Prot | NA | Perm |
| Protected Phases |  | 8 |  | 4 | 5 | 2 | 1 | 6 |  |
| Permitted Phases | 8 |  | 4 |  |  |  |  |  | 6 |
| Detector Phase | 8 | 8 | 4 | 4 | 5 | 2 | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 10.0 | 6.0 | 10.0 | 10.0 |
| Minimum Split (s) | 29.5 | 29.5 | 29.5 | 29.5 | 10.5 | 27.6 | 10.5 | 27.6 | 27.6 |
| Total Split (s) | 30.0 | 30.0 | 30.0 | 30.0 | 20.0 | 60.0 | 11.0 | 60.0 | 60.0 |
| Total Split (\%) | 27.3\% | 27.3\% | 27.3\% | 27.3\% | 18.2\% | 54.5\% | 10.0\% | 54.5\% | 54.5\% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.6 | 3.5 | 3.6 | 3.6 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.6 | 4.5 | 4.6 | 4.6 |
| Lead/Lag |  |  |  |  | Lead | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? |  |  |  |  | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | Min | None | Min | Min |
| Act Effct Green (s) | 25.5 | 25.5 | 25.5 | 25.5 | 12.6 | 70.4 | 6.3 | 55.5 | 55.5 |
| Actuated g/C Ratio | 0.24 | 0.24 | 0.24 | 0.24 | 0.12 | 0.66 | 0.06 | 0.52 | 0.52 |
| v/c Ratio | 1.81 | 0.46 | 0.14 | 0.11 | 0.65 | 0.54 | 0.22 | 2.08 | 0.94 |
| Control Delay | 405.7 | 9.7 | 36.0 | 23.8 | 61.2 | 12.6 | 59.1 | 513.4 | 25.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 405.7 | 9.7 | 36.0 | 23.8 | 61.2 | 12.6 | 59.1 | 513.4 | 25.7 |
| LOS | F | A | D | C | E | B | E | F | C |
| Approach Delay |  | 284.2 |  | 27.9 |  | 20.9 |  | 315.9 |  |
| Approach LOS |  | F |  | C |  | C |  | F |  |

## Intersection Summary

Cycle Length: 110
Actuated Cycle Length: 107.2
Natural Cycle: 150
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 2.08

| Intersection Signal Delay: 236.8 | Intersection LOS: F |
| :--- | :--- |
| Intersection Capacity Utilization 137.9\% | ICU Level of Service H |

Analysis Period (min) 15
Splits and Phases: 3: SR 3 \& NE Clifton Lane/Rite Aid Driveway



| Major/Minor | Minor2 | Major1 | Major2 |  |  |  |
| :--- | ---: | ---: | ---: | :--- | :--- | :--- |
| Conflicting Flow All | 2671 | 1311 | 1320 | 0 | - | 0 |
| $\quad$ Stage 1 | 1309 | - | - | - | - | - |
| $\quad$ Stage 2 | 1362 | - | - | - | - | - |
| Critical Hdwy | 6.44 | 6.24 | 4.12 | - | - | - |
| Critical Hdwy Stg 1 | 5.44 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.44 | - | - | - | - | - |
| Follow-up Hdwy | 3.536 | 3.336 | 2.218 | - | - | - |
| Pot Cap-1 Maneuver | 24 | $\sim 192$ | 524 | - | - | - |
| $\quad$ Stage 1 | 250 | - | - | - | - | - |
| Stage 2 | 236 | - | - | - | - | - |

Platoon blocked, \%
Mov Cap-1 Maneuver $\quad 9 \sim 191 \quad 523$

Mov Cap-2 Maneuver 465
Stage $1 \quad 93$
Stage $2 \quad 236$

| Approach | EB | NB |
| :--- | ---: | :---: | SB 9


| Minor Lane/Major Mvmt | NBL | NBTEBLn1EBLn2 | SBT | SBR |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 523 | - | 465 | 191 | - | - |
| HCM Lane V/C Ratio | 0.627 | -0.012 | 2.505 | - | - |  |
| HCM Control Delay (s) | 22.8 | - | $12.8 \$ 731.2$ | - | - |  |
| HCM Lane LOS | C | - | B | F | - | - |
| HCM 95th \%tile Q(veh) | 4.3 | - | 0 | 40.4 | - | - |

Notes
$\sim$ : Volume exceeds capacity $\$$ : Delay exceeds 300s + : Computation Not Defined $\quad$ : All major volume in platoon

| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | 「 | ${ }^{7}$ | 4 | 4 | 「゙ |
| Traffic Volume（vph） | 235 | 45 | 60 | 595 | 1255 | 565 |
| Future Volume（vph） | 235 | 45 | 60 | 595 | 1255 | 565 |
| Turn Type | Prot | Perm | Prot | NA | NA | $\mathrm{pm}+0 \mathrm{v}$ |
| Protected Phases | 4 |  | 5 | 2 | 6 | 4 |
| Permitted Phases |  | 4 |  |  |  | 6 |
| Detector Phase | 4 | 4 | 5 | 2 | 6 | 4 |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial（s） | 10.0 | 10.0 | 6.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split（s） | 27.7 | 27.7 | 11.7 | 22.5 | 40.7 | 27.7 |
| Total Split（s） | 50.0 | 50.0 | 40.0 | 50.0 | 30.0 | 50.0 |
| Total Split（\％） | 41．7\％ | 41．7\％ | 33．3\％ | 41．7\％ | 25．0\％ | 41．7\％ |
| Yellow Time（s） | 3.9 | 3.9 | 4.7 | 4.7 | 4.7 | 3.9 |
| All－Red Time（s） | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 4.9 | 4.9 | 5.7 | 5.7 | 5.7 | 4.9 |
| Lead／Lag |  |  | Lead |  | Lag |  |
| Lead－Lag Optimize？ |  |  | Yes |  | Yes |  |
| Recall Mode | None | None | None | Min | Min | None |
| Act Effct Green（s） | 15.3 | 15.3 | 8.0 | 33.1 | 25.4 | 41.6 |
| Actuated g／C Ratio | 0.26 | 0.26 | 0.13 | 0.56 | 0.43 | 0.70 |
| v／c Ratio | 0.55 | 0.11 | 0.27 | 0.61 | 1.68 | 0.50 |
| Control Delay | 25.9 | 7.4 | 29.8 | 12.4 | 333.2 | 3.1 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 25.9 | 7.4 | 29.8 | 12.4 | 333.2 | 3.1 |
| LOS | C | A | C | B | F | A |
| Approach Delay | 22.9 |  |  | 14.0 | 230.7 |  |
| Approach LOS | C |  |  | B | F |  |

## Intersection Summary

Cycle Length： 120
Actuated Cycle Length： 59.5
Natural Cycle： 145
Control Type：Actuated－Uncoordinated
Maximum v／c Ratio： 1.68

| Intersection Signal Delay： 158.1 | Intersection LOS：F |
| :--- | :--- |
| Intersection Capacity Utilization $92.3 \%$ | ICU Level of Service F |

Analysis Period（min） 15
Splits and Phases：5：SR 3 \＆SR 106


3: SR 3 \& NE Clifton Lane/Rite Aid Drivewalyorizon Year AM Peak Hour 2040 Three Connectors Build Conditions

| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | * | $\uparrow$ | * | $\hat{p}$ | * | $\hat{F}$ | 7 | 4 | 「 |
| Traffic Volume (vph) | 575 | 30 | 5 | 10 | 75 | 310 | 5 | 230 | 180 |
| Future Volume (vph) | 575 | 30 | 5 | 10 | 75 | 310 | 5 | 230 | 180 |
| Turn Type | Perm | NA | Perm | NA | Prot | NA | Prot | NA | Perm |
| Protected Phases |  | 8 |  | 4 | 5 | 2 | 1 | 6 |  |
| Permitted Phases | 8 |  | 4 |  |  |  |  |  | 6 |
| Detector Phase | 8 | 8 | 4 | 4 | 5 | 2 | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 10.0 | 6.0 | 10.0 | 10.0 |
| Minimum Split (s) | 29.5 | 29.5 | 29.5 | 29.5 | 10.5 | 27.6 | 10.5 | 27.6 | 27.6 |
| Total Split (s) | 30.0 | 30.0 | 30.0 | 30.0 | 20.0 | 60.0 | 11.0 | 60.0 | 60.0 |
| Total Split (\%) | 27.3\% | 27.3\% | 27.3\% | 27.3\% | 18.2\% | 54.5\% | 10.0\% | 54.5\% | 54.5\% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.6 | 3.5 | 3.6 | 3.6 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.6 | 4.5 | 4.6 | 4.6 |
| Lead/Lag |  |  |  |  | Lead | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? |  |  |  |  | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | Min | None | Min | Min |
| Act Effct Green (s) | 26.9 | 26.9 | 26.9 | 26.9 | 9.0 | 33.3 | 6.5 | 24.4 | 24.4 |
| Actuated g/C Ratio | 0.38 | 0.38 | 0.38 | 0.38 | 0.13 | 0.47 | 0.09 | 0.34 | 0.34 |
| v/c Ratio | 1.29 | 0.14 | 0.01 | 0.06 | 0.38 | 0.41 | 0.06 | 0.76 | 0.49 |
| Control Delay | 172.9 | 11.6 | 22.0 | 12.1 | 38.5 | 13.4 | 39.6 | 37.4 | 7.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 172.9 | 11.6 | 22.0 | 12.1 | 38.5 | 13.4 | 39.6 | 37.4 | 7.4 |
| LOS | F | B | C | B | D | B | D | D | A |
| Approach Delay |  | 153.1 |  | 13.3 |  | 18.3 |  | 24.4 |  |
| Approach LOS |  | F |  | B |  | B |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |
| Cycle Length: 110 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 71.5 |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 90 |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Uncoordinated |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.29 |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 78.8 |  |  |  | Intersection LOS: E |  |  |  |  |  |
| Intersection Capacity Utilization 79.6\%Analysis Period (min) 15 |  |  |  | ICU Level of Service D |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 3: SR 3 \& NE Clifton Lane/Rite Aid Driveway



|  | Minor2 | Major1 |  | Major2 |  |  |
| :--- | ---: | ---: | ---: | :--- | :--- | :--- |
| Major/Minor | Manflicting Flow All | 1282 | 310 | 318 | 0 | - |
| $\quad$ Stage 1 | 310 | - | - | - | - | - |
| $\quad$ Stage 2 | 972 | - | - | - | - | - |
| Critical Hdwy | 6.49 | 6.29 | 4.13 | - | - | - |
| Critical Hdwy Stg 1 | 5.49 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.49 | - | - | - | - | - |
| Follow-up Hdwy | 3.581 | 3.381 | 2.227 | - | - | - |
| Pot Cap-1 Maneuver | 176 | 714 | 1236 | - | - | - |
| $\quad$ Stage 1 | 728 | - | - | - | - | - |
| Stage 2 | 356 | - | - | - | - | - |

Platoon blocked, \%
Mov Cap-1 Maneuver $138 \quad 7141236$

| Mov Cap-2 Maneuver | 76 | - | - | - | - | - |
| :---: | ---: | ---: | ---: | :--- | :--- | :--- |
| Stage 1 | 571 | - | - | - | - | - |
| Stage 2 | 356 | - | - | - | - | - |


| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 16.2 | 3.3 | 0 |
| HCM LOS | C |  |  |

HCM LOS C

| Minor Lane/Major Mvmt | NBL | NBTEBLn1EBLn2 | SBT | SBR |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 1236 | - | 76 | 714 | - | - |
| HCM Lane V/C Ratio | 0.216 | - | 0.15 | 0.485 | - | - |
| HCM Control Delay (s) | 8.7 | - | 60.5 | 14.7 | - | - |
| HCM Lane LOS | A | - | F | B | - | - |
| HCM 95th \%tile Q(veh) | 0.8 | - | 0.5 | 2.7 | - | - |



## Intersection Summary

Cycle Length: 140
Actuated Cycle Length: 73.8
Natural Cycle: 85
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.68
Intersection Signal Delay: 19.7 Intersection LOS: B
Intersection Capacity Utilization 50.9\% ICU Level of Service A
Analysis Period (min) 15
Splits and Phases: 5: SR 3 \& SR 106


3: SR 3 \& NE Clifton Lane/Rite Aid Drivewapening Year PM Peak Hour 2040 Three Connections Build Conditions


Analysis Period (min) 15
Splits and Phases: 3: SR 3 \& NE Clifton Lane/Rite Aid Driveway


4: SR 3 \& Old Belfair Highway (SR 300) Opening Year PM Peak Hour 2040 Three Connections Build Conditions

| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 2.1 |  |  |  |  |  |
| Movement E | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | 7 | 「 | ${ }^{*}$ | 4 | $\uparrow$ |  |
| Traffic Vol, veh/h | 5 | 455 | 310 | 345 | 735 | 20 |
| Future Vol, veh/h | 5 | 455 | 310 | 345 | 735 | 20 |
| Conflicting Peds, \#/hr | 2 | 2 | 2 | 0 | 0 | 2 |
| Sign Control Stop | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length 3 | 300 | 0 | 100 | - | - | - |
| Veh in Median Storage, \# |  | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor 93 | 93 | 93 | 93 | 93 | 93 | 93 |
| Heavy Vehicles, \% | 4 | 4 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 5 | 489 | 333 | 371 | 790 | 22 |


| Major/Minor | Minor2 | Major1 |  | Major2 |  |  |
| :--- | ---: | ---: | ---: | :--- | :--- | :--- |
| Conflicting Flow All | 1842 | 805 | 814 | 0 | - | 0 |
| $\quad$ Stage 1 | 803 | - | - | - | - | - |
| $\quad$ Stage 2 | 1039 | - | - | - | - | - |
| Critical Hdwy | 6.44 | 6.24 | 4.12 | - | - | - |
| Critical Hdwy Stg 1 | 5.44 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.44 | - | - | - | - | - |
| Follow-up Hdwy | 3.536 | 3.336 | 2.218 | - | - | - |
| Pot Cap-1 Maneuver | 82 | $\sim 379$ | 813 | - | - | - |
| $\quad$ Stage 1 | 437 | - | - | - | - | - |
| Stage 2 | 338 | - | - | - | - | - |

Platoon blocked, \%
Mov Cap-1 Maneuver 48 ~ $378 \quad 811$
Mov Cap-2 Maneuver ~-7 - - -

| Stage 1 | 257 | - | - | - | - | - |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Stage 2 | 337 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | EB | NB | SB |  |  |  |
| HCM Control Delay, s |  | 5.9 | 0 |  |  |  |
| HCM LOS | - |  |  |  |  |  |


| Minor Lane/Major Mvmt | NBL | NBTEBLn1EBLn2 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 811 | - | +378 | - | - |
| HCM Lane V/C Ratio | 0.411 | - | -1.294 | - | - |
| HCM Control Delay (s) | 12.5 | - | -180.4 | - | - |
| HCM Lane LOS | B | - | - | F | - |
| HCM 95th \%tile Q(veh) | 2 | - | -22.2 | - | - |

Notes
~: Volume exceeds capacity $\$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ : All major volume in platoon

5: SR 3 \& SR 106


## Intersection Summary

Cycle Length: 120
Actuated Cycle Length: 60.5
Natural Cycle: 85
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 1.11

| Intersection Signal Delay: 42.5 | Intersection LOS: D |
| :--- | :--- |
| Intersection Capacity Utilization $77.0 \%$ | ICU Level of Service D |

Analysis Period (min) 15
Splits and Phases: 5: SR 3 \& SR 106


Phone:
E-Mail:

Fax:
$\qquad$ Directional Two-Lane Highway Segment Analysis $\qquad$

Analyst
Agency/Co. Parametrix
Date Performed 9/3/2019
Analysis Time Period PM Peak Hour
Highway
From/To North of Lake Flora
Jurisdiction WSDOT
Analysis Year Existing Conditions 2019
Description SR 3 Freight Corridor LOS

Input Data $\qquad$

| Highway class | Class | 1 | Peak hour factor, PHF | 0.89 |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 4 | $\%$ |  |
| Lane width | 10.0 | ft | \% Trucks crawling | 0.0 | $\%$ |  |
| Segment length | 1.0 | mi | Truck crawl speed | 0.0 | $\mathrm{mi} / \mathrm{hr}$ |  |
| Terrain type | Level |  | $\%$ Recreational vehicles | 0 | $\%$ |  |
| Grade: Length | - | mi | \% No-passing zones | 30 | $\%$ |  |
|  | Up/down | - | $\%$ | Access point density | 0 | $/ \mathrm{mi}$ |

Analysis direction volume, Vd 665 veh/h
Opposing direction volume, Vo 580 veh/h
Average Travel Speed

$\qquad$

$\qquad$ Level of Service and Other Performance Measures $\qquad$
Level of service, LOS
Volume to capacity ratio, v/c
D
Peak 15-min vehicle-miles of travel, VMT15
Peak-hour vehicle-miles of travel, VMT60
0.44

Peak 15-min total travel time, TT15
187 veh-mi

Capacity from ATS, CdATS 1700 veh/h
Capacity from PTSF, CdPTSF 1700 veh/h
Directional Capacity 1700 veh/h
Passing Lane Analysis $\qquad$
Total length of analysis segment, Lt 1.0 mi
Length of two-lane highway upstream of the passing lane, Lu

- mi

Length of passing lane including tapers, Lpl

- mi

Average travel speed, ATSd (from above)
$47.0 \mathrm{mi} / \mathrm{h}$
Percent time-spent-following, PTSFd (from above)
76.9

Level of service, LOSd (from above)
D

Average Travel Speed with Passing Lane
Downstream length of two-lane highway within effective length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl 0.0 \%
Percent Time-Spent-Following with Passing Lane $\qquad$
Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following including passing lane, PTSFpl - \%
$\qquad$ Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl
E
Peak 15-min total travel time, TT15

- veh-h

Bicycle Level of Service $\qquad$
Posted speed limit, Sp 50
Percent of segment with occupied on-highway parking 0
Pavement rating, P 3
Flow rate in outside lane, vOL 747.2
Effective width of outside lane, We 22.00
Effective speed factor, St
4.62
Bicycle LOS Score, BLOS 4.33
Bicycle LOS D
Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) >= $1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F .
3. For the analysis direction only and for $v>200$ veh/h.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
E-Mail:

Fax:
$\qquad$ Directional Two-Lane Highway Segment Analysis $\qquad$
Analyst
Agency/Co. Parametrix
Date Performed 9/3/2019
Analysis Time Period PM Peak Hour
Highway
From/To North of Lake Flora
Jurisdiction WSDOT
Analysis Year No Build 2025 Conditions
Description SR 3 Freight Corridor LOS

Input Data


Average Travel Speed $\qquad$


Free-Flow Speed from Field Measurement:
Field measured speed, (note-3) S FM - mi/h
Observed total demand, (note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed, (note-3) BFFS $60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width, (note-3) fLS $1.1 \mathrm{mi} / \mathrm{h}$
Adj. for access point density, (note-3) fA 0.0 mi/h
Free-flow speed, FFSd
$0.9 \mathrm{mi} / \mathrm{h}$
Average travel speed, ATSd $46.4 \mathrm{mi} / \mathrm{h}$
Percent Free Flow Speed, PFFS
78.7 \%
$\qquad$

$\qquad$ Level of Service and Other Performance Measures $\qquad$
Level of service, LOS
Volume to capacity ratio, v/c
D
Peak 15-min vehicle-miles of travel, VMT15
Peak-hour vehicle-miles of travel, VMT60
0.47

Peak 15-min total travel time, TT15 4.3
Capacity from ATS, CdATS 1700
Capacity from PTSF, CdPTSF
veh/h
Directional Capacity $1700 \mathrm{veh} / \mathrm{h}$
Passing Lane Analysis $\qquad$
Total length of analysis segment, Lt 1.0 mi
Length of two-lane highway upstream of the passing lane, Lu

- mi

Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)
Percent time-spent-following, PTSFd (from above)
$46.4 \mathrm{mi} / \mathrm{h}$
79.2

Level of service, LOSd (from above)
D

Average Travel Speed with Passing Lane
Downstream length of two-lane highway within effective length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl 0.0 \%
Percent Time-Spent-Following with Passing Lane $\qquad$
Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following including passing lane, PTSFpl - \%
$\qquad$ Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl
E
Peak 15-min total travel time, TT15

- veh-h

Bicycle Level of Service $\qquad$
Posted speed limit, Sp 50
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL
3
792.1
Effective width of outside lane, We
22.00
Effective speed factor, St
4.62
Bicycle LOS Score, BLOS
4.36
Bicycle LOS
D
Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain
is one of the base conditions. For the purpose of grade adjustment, specific
dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F .
3. For the analysis direction only and for $v>200$ veh/h.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a
specific downgrade.

Phone:
E-Mail:

Fax:
$\qquad$ Directional Two-Lane Highway Segment Analysis $\qquad$

Analyst
Agency/Co. Parametrix
Date Performed 9/3/2019
Analysis Time Period PM Peak Hour
Highway
From/To North of Lake Flora
Jurisdiction WSDOT
Analysis Year No Build 2040 Conditions
Description SR 3 Freight Corridor LOS

Input Data $\qquad$

| Highway class | Class | 1 | Peak hour factor, PHF | 0.89 |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 4 | $\%$ |  |
| Lane width | 10.0 | ft | \% Trucks crawling | 0.0 | $\%$ |  |
| Segment length | 1.0 | mi | Truck crawl speed | 0.0 | mi/hr |  |
| Terrain type | Level |  | \% Recreational vehicles | 0 | $\%$ |  |
| Grade: Length | - | mi | \% No-passing zones | 30 | $\%$ |  |
|  | Up/down | - | $\%$ | Access point density | 0 | $/ \mathrm{mi}$ |

Analysis direction volume, Vd 835 veh/h
Opposing direction volume, Vo 735 veh/h
Average Travel Speed

$\qquad$


Ad time-spent following, PTSFd

Level of Service and Other Performance Measures $\qquad$
Level of service, LOS
Volume to capacity ratio, v/c
E

Peak 15-min vehicle-miles of travel, VMT15
Peak-hour vehicle-miles of travel, VMT60
55

Peak 15-min total travel time, TT15
8
835
Capacity from ATS, CdATS 170
Capacity from PTSF, CdPTSF
$1700 \quad \mathrm{veh} / \mathrm{h}$
$1700 \mathrm{veh} / \mathrm{h}$
Directional Capacity 1700 veh/h
Passing Lane Analysis $\qquad$
Total length of analysis segment, Lt 1.0 mi
Length of two-lane highway upstream of the passing lane, Lu

- mi

Length of passing lane including tapers, Lpl
-
mi

Average travel speed, ATSd (from above)
$44.5 \mathrm{mi} / \mathrm{h}$
Percent time-spent-following, PTSFd (from above)
83.7

Level of service, LOSd (from above)
E

Average Travel Speed with Passing Lane
Downstream length of two-lane highway within effective length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl 0.0 \%
Percent Time-Spent-Following with Passing Lane $\qquad$
Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following including passing lane, PTSFpl - \%
$\qquad$ Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 50
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL 938.2
3
Effective width of outside lane, We 22.00
Effective speed factor, St
4.62
Bicycle LOS Score, BLOS
4.44
Bicycle LOS
D
Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F .
3. For the analysis direction only and for $v>200$ veh/h.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
E-Mail:

Fax:
$\qquad$ Directional Two-Lane Highway Segment Analysis $\qquad$
Analyst
Agency/Co. Parametrix
Date Performed 9/3/2019
Analysis Time Period PM Peak Hour
Highway
From/To Lake Flora/SR 302
Jurisdiction WSDOT
Analysis Year Alta Build 2025 Conditions
Description SR 3 Freight Corridor LOS

Input Data


Average Travel Speed $\qquad$

Direction
PCE for trucks, ET
PCE for RVs, ER
Heavy-vehicle adj. factor, (note-5) fHV
Grade adj. factor, (note-1) fg
Directional flow rate, (note-2) vi

Analysis(d)
1.5
1.0
0.980
1.00

235
$\mathrm{pc} / \mathrm{h}$

Field measured speed, (note-3) S FM - mi/h
Observed total demand, (note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed, (note-3) BFFS $60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width, (note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density, (note-3) fA $0.3 \mathrm{mi} / \mathrm{h}$
Free-flow speed, FFSd
$59.8 \mathrm{mi} / \mathrm{h}$
Adjustment for no-passing zones, fnp $2.1 \mathrm{mi} / \mathrm{h}$
Average travel speed, ATSd
Percent Free Flow Speed, PFFS
$54.2 \mathrm{mi} / \mathrm{h}$
90.7 \%
$\qquad$

$\qquad$ Level of Service and Other Performance Measures $\qquad$
Level of service, LOS
Volume to capacity ratio, v/c
B

Peak 15-min vehicle-miles of travel, VMT15
Peak-hour vehicle-miles of travel, VMT60
0.14

1150
1150 veh-mi
Peak 15-min total travel time, TT15
5.3 veh-h

Capacity from ATS, CdATS 1700 veh/h
Capacity from PTSF, CdPTSF 1700 veh/h
Directional Capacity 1700 veh/h
Passing Lane Analysis $\qquad$
Total length of analysis segment, Lt 5.0 mi
Length of two-lane highway upstream of the passing lane, Lu

- mi

Length of passing lane including tapers, Lpl
-
mi

Average travel speed, ATSd (from above)
Percent time-spent-following, PTSFd (from above)
$54.2 \mathrm{mi} / \mathrm{h}$
Level of service, LOSd (from above)
46.1

B
Average Travel Speed with Passing Lane
Downstream length of two-lane highway within effective length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl 0.0 \%
Percent Time-Spent-Following with Passing Lane $\qquad$
Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following including passing lane, PTSFpl - \%
$\qquad$ Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl
E
Peak 15-min total travel time, TT15

- veh-h

Bicycle Level of Service $\qquad$
Posted speed limit, Sp 50
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL
230.0
Effective width of outside lane, We 24.00
Effective speed factor, St
4.62
Bicycle LOS Score, BLOS
3.27
Bicycle LOS
C

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F .
3. For the analysis direction only and for $v>200$ veh/h.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
E-Mail:

Fax:
$\qquad$ Directional Two-Lane Highway Segment Analysis $\qquad$

Analyst
Agency/Co. Parametrix
Date Performed 8/19/2019
Analysis Time Period PM Peak Hour
Highway
From/To Lake Flora/SR 302
Jurisdiction WSDOT
Analysis Year
Description SR 3 Freight Corridor LOS

Input Data $\qquad$

| Highway class | Class 1 |  | Peak hour factor, PHF | 1.00 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 4 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment length | 5.0 | mi | Truck crawl speed | 0.0 | mi/hr |
| Terrain type | Level |  | \% Recreational vehicles | 0 | \% |
| Grade: Length | - | mi | \% No-passing zones | 25 | \% |
| Up / down | - | \% | Access point density | 1 | /mi |

Analysis direction volume, Vd 755 veh/h
Opposing direction volume, Vo 515 veh/h

| Direction An | Analysis(d) |  | Opposing (o) |  |
| :---: | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.1 |  | 1.2 |  |
| PCE for RVs, ER | 1.0 |  | 1.0 |  |
| Heavy-vehicle adj. factor, (note-5) fHV | $V \quad 0.996$ |  | 0.992 |  |
| Grade adj. factor, (note-1) fg | 1.00 |  | 1.00 |  |
| Directional flow rate, (note-2) vi | 758 | $\mathrm{pc} / \mathrm{h}$ | 519 |  |
| Free-Flow Speed from Field Measurement: |  |  |  |  |
| Field measured speed, (note-3) S FM |  | - | $\mathrm{mi} / \mathrm{h}$ |  |
| Observed total demand, (note-3) V |  | - | veh/h |  |
| Estimated Free-Flow Speed: |  |  |  |  |
| Base free-flow speed, (note-3) BFFS |  | 60.0 | $\mathrm{mi} / \mathrm{h}$ |  |
| Adj. for lane and shoulder width, (note-3 | -3) fLS | 0.0 | $\mathrm{mi} / \mathrm{h}$ |  |
| Adj. for access point density, $n$ ( ${ }^{\text {a }}$ (e-3) f | fA | 0.3 | $\mathrm{mi} / \mathrm{h}$ |  |
| Free-flow speed, FFSd |  | 59.8 | mi/h |  |
| Adjustment for no-passing zones, fnp |  | 1.3 | $\mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd |  | 48.5 | $\mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS |  | 81.2 | \% |  |

$\qquad$

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.0 | 1.0 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adjustment factor, fHV | 1.000 | 1.000 |  |  |
| Grade adjustment factor, (note-1) fg | 1.00 |  | 1.00 | pc/h |
| Directional flow rate, (note-2) vi | 755 | pc/h | 515 |  |
| Base percent time-spent-following, (note-4) | BPTSFd | 64.7 | $\%$ |  |
| Adjustment for no-passing zones, fnp |  | 21.9 |  |  |
| Percent time-spent-following, PTSFd |  | 77.7 | $\%$ |  |

dime-spent following, PTSFd

Level of Service and Other Performance Measures $\qquad$
Level of service, LOS
Volume to capacity ratio, v/c

## D

Peak 15-min vehicle-miles of travel, VMT15
Peak-hour vehicle-miles of travel, VMT60
0.44

Peak 15-min total travel time, TT15
944
3775
19.4

Capacity from ATS, CdATS
Capacity from PTSF, CdPTSF
$1700 \mathrm{veh} / \mathrm{h}$
Directional Capacity
$1700 \mathrm{veh} / \mathrm{h}$
Passing Lane Analysis $\qquad$
Total length of analysis segment, Lt 5.0 mi
Length of two-lane highway upstream of the passing lane, Lu - mi
Length of passing lane including tapers, Lpl -

- mi

Average travel speed, ATSd (from above)
$48.5 \mathrm{mi} / \mathrm{h}$
Percent time-spent-following, PTSFd (from above)
77.7

Level of service, LOSd (from above)
D

Average Travel Speed with Passing Lane
Downstream length of two-lane highway within effective length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl 0.0 \%
Percent Time-Spent-Following with Passing Lane
Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following including passing lane, PTSFpl - \%
$\qquad$ Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl
E
Peak 15-min total travel time, TT15

- veh-h

Bicycle Level of Service $\qquad$
Posted speed limit, Sp 50
Percent of segment with occupied on-highway parking 0
Pavement rating, $P$
Flow rate in outside lane, vOL
755.0
Effective width of outside lane, We 24.00
Effective speed factor, St
4.62
Bicycle LOS Score, BLOS
3.87
Bicycle LOS
D
Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F .
3. For the analysis direction only and for $v>200$ veh/h.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

[^0]:    ${ }^{1}$ As of January 2024, the "existing year" for the Kitsap County travel demand model is still the year 2019.

[^1]:    2 The horizon year (2050) identified in this report reflects the growth assumed in the local agency comprehensive plans and the growth (full build-out) assumed for the PSIC. The SR 3 Freight Corridor Planning Study (WSDOT 2020) estimated traffic forecasts for a horizon year of 2040. For this report, additional growth between 2040 - 2050 was not assumed because the 2040 forecast assumed the level of growth allowed under the Growth Management Act which defines and allocates the growth allowed by each UGAs and Urban Growth Centers. Therefore, the 2040 forecasts and volumes included in the SR 3 Freight Corridor Planning Study were not updated for this report.

[^2]:    CMapbax, O OpenStreetMap

[^3]:    ${ }^{\text {a }}$ Average time percent of total travel time that vehicles must travel in platoons behind slower vehicles due to inability to pass on a two-lane highway (HCM 6th Edition, 2016).

[^4]:    © Mapbox, © OpenStreetMap

[^5]:    3 The software was consistent with most recent WSDOT Synchro protocol (August 2018).

[^6]:    ${ }^{4}$ More than one contributing factor was attributed to some of the crashes.

[^7]:    C Mapbox, O OpenStreetMap

[^8]:    ©Mapbax, © OpenStreetMap

[^9]:    © Mapbax, © OpenStreetMap

[^10]:    O Mapbox O OpenStreetMap

[^11]:    SIDRA INTERSECTION 8.0 | Copyright © 2000-2019 Akcelik and Associates Pty Ltd | sidrasolutions.com
    Organisation: PARAMETRIX | Processed: Tuesday, August 13, 2019 8:33:05 AM
    Project: U:IPSO\Projects\Clients\1631-WSDOT\234-1631-130 SR3FreightCorr TOAAIO2WBSI07_OperationsAnalysisISR3_RBTs_v2.sip8

[^12]:    SIDRA INTERSECTION 8.0 | Copyright © 2000-2019 Akcelik and Associates Pty Ltd | sidrasolutions.com
    Organisation: PARAMETRIX | Processed: Tuesday, August 13, 2019 8:33:19 AM
    Project: U:IPSO\Projects\Clients\1631-WSDOT\234-1631-130 SR3FreightCorr TOAAIO2WBSI07_OperationsAnalysisISR3_RBTs_v2.sip8

[^13]:    IDRA INTERSECTION 8.0 Copyright © 2000-2019 Akcelik and Associates Pty Ltd sidrasolutions.com
    Organisation: PARAMETRIX | Processed: Monday, August 12, 2019 11:34:09 AM
    Project: U:IPSO\Projects\Clients\1631-WSDOT\234-1631-130 SR3FreightCorr TOAAI02WBSISR3_RBTs_v2.sip8

[^14]:    SIDRA INTERSECTION 8.0 Copyright © 2000-2019 Akcelik and Associates Pty Ltd sidrasolutions.com
    Organisation: PARAMETRIX | Processed: Monday, August 12, 2019 10:54:46 AM
    Project: U:IPSO\Projects\Clients\1631-WSDOT\234-1631-130 SR3FreightCorr TOAAI02WBSISR3_RBTs_v2.sip8

[^15]:    SIDRA INTERSECTION 8.0 | Copyright © 2000-2019 Akcelik and Associates Pty Ltd | sidrasolutions.com
    Organisation: PARAMETRIX | Processed: Friday, July 12, 2019 10:28:15 AM
    Project: U:IPSO\ProjectsIClients\1631-WSDOT\234-1631-130 SR3FreightCorr TOAAI02WBSI07_OperationsAnalysis\02_OpeningYear\Log
    Yard Road.sip8

[^16]:    SIDRA INTERSECTION 8.0 | Copyright © 2000-2019 Akcelik and Associates Pty Ltd | sidrasolutions.com
    Organisation: PARAMETRIX | Processed: Friday, July 12, 2019 10:35:39 AM
    Project: U:IPSOIProjectsIClients\1631-WSDOT\234-1631-130 SR3FreightCorr TOAAI02WBSI07_OperationsAnalysis\02_OpeningYearlLog Yard Road.sip8

[^17]:    SIDRA INTERSECTION 8.0 | Copyright © 2000-2019 Akcelik and Associates Pty Ltd | sidrasolutions.com
    Organisation: PARAMETRIX | Processed: Monday, July 15, 2019 3:52:46 PM
    Project: U:IPSO\Projects\Clients\1631-WSDOT\234-1631-130 SR3FreightCorr TOAAI02WBSI07_OperationsAnalysis\SR3_RBTs.sip8

[^18]:    SIDRA INTERSECTION 8.0 | Copyright © 2000-2019 Akcelik and Associates Pty Ltd | sidrasolutions.com
    Organisation: PARAMETRIX | Processed: Monday, July 15, 2019 4:30:10 PM
    Project: U:IPSO\Projects\Clients\1631-WSDOT\234-1631-130 SR3FreightCorr TOAAI02WBSI07_OperationsAnalysis\SR3_RBTs.sip8

[^19]:    SIDRA INTERSECTION 8.0 | Copyright © 2000-2019 Akcelik and Associates Pty Ltd | sidrasolutions.com
    Organisation: PARAMETRIX | Processed: Thursday, July 11, 2019 3:42:37 PM
    Project: U:IPSO\Projects\Clients\1631-WSDOT\234-1631-130 SR3FreightCorr TOAAIO2WBSI07_OperationsAnalysisl02_OpeningYearl2025
    Opening Year Sidra.sip8

[^20]:    SIDRA INTERSECTION 8.0 | Copyright © 2000-2019 Akcelik and Associates Pty Ltd | sidrasolutions.com
    Organisation: PARAMETRIX | Processed: Friday, July 12, 2019 10:36:14 AM
    Project: U:IPSO\Projects\Clients\1631-WSDOT\234-1631-130 SR3FreightCorr TOAAIO2WBSI07_OperationsAnalysis102_OpeningYearlLog
    Yard Road.sip8

[^21]:    SIDRA INTERSECTION 8.0 | Copyright © 2000-2019 Akcelik and Associates Pty Ltd | sidrasolutions.com
    Organisation: PARAMETRIX | Processed: Monday, July 15, 2019 3:52:48 PM
    Project: U:IPSO\Projects\Clients\1631-WSDOT\234-1631-130 SR3FreightCorr TOAAI02WBSI07_OperationsAnalysis\SR3_RBTs.sip8

[^22]:    SIDRA INTERSECTION 8.0 | Copyright © 2000-2019 Akcelik and Associates Pty Ltd | sidrasolutions.com
    Organisation: PARAMETRIX | Processed: Monday, July 15, 2019 4:30:12 PM
    Project: U:IPSO\Projects\Clients\1631-WSDOT\234-1631-130 SR3FreightCorr TOAAI02WBSI07_OperationsAnalysis\SR3_RBTs.sip8

