| Transmittal Number <br> PT 07-009 | Date <br> February 26, 2007 |
| :---: | :--- |
| Publication Distribution <br> To: All Bridge Design Manual holders |  |
| Publication Title <br> Bridge Design Manual Revision M 23-50.01 | Publication Number |
| Originating Organization <br> Washington State Department of Transportation, and Bridge Design Office through <br> Engineering Publications |  |

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February 26, 2007

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Program Development Division
Bridge and Structures

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Appendix 5.1-A6
Appendix 5.1-A7
Appendix 5.1-A8
Appendix 5.2-A1
Appendix 5.2-A2
Appendix 5.2-A3
Appendix 5.3-A1
Appendix 5.3-A2
Appendix 5.3-A3
August 2006 Beams and Columns

August 2006
Reinforcing Bar Properties
August 2006
Tension Development Length of Deformed Bars
Compression Development Length and Minimum Lap Splice of Grade 60 Bars

August 2006
Tension Development Length of $90^{\circ}$ and $180^{\circ}$ Standard Hooks August 2006
Tension Lap Splice Lengths of Grade 60 Uncoated Bars ~ Class B August 2006
Prestressing Strand Properties and Development Length August 2006
August 2006
August 2006
August 2006
Positive Moment Reinforcement
August 2006
Negative Moment Reinforcement
August 2006
Adjusted Negative Moment Case I
(Design for M @ Face of Support)
August 2006

Appendix 5.3-A4
Appendix 5.3-A5
Appendix 5.3-A6
Appendix 5.3-A7
Appendix 5.3-A8
Appendix 5.6-A1-1
Appendix 5.6-A1-2
Appendix 5.6-A1-3
Appendix 5.6-A1-4
Appendix 5.6-A1-5
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Appendix 5.6-A1-7
Appendix 5.6-A1-8
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Appendix 5.6-A1-10
Appendix 5.6-A1-11
Appendix 5.6-A1-12
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Appendix 5.6-A1-8
Appendix 5.6-A1-9
Appendix 5.6-A1-10
Appendix 5.6-A1-11
Appendix 5.6-A1-12
Appendix 5.6-A1-13
Appendix 5.6-A1-14
Appendix 5.6-A1-15
Appendix 5.6-A2-1
Appendix 5.6-A2-2
Appendix 5.6-A2-3
Appendix 5.6-A3-1
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Appendix 5.6-A3-6
Appendix 5.6-A3-7
Appendix 5.6-A3-8
Appendix 5.6-A3-9
Appendix 5.6-A3-10
Appendix 5.6-A4-1
Appendix 5.6-A4-2

Adjusted Negative Moment Case II (Design for M @ 1/4 Point)
August 2006
Cast-In-Place Deck Slab Design for Positive Moment Regions $\mathrm{f}^{\prime} \mathrm{c}=4,0 \mathrm{ksi}$
Cast-In-Place Deck Slab Design for Negative Moment Regions $\mathrm{f}^{\prime} \mathrm{c}=4,0 \mathrm{ksi}$

August 2006
Slab Overhang Design-Interior Barrier Segment February 26, 2007
Slab Overhang Design-End Barrier Segment
Span Capability of Prestressed I-Girders
Span Capability of Prestressed Wide Flange I-Girders
Span Capability of Thin Flange Bulb Tee Girders
Span Capability of Trapezoidal Tub Girders without Top Flange
Span Capability of Trapezoidal Tub Girders with Top Flange for S-I-P Deck Panels
Span Capability of 1'-0" Solid Slabs with 5" CIP Topping
Span Capability of $1^{\prime}-6^{\prime \prime}$ Voided Slab with $5^{\prime \prime}$ CIP Topping
Span Capability of 2'-2" Voided Slab with 5" CIP Topping
Span Capability of Precast Prestressed Double Tee Girders
Span Capability Precast Prestressed Ribbed Girders
Span Capability of Deck Bulb Tee Girders
Span Capability of Post-Tensioned Spliced I-Girders
Span Capability of Post-Tensioned Spliced Tub Girders
I-Girder Sections
Wide Flange Girder Sections
Bulb Tee Girder Sections
Wide Flange bulb Tee Girder Sections
Trapezoidal Tub Girder Sections
Trapezoidal Tub Girders with Top Flange Sections
Decked Bulb Tee Girder Section
Precast Prestressed Slab Sections
Double-Tee and Ribbed Deck Girder Sections
Spliced I-Girder Sections
Spliced Trapezoidal Tub Girder Sections
I-Girder Sections
Decked Girder Sections
Spliced-Girder Sections
Trapezoidal Tub Sections
Single Span Prestressed Girder Construction Sequence
Multiple Span Prestressed Girder Construction Sequence
Raised Crossbeam Prestressed Girder Construction Sequence
W42G Girder Details 1 of 2
W42G Girder Details 2 of 2
W42G End Diaphragm on Girder Details
W42G Abutment Type Pier Diaphragm Details
W42G Fixed Flush-Face Diaphragm at Intermediate Pier Details January 2006
W42G Fixed Recessed-Face Diaphragm at Intermediate Pier DetailsJanuary 2006
W42G Hinge Diaphragm at Intermediate Pier Details
W42G Intermediate Diaphragm Details
W42G Miscellaneous Bearing Details
Multiple Simple Spans Intermediate Pier Details
W50G Girder Details 1 of 2
W50G Girder Details 2 of 2

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Appendix 5.6-A4-3
Appendix 5.6-A4-4
Appendix 5.6-A4-5
Appendix 5.6-A4-6
Appendix 5.6-A4-7
Appendix 5.6-A4-8
Appendix 5.6-A4-9
Appendix 5.6-A5-1
Appendix 5.6-A5-2
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Appendix 5.6-A5-6
Appendix 5.6-A5-7
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Appendix 5.6-A7-1
Appendix 5.6-A7-2
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Appendix 5.6-A7-4
Appendix 5.6-A7-5
Appendix 5.6-A8-1
Appendix 5.6-A8-2
Appendix 5.6-A9-1
Appendix 5.6-A9-2
Appendix 5.6-A10-1
Appendix 5.6-A10-2
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Appendix 5.6-A11-2
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Appendix 5.6-A11-4
Appendix 5.6-A11-5

W50G End Diaphragm on Girder Details
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W50G Abutment Type Pier Diaphragm Details
February 2007
W50G Fixed Flush-Face Diaphragm at Intermediate Pier Details January 2006
W50G Fixed Recessed-Face Diaphragm at Intermediate Pier DetailsJanuary 2006
W50G Hinge Diaphragm at Intermediate Pier Details January 2006
W50G Intermediate Diaphragm Details
W50G Miscellaneous Bearing Details
W58G Girder Details 1 of 3
W58G Girder Details 2 of 3
W58G Girder Details 3 of 3
W58G End Diaphragm on Girder Details
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W58G Abutment Type Pier Diaphragm Details
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W58G Fixed Flush-Face Diaphragm at Intermediate Pier Details January 2006
W58G Fixed Recessed-Face Diaphragm at Intermediate Pier DetailsJanuary 2006
W58G Hinge Diaphragm at Intermediate Pier Details January 2006
W58G Intermediate Diaphragm Details January 2006
W58G Miscellaneous Bearing Details
W74G Girder Details 1 of 3
W74G Girder Details 2 of 3
W74G Girder Details 3 of 3
W74G End Diaphragm on Girder Details
W74G Abutment Type Pier Diaphragm Details
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W74G Fixed Flush-Face Diaphragm at Intermediate Pier Details January 2006
W74G Fixed Recessed-Face Diaphragm at Intermediate Pier DetailsJanuary 2006
W74G Hinge Diaphragm at Intermediate Pier Details January 2006
W74G Intermediate Diaphragm Details February 2007
W74G Miscellaneous Bearing Details February 2007
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Miscellaneous Bearing Details February 2007
WF42G Girder Details 1 of $3 \quad$ February 2007
WF42G Girder Details 2 of $3 \quad$ February 2007
WF50G Girder 1 of $3 \quad$ February 2007
WF50G Girder 2 of 3
WF58G Girder Details 1 of 3
WF58G Girder Details 2 of 3
WF74G Girder Details 1 of 3
WF74G Girder Details 2 of 3
WF74G End Diaphragm on Girder Details
WF74G Abutment Type Pier Diaphragm Details
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WF74G Fixed Flush-Face Diaphragm at Intermediate Pier Details February 2007
WF74G Fixed Recessed-Face Diaphragm at
Intermediate Pier Details
WF74G Hinge Diaphragm at Intermediate Pier Details
WF74G Intermediate Diaphragm Details
WF83G Girder Details 1 of 3
WF83G Girder Details 2 of 3
WF83G End Diaphragm on Girder Details
WF83G Abutment Type Pier Diaphragm Details
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WF83G Fixed Flush-Face Diaphragm at Intermediate Pier Details February 2007

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Appendix 5.6-A12-1
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Appendix 5.6-A12-7
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Appendix 5.6-A14-1
Appendix 5.6-A14-2
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Appendix 5.6-A15-2
Appendix 5.6-A15-3
Appendix 5.6-A16-1
Appendix 5.6-A16-2
Appendix 5.6-A16-3
Appendix 5.6-A16-4
Appendix 5.6-A16-5
Appendix 5.6-A16-6
Appendix 5.6-A17-1
Appendix 5.6-A17-2
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Appendix 5.6-A17-7
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Appendix 5.6-A19-1
Appendix 5.6-A19-2
Appendix 5.6-A20-1
Appendix 5.6-A20-2
Appendix 5.6-A21-1
Appendix 5.6-A21-2
Appendix 5.6-A21-3
Appendix 5.6-A21-4
Appendix 5.6-A21-5

WF83G Fixed Recessed-Face Diaphragm at Intermediate Pier Details
WF83G Hinge Diaphragm at Intermediate Pier Details
WF83G Intermediate Diaphragm Details
WF95G Girder Details 1 of 3
WF95G Girder Details 2 of 3
WF95G End Diaphragm on Girder Details
WF95G Abutment Type Pier Diaphragm Details
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WF95G Fixed Flush-Face Diaphragm at Intermediate Pier Details February 2007 WF95G Fixed Recessed-Face Diaphragm at Intermediate Pier Details
WF95G Hinge Diaphragm at Intermediate Pier Details
WF95G Intermediate Diaphragm Details
W32BTG Girder Details 1 of 3
W32BTG Girder Details 2 of 3
W32BTG Girder Details 3 of 3
W38BTG Girder Details 1 of 3
W38BTG Girder Details 2 of 3
W38BTG Girder Details 3 of 3
W62BTG Girder Details 1 of 3
W62BTG Girder Details 2 of 3
W62BTG Girder Details 3 of 3
Prestressed Trapezoidal Tub Girder Details 1 of 3
Prestressed Trapezoidal Tub Girder Detials 2 of 3
Prestressed Trapezoidal Tub Girder Detials 3 of 3
Prestressed Trapezoidal Tub Girder End Diaphragm on Girder Details
Prestressed Trapezoidal Tub Girder Raised Crossbeam Details
Prestressed Trapezoidal Tub Girder Miscellaneous Diaphragm Details
Trapezoidal Tub S-I-P Deck Panel Girder Details 1 of 4
Trapezoidal Tub S-I-P Deck Panel Girder Details 2 of 4
Trapezoidal Tub S-I-P Deck Panel Girder Details 3 of 4
Trapezoidal Tub S-I-P Deck Panel Girder Details 4 of 4
Trapezoidal Tub S-I-P Deck Panel Girder - End Diaphragm on Girder Details
Trapezoidal Tub S-I-P Deck Panel Girder - Raised Crossbeam Details
Trapezoidal Tub S-I-P Deck Panel Girder Miscellaneous Diaphragm Details
Precast Prestressed Stay-In-Place Deck Panel Details
Precast Prestressed 1'-0" Solid Slab Details 1 of 2
Precast Prestressed 1'-0" Solid Slab Details 2 of 2
Precast Prestressed 1'-6" Voided Slab - Details 1 of 2
Precast Prestressed 1'- $6^{\prime \prime}$ Voided Slab - Details 2 of 2
Precast Prestressed 2'-2" Voided Slab - Details 1 of 2
Precast Prestressed 2'-2" Voided Slab - Details 2 of 2
Precast Prestressed Slab Layout
Precast Prestressed Slab End Pier Details 1 of 2
Precast Prestressed Slab End Pier Details 2 of 2

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Appendix 5.6-A22-1
Appendix 5.6-A22-2
Appendix 5.6-A22-3
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Appendix 5.6-A24-2
Appendix 5.6-A24-3
Appendix 5.6-A25-1
Appendix 5.6-A25-2
Appendix 5.6-A25-3
Appendix 5.6-A26-1
Appendix 5.6-A26-2
Appendix 5.6-A26-3
Appendix 5.6-A27-1
Appendix 5.6-A27-2
Appendix 5.6-A27-3
Appendix 5.6-A27-4
Appendix 5.9-A1-1
Appendix 5.9-A1-2
Appendix 5.9-A1-3
Appendix 5.9-A1-4
Appendix 5.9-A1-5
Appendix 5.9-A2-1
Appendix 5.9-A2-2
Appendix 5.9-A2-3
Appendix 5.9-A2-4
Appendix 5.9-A2-5
Appendix 5.9-A3-1
Appendix 5.9-A3-2
Appendix 5.9-A3-3
Appendix 5.9-A3-4
Appendix 5.9-A3-5
Appendix 5.9-A4-1
Appendix 5.9-A4-2
Appendix 5.9-A4-3
Appendix 5.9-A4-4
Appendix 5.9-A4-5
Appendix 5.9-A4-6
Appendix 5.9-A4-7
Appendix 5.9-A4-8
Appendix 5.9-A5-1
Appendix 5.9-A5-2
Appendix 5.9-A5-3
Appendix 5.9-A5-4
Appendix 5.9-A5-5
Appendix 5.9-A5-6

Precast Prestressed Slab Intermediate Pier Details 1 of 2
Precast Prestressed Slab Intermediate Pier Details 2 of 2
Precast Prestressed Double T Details 1 of 2
Precast Prestressed Double T Details 2 of 2
Precast Prestressed Ribbed Girder Pier Details
Precast Prestressed Ribbed Girder Details 1 of 2
Precast Prestressed Ribbed Girder Details 2 of 2
W35DG Deck Bulb Tee Girder Details 1 of 2
W35DG Deck Bulb Tee Girder Details 2 of 2
W35DG Deck Bulb Tee Diaphragm Details
W41DG Deck Bulb Tee Girder Details 1 of 2
W41DG Deck Bulb Tee Girder Details 2 of 2
W41DG Deck Bulb Tee Girder Diaphragm Details
W53DG Deck Bulb Tee Girder Details 1 of 2
W53DG Deck Bulb Tee Girder Details 2 of 2
W53DG Deck Bulb Tee Diaphragm Details
W65DG Deck Bulb Tee Girder Details 1 of 2
W65DG Deck Bulb Tee Girder Details 2 of 2
W65DG Deck Bulb Tee Girder Diaphragm Details
Deck Bulb Tee Girder Diaphragm Details
WF74PTG Spliced Girder Details 1 of 5
WF74PTG Spliced Girder Details 2 of 5
WF74PTG Girder Details 3 of 5
WF74PTG Girder Details 4 of 5
WF74PTG Spliced Girder Details 5 of 5
W83PTG Spliced Girder Details 1 of 5
W83PTG Spliced Girder Details 2 of 5
W83PTG Spliced Girder Details 3 of 5
W83PTG Spliced Girder Details 4 of 5
W83PTG Spliced Girder Details 5 of 5
W95PTG Spliced Girder Details 1 of 5
W95PTG Spliced Girder Details 2 of 5
W95PTG Spliced Girder Details 3 of 5
W95PTG Spliced Girder Details 4 of 5
W95PTG Spliced Girder Details 5 of 5
Trapezoidal Tub Spliced Girder Details 1 of 5
Trapezoidal Tub Spliced Girder Details 2 of 5
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Prestressed Trapezoidal Tub Girder Details 5 of 5
Trapezoidal Tub Spliced Girder End Diaphragm on Girder Details
Trapezoidal Tub Spliced Girder Raised Crossbeam Details
Trapezoidal Tub Spliced Girder Miscellaneous Details
Trapezoidal Tub S-I-P Deck Panel Spliced Girder Details 1 of 5
Trapezoidal Tub S-I-P Deck Panel Spliced Girder Details 2 of 5
Trapezoidal Tub S-I-P Deck Panel Spliced Girder Details 3 of 5
Trapezoidal Tub S-I-P Deck Panel Spliced Girder Details 4 of 5
Trapezoidal Tub S-I-P Deck Panel Spliced Girder Details 5 of 5
Trapezoidal Tub S-I-P Deck Panel Girder End Diaphragm on Girder Details

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Appendix 5.9-A5-7 Trapezoidal Tub S-I-P Deck Panel Girder Raised Crossbeam Details

June 2006
Appendix 5.9-A5-8
Appendix 5-B1
Appendix 5-B1-1
Appendix 5-B1-2
Appendix 5-B1-3
Appendix 5-B2
Appendix 5-B3
Appendix 5-B4
Appendix 5-B5
Appendix 5-B6
Appendix 5-B7
Appendix 5-B8
Appendix 5-B9
Appendix 5-B10
Appendix 5-B11
Appendix 5-B12
Appendix 5-B13
Appendix 5-B14
Appendix 5-B15
Trapezoidal Tub S-I-P Deck Panel Girder Miscellaneous

Diaphragm Details
"A" Dimension for Prestressed Girder Bridges
Girder Details 3 of 3
Additional Extended Strands
Miscellaneous Bearing Details
Pre-approved Post-Tensioning Anchorages
Existing Bridge Widenings
P.T. Box Girder Bridges Single Span

Prestressed Girder Design Example
Cast-in-Place Slab Design Example
Precast Concrete Stay-In-Place (SIP) Deck Panel
W35DG Deck Bulb Tee, 48" Wide
Prestressed Voided Slab with Cast-in-Place Topping
Positive EQ Reinforcement at Interior Pier of a Prestressed Girder
LRFD Wingwall Design-Vehicle Collision
Flexural Strength Calculations for Composite T-Beams
Strut-and-Tie Model Design Example for Hammerhead Pier
Shear and Torsion Capacity of a Reinforced Concrete Beam
Sound Wall Design - Type D-2k

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| Type | Depth in | Unit <br> Weight k/ft | Max. <br> Span ft | Relative <br> Cost <br> Factor | Fabrication Cost <br> Range |  | Final <br> In-Place <br> Cost** |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| W42G | 42.00 | 0.424 | 85 | 0.75 | $\$ 85$ | $\$ 90$ | $\$ 99$ |
| W50G | 50.00 | 0.585 | 110 | 0.83 | $\$ 95$ | $\$ 100$ | $\$ 110$ |
| W58G | 58.00 | 0.672 | 125 | 0.92 | $\$ 105$ | $\$ 110$ | $\$ 121$ |
| W74G | 73.50 | 0.831 | 150 | $1.00^{*}$ | $\$ 115$ | $\$ 120$ | $\$ 132$ |
| WF42G | 42.00 | 0.806 | 115 | 1.35 | $\$ 150$ | $\$ 155$ | $\$ 178$ |
| WF50G | 50.00 | 0.859 | 130 | 1.44 | $\$ 160$ | $\$ 165$ | $\$ 190$ |
| WF58G | 58.00 | 0.913 | 145 | 1.52 | $\$ 170$ | $\$ 175$ | $\$ 201$ |
| WF74G | 74.00 | 1.020 | 165 | 1.61 | $\$ 180$ | $\$ 185$ | $\$ 213$ |
| W83G | 82.61 | 1.087 | 175 | 1.70 | $\$ 190$ | $\$ 195$ | $\$ 224$ |
| W95G | 94.49 | 1.167 | 160 | 2.00 | $\$ 200$ | $\$ 230$ | $\$ 265$ |
| WBT32G | 32.00 | 0.598 | 75 | 1.57 | $\$ 150$ | $\$ 180$ | $\$ 207$ |
| WBT38G | 38.00 | 0.638 | 90 | 1.61 | $\$ 155$ | $\$ 185$ | $\$ 213$ |
| WBT62G | 62.00 | 0.798 | 130 | 1.74 | $\$ 170$ | $\$ 200$ | $\$ 230$ |
| U54G4 | 54.00 | 1.154 | 130 | 3.40 | $\$ 290$ | $\$ 390$ | $\$ 449$ |
| U54G5 | 54.00 | 1.234 | 130 | 3.44 | $\$ 295$ | $\$ 395$ | $\$ 454$ |
| U54G6 | 54.00 | 1.394 | 120 | 3.48 | $\$ 300$ | $\$ 400$ | $\$ 460$ |
| U66G4 | 66.00 | 1.343 | 155 | 3.44 | $\$ 295$ | $\$ 395$ | $\$ 454$ |
| U66G5 | 66.00 | 1.423 | 150 | 3.48 | $\$ 300$ | $\$ 400$ | $\$ 460$ |
| U66G6 | 66.00 | 1.583 | 145 | 3.53 | $\$ 305$ | $\$ 405$ | $\$ 466$ |
| U78G4 | 78.00 | 1.531 | 170 | 3.70 | $\$ 325$ | $\$ 425$ | $\$ 489$ |
| U78G5 | 78.00 | 1.611 | 170 | 3.79 | $\$ 335$ | $\$ 435$ | $\$ 500$ |
| U78G6 | 78.00 | 1.771 | 165 | 3.88 | $\$ 345$ | $\$ 445$ | $\$ 512$ |
| UF60G4 | 60.00 | 1.342 | 150 | 3.48 | $\$ 300$ | $\$ 400$ | $\$ 460$ |
| UF60G5 | 60.00 | 1.422 | 150 | 3.53 | $\$ 305$ | $\$ 405$ | $\$ 466$ |
| UF60G6 | 60.00 | 1.582 | 135 | 3.57 | $\$ 310$ | $\$ 410$ | $\$ 472$ |
| UF72G4 | 72.00 | 1.530 | 165 | 3.62 | $\$ 315$ | $\$ 415$ | $\$ 477$ |
| UF72G5 | 72.00 | 1.610 | 170 | 3.66 | $\$ 320$ | $\$ 420$ | $\$ 483$ |
| UF72G6 | 72.00 | 1.770 | 160 | 3.70 | $\$ 325$ | $\$ 425$ | $\$ 489$ |
| UF84G4 | 84.00 | 1.719 | 190 | 3.96 | $\$ 355$ | $\$ 455$ | $\$ 523$ |
| UF84G5 | 84.00 | 1.799 | 185 | 4.05 | $\$ 365$ | $\$ 465$ | $\$ 535$ |
| UF84G6 | 84.00 | 1.959 | 170 | 4.14 | $\$ 375$ | $\$ 475$ | $\$ 546$ |
| WF74PTG | 74.00 | 1.020 | 175 | 1.31 | $\$ 120$ | $\$ 150$ | $\$ 173$ |
| W83PTG | 82.61 | 1.087 | 205 | 1.35 | $\$ 130$ | $\$ 155$ | $\$ 178$ |
| W95PTG | 94.49 | 1.167 | 235 | 1.31 | $\$ 145$ | $\$ 150$ | $\$ 173$ |

* W74G is used as basis for relative cost analysis
** The final In-Place Cost is based on 1.15 x Fabrication Cost. Producers should be consulted for shipping circumstances

3. Girder Spacing

Consideration must be given to the slab cantilever length to determine the most economical girder spacing. This matter is discussed in Section 5.6.4.B. The slab cantilever length should be made a maximum if a line of girders can be saved. The spacing of the interior girders must be considered at the same time. Once the positions of the exterior girders have been set, the positions and lengths of interior girders can be established. The following guidance is suggested.
a. Straight Spans

On straight constant width roadways, all girders should be parallel to bridge centerline and girder spacing should be equal.
b. Tapered Spans

On tapered roadways, the minimum number of girder lines should be determined as if all girder spaces were to be equally flared. As many girders as possible, within the limitations of girder capacity should be placed. Slab thickness may have to be increased in some locations in order to accomplish this.
c. Curved Spans

On curved roadways, normally all girders will be parallel to each other. It is critical that the exterior girders are positioned properly in this case, as described in Subsection 5.6.4.B.
d. Geometrically Complex Spans

Spans which are combinations of taper and curves will require especially careful consideration in order to develop the most effective and economical girder arrangement. Where possible, girder lengths and numbers of straight and harped strands should be made the same for as many girders as possible in each span.
e. Number of Girders in a Span

Usually all spans will have the same number of girders. Where aesthetics of the underside of the bridge is not a factor and where a girder can be saved in a short side span, consideration should be given to using unequal numbers of girders. It should be noted that this will complicate crossbeam design by introducing torsion effects and that additional reinforcement will be required in the crossbeam.

## B. Slab Cantilevers

The selection of the location of the exterior girders with respect to the curb line of a bridge is a critical factor in the development of the framing plan. This location is established by setting the curb distance, which is that dimension from centerline of the exterior girder to the adjacent curb line. For straight bridges, the distance between the edge of girder and the curb will normally be no less than $2^{\prime}-6^{\prime \prime}$ for W42G, W50G, and W58G; $3^{\prime}-0^{\prime \prime}$ for W74G; and $3^{\prime}-6^{\prime \prime}$ for WF74G, W83G, and W95G. Some considerations which affect this are noted below.

## 1. Appearance

In the past, some prestressed girder bridges have been designed by placing the exterior girders directly under the curb (traffic barrier). This gives a very poor bridge appearance and is uneconomical. Normally, for best appearance, the largest slab overhang which is practical should be used.

### 5.7 Roadway Slab

The following information is intended to provide guidance for slab thickness and transverse and longitudinal reinforcement of roadway slab. Information on deck deterioration prevention systems is section 5.7.4.

### 5.7.1 Roadway Slab Requirements

A. Slab Thickness

Slab thickness for prestressed girder bridges shall be taken as shown in Table 5.7.2-2.
The minimum slab thickness is established in order to ensure that overloads on the bridge will not result in premature slab cracking.
B. Computation of Slab Strength

The thickness for usual slabs are shown in Figure 5.7.1-1 and Figure 5.7.1-2. The slab design span and thickness are defined in Table 5.7.2-2

The thickness of the slab and reinforcement in the area of the cantilever may be governed by traffic barrier loading. Wheel loads plus dead load shall be resisted by the sections shown in Figure 5.7.1-2.

Cantilever loads may govern the slab thickness just inside the exterior girder as shown by " $Z$ " in Figure 5.7.1-2.

Design of the cantilever is normally based on the expected depth of slab at centerline of girder span. This is less than the dimensions at the girder ends (somtimes).


Depths for Slab Design at Centerline of Girder Span


## Depths for Slab Design at Deck Overhang Figure 5.7.1-2

C. Computation of "A" Dimension

The distance from the top of the slab to the top of the girder at centerline bearing is represented by the "A" Dimension. It is calculated in accordance with the guidance of Appendix B. This ensures that adequate allowance will be made for excess camber, transverse deck slopes, vertical and horizontal curvatures. Ideally the section at centerline of span will have the final geometry shown in Figure 5.7.1-1. Where temporary prestress strands at top of girder are used to control the girder stresses due to shipping and handling, the "A" dimension must be adjusted accordingly.

The note in left margin of the Layout Sheet should read: "A" Dimen. = X " (not for design).


## Notes:

1. Top and bottom mats each carry one-half the tension impact load.
2. Only Design Case 1 of LRFD A13.4.1 is considered. Designer must also check Design Cases 2 and 3.
3. Section considered is a vertical section through the slab overhang at the toe of the barrier.
Prestressed Concrete Superstructure

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8．FOR SAWTOOTH DETALS SEE W42G GIRDER DETALLS 2 OF 2 ．
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IS TEMPORARY STRANDS MAY BE POST－TENSIONED BEFORE THE GIRDER IS
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Appendix A
Prestressed Concrete Superstructure
$42 G$ End Diaphragm
on Girder Details


Appendix A


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Prestressed Concrete Superstructure


W42G Miscelleneous
Diaphragm Details



Appendix A

Appendix A


Appendix A
Prestressed Concrete Superstructure


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Prestressed Concrete Superstructure

Prestressed Concrete Superstructure


WITH A $9^{\prime \prime}$ LONG $90^{\circ}$ HOOK TO WITHIN $3^{\prime \prime}$ CLEAR OF THE BOTTOM OF THE
GIRDER． 6．CAUTION SHALL BE EXERCISED IN HANDLING AND PLACING GIRDERS．ALL
GIRDERS SHALL BE CHECKED BY THE CONTRACTOR TO ENSURE THAT THEY
ARE BRACED ADEQUATELY TO PREVENT TIPPING AND TO CONTROL LATERAL
BENDING DURING SHIPPING．ONCE ERECTED．ALL GIRDERS SHALL BE BRACED BENDING DURING SHIPPING．ONCE ERECTED，ALL GIRDERS SHALL BE BRACED
LATERALLY TO PREVENT TIPPING UNTIL THE DIAPHRAGMS ARE CAST AND LATERALLY
CURED．
  FOR SAWTOOTH DETAILS SEE W58G GIRDER DETAILS 2 OF 3. 9．TEMPORARY STRANDS ARE EITHER PRETENSIONED OR POST－TENSIONED．IF BUT THE END $10^{\prime}$＇－O＂OF THE GIRDER LENGTH．AS AN ALTERNATE， TEMPORARY STRANDS MAY BE POST－TENSIONED BEFORE THE GIRDER IS
LIFTED FROM THE FORM．TEMPORARY STRANDS SHALL BE CUT AFTER ALL
GIRDERS ARE ERECTED，BUT BEFORE DIAPHRAGMS ARE CAST．


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| :--- | :---: | :---: |
| Fixed Diaph．＠interm．Pier | D | NO |




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PRESTRESSED CONCRETE GIRDERS \％ 1



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14 kips per each $0.6^{\prime \prime} \otimes l \mid 1$ ting strand．

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bRIDGE DESIGN MANUAL
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## GIRDER ELEVATION

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Prestressed Concrete Superstructure

Appendix A
Prestressed Concrete Superstructure




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& \frac{\text { CONSTRUCTION }}{\text { SEQUENCE }} \\
& \text { (1) CROSSBEAM } \\
& \text { (2) PLACE GIRDER ON BLOCKS } \\
& \text { (3) DIAPHRAGM STAGE } 2 \\
& \text { (4) ROADWAY SLAB } \\
& \text { (5) COMPLETE DIAPHRAGM }
\end{aligned}
$$

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Appendix A



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PLAN - HINGE DIAPHRAGM
100 MAX. SKEW FOR HINGE DIAPHRAGM.

* FOR EXTENDED STRAND DETALL SEE GIRDER SHEET




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Prestressed Concrete Superstructure

GIRDER ELEVATION


$\begin{aligned} & \text { W74G } \text { Girder } \\ & \text { Details } 1 \text { of } 3\end{aligned}$

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9．TEMPORARY STRANDS ARE EITHER PRETENSIONED OR POSTT－TENSIONED．IF BUT THE END 10＇O＂OF THE GIRDER LENGTT．AS AN ALTERNATE，
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LIITED FROM THE FORM．TEMPRARY STRAND SHAL BE CUT AFTER ALL
GIRDERS ARE ERECTED，BUT BEFORE DIAPHRAGMS ARE CAST．

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Appendix A


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HINGE BAR PLAN

typical hinge section


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POST-TENSIONED ALTERNATE

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Appendix A


bRIdGE design manual


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WF74G Abutment Type Pier
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Prestressed Concrete Superstructure




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Prestressed Concrete Superstructure

WF83G Abutment Type Pier
Diaphragm Details
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Appendix A
Prestressed Concrete Superstructure

Appendix A
Prestressed Concrete Superstructure STRAND PATTERN HAPPED STRAND LOCATION SERUENCE.
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WF95G Abutment Type Pier
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Chapter 10


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Appendix 13.4-A1 Bridge Rating Summary
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### 13.1 General

Bridge Load Rating is a procedure to evaluate the adequacy of various structural components to carry predetermined live loads. The Bridge Load Rating Engineer in the WSDOT Bridge Preservation Office is responsible for the bridge inventory and load rating of existing and new bridges in accordance with the NBIS and the AASHTO Manual for Condition Evaluation of Bridges, latest edition. As presently required, only elements of the superstructure will be rated. Generally, the superstructure shall be defined as all structural elements above the column tops including drop crossbeams.

In order to provide a baseline rating for new bridges, load ratings are required for all new bridges, widened (one lane width or more throughout the length of the bridge), or rehabilitated bridges where the rehabilitation alters the load carrying capacity of the structure. The carrying capacity of a widened or rehabilitated structure shall equal or exceed the capacity of the existing structure.

The Bridge Design Section does not load rate new bridges during the design phase. However, copies of the computer models used in the design process shall be submitted to the Bridge Load Rating Engineer in the Bridge Preservation Section for the more complex structures where computer models were used in the design process.
The Bridge Preservation Office is responsible for maintaining an updated bridge load rating throughout the life of the bridge based on current bridge condition. Conditions of existing bridges change over time, resulting in the need for reevaluation of the load rating. Such changes may be caused by damage to structural elements, extensive maintenance or rehabilitative work, or any other deterioration identified by the Bridge Preservation Office through their regular inspection program.

This criteria applies only to concrete and steel bridges. For timber bridges, rating procedure shall be as per Chapters 6 and 7 of the 1994 AASHTO Manual for Condition Evaluation of Bridges.
Structural elements as defined above shall be evaluated for flexural, vertical shear, and torsional capacities based on Load Resistance Factor Design (LRFR) as outlined in the AASHTO 1989 Guide Specifications for Strength Evaluation of Existing Steel and Concrete Bridges and Load Factor Design (LFD) as outlined in the latest AASHTO Manual for Condition Evaluation of Bridges. Consider all reinforcing, including temperature/distribution reinforcement, in the rating analysis.

By definition, the adequacy or inadequacy of a structural element to carry a specified truck load will be indicated by the value of its rating factor (RF); that is, whether it is greater or smaller than 1.0. For a specific loading, the lowest RF value of the structural elements will be the overall rating of the bridge.

### 13.1.1 WSDOT Rating (LRFR)

Ratings shall be performed per the 1989 AASHTO Guide Specifications for Strength Evaluation of Existing Steel and Concrete Bridges. All bridges, except timber, shall be rated based on the Strength method.
A. Strength Method (LRFR)

The basic rating equations shall be:

$$
\mathrm{RF}=\frac{\Phi \mathrm{R}_{\mathrm{n}}-\gamma_{\mathrm{DL}} \mathrm{D} \pm \mathrm{S}}{\gamma_{\mathrm{L}} \mathrm{~L}(1+\mathrm{I})}
$$

When rating the full section of a bridge, like box girders, or crossbeams, which have two or more lanes, the following formulas apply for the overload trucks:

$$
\mathrm{RF}=\frac{\Phi \mathrm{R}_{\mathrm{n}}-\gamma_{\mathrm{DL}} \mathrm{D} \pm \mathrm{S}-\gamma_{\mathrm{L}} \mathrm{~L}_{\mathrm{Lcgal} \text { Load }}(1+\mathrm{I})}{\gamma_{\mathrm{L}} \mathrm{~L}(1+\mathrm{I})}
$$

The formulas for the overloads assume that there is one overload truck in one lane, and legal trucks occupy the remaining lanes. Trucks shall be placed, in the lanes, in a manner that produces the maximum forces.

Where:
R.F. $=$ Rating Factor (Ratio of Capacity to Demand)
$\underline{\mathrm{R}}_{\underline{n}} \quad=$ Nominal Capacity of Section
D $\quad=$ Calculated Dead Load
$\underline{\text { S }} \quad=$ Secondary Prestressing
$\underline{\mathrm{L}} \quad=$ Calculated Live Load
$\Phi \quad=$ Resistance Factor (Capacity Reduction Factor)
$\gamma_{\mathrm{DL}}=$ Dead Load Factor.
$\gamma_{\mathrm{L}} \quad=$ Live Load Factor
$\gamma_{\mathrm{P}} \quad=$ Prestress Factor
I $\quad=$ Impact
*For continuous structures, a one-half support width moment increase is to be used.
B. Service Method (LRFR)

## Prestressed and Post- tensioned Members

Prestressed and post-tensioned members in positive moment regions, and where posttensioning is continuous over the supports, shall also be rated based on allowable stresses at service loads. The lowest rating factors between Service and Strength methods shall be the governing rating. The rating equations shall be:

Concrete Tension:

$$
\text { R.F. }=\frac{\mathrm{F}_{\mathrm{A}}-\left(F_{D}+F_{P}+F_{S}\right)}{\mathrm{F}_{\mathrm{L}(1+1)}}
$$

Concrete Compression:

$$
\begin{aligned}
& \text { R.F. }=\frac{\mathrm{F}_{\mathrm{A}}-\left(F_{D}+F_{P}+F_{S}\right)}{\mathrm{F}_{\mathrm{L}(1+\mathrm{I})}} \\
& \text { R.F. }=\frac{\mathrm{F}_{\mathrm{A}}-{ }^{1} /{ }_{2}\left(F_{D}+F_{P}+F_{S}\right)}{\mathrm{F}_{\mathrm{L}(1+1)}}
\end{aligned}
$$

Prestressing Steel:

$$
\text { R.F. }=\frac{\mathrm{F}_{\mathrm{A}}-\left(F_{D}+F_{P}+F_{S}\right)}{\mathrm{F}_{\mathrm{L}(1+\mathrm{I})}}
$$

R.F. $=$ Rating Factor (Ratio of Capacity to Demand)

Allowable Concrete Tensile Stress:

$$
\begin{aligned}
\mathrm{F}_{\mathrm{A}} & =6 \sqrt{ } \mathrm{f}^{\prime}{ }_{\mathrm{c}} \\
& =3 \sqrt{ }{ }^{\prime}{ }_{\mathrm{c}} \text { for severe corrosive exposure } \\
& =0 \text { for members without bonded reinforcement }
\end{aligned}
$$

Allowable Concrete compressive Stress:
$\mathrm{F}_{\mathrm{A}}=0.6 \mathrm{f}^{\prime}{ }_{\mathrm{c}}$
$=0.4 \mathrm{f}{ }^{\prime}$ c when checking live load plus one half of the dead and prestress compressive stresses.
Allowable Prestressing Tensile Stress
$\mathrm{F}_{\mathrm{A}} \quad=0.80 \mathrm{f}^{*} \mathrm{y}$ (Allowable Prestressing Tensile Stress) where $f^{*}$ y is the yield stress of the prestressing.
$\mathrm{F}_{\mathrm{D}}=$ Dead Load Stress
$\mathrm{F}_{\mathrm{p}} \quad=$ Stress due to Prestress Force after all losses
FS $=$ Stress due to Secondary Prestress forces
$\mathrm{F}_{\mathrm{L}(1+\mathrm{I})}=$ Stress due to Live Load including Impact
For all loadings, prestress losses shall be per design or current Bridge Design Manual.
For the overload trucks, the allowable stresses shall be increased by 15 percent.

When the bending moment rating for the overload vehicles is less than 1.0 based on the Service Method, and greater than 1.0 based on the Strength Method, the moment rating shall be calculated by dividing the strength rating factor by 1.30 , and the result cannot exceed 1.0.

## Timber Members

R.F. $=\frac{F_{A}-F_{D}}{F_{L}}$
R.F. $=$ Rating Factor (Ratio of Capacity to Demand)
$\mathrm{F}_{\mathrm{A}}=$ Allowable bending stress
$\mathrm{F}_{\mathrm{D}}=$ Dead Load Stress
$\mathrm{F}_{\mathrm{L}}=$ Stress due to Live Load, does not include Impact
$\mathrm{F}_{\mathrm{A}}$ is per AASHTO Standard Specs. with an increase of $33 \%$.
C. Resistance Factors (LRFR)

The resistance factors shall be per Table 3b or Figure 4 of the 1989 AASHTO Guide Specifications for Strength Evaluation of Existing Steel and Concrete Bridges. The resistance factors can be increased up to a maximum of 0.95 , or decreased, depending on the condition, redundancy, type of inspection, and type of maintenance. For state owned bridges, assume careful inspection and vigorous maintenance and for local agency bridges, consult with the agency's Bridge Engineer.
Following are the NBI and BMS condition codes and their interpretation:
For NBI Codes $>$ or $=6($ BMS States 1 and 2$)$ - no deterioration
For NBI Codes $=5($ BMS State 3$)$ - some deterioration
For NBI Codes $<5$ (BMS State 4) - heavy deterioration
The BMS coding shall be used to identify the conditions of the elements being rated, and the appropriate resistance factors shall be applied.

When rating members that have section loss identified in the inspection report, the members should be modeled using the reduced section. Then, use the resistance factors for members in satisfactory condition.
D. Load Factors (LRFR)

Dead Load $\quad \gamma \mathrm{D}=1.20$
Prestress Load $\quad \gamma \mathrm{P}=1.00$
Live Load

1. Low volume roadways (ADTT less than 1,000 ), significant sources of over weight trucks without effective enforcement.

$$
\gamma \mathrm{L}=1.65
$$

2. Heavy volume roadways (ADTT equal to or greater than 1,000 ), significant sources of over weight trucks without effective enforcement. $\gamma \mathrm{L}=1.80$
3. OL-1 and OL-2 (or other permit vehicles). $\gamma \mathrm{L}=1.30$

If ADTT is unavailable from traffic data, it may be estimated as 20 percent of ADT. The listed factors are essentially the same as Table 2 of AASHTO Guide Specifications except that Live Load Category 1 and 2 have been eliminated based on the assumption that Washington State does not have effective enforcement or control of overloads.
E. Impact (LRFR)

For new bridge designs, impact shall be 10 percent (0.1).
For existing bridges, the impact factor shall be determined by the approach roadway and the deck condition. For approach roadway condition codes 6 or greater, assume 10 percent impact; for codes less than 6 , assume 20 percent impact. If the bridge deck condition is 6 or greater or has 0 to 4 percent scaling, assume 10 percent impact; if the deck condition is 5 or has between 5 and 15 percent scaling, assume 20 percent impact; if the deck condition is 4 or less and has greater than 15 percent scaling, assumes 30 percent impact.
F. Live Load Reduction Factors (LRFR)

| Number of Loaded Lanes | Reduction Factor |
| :---: | :---: |
| One or two lanes | 1.0 |
| Three lanes | 0.8 |
| Four lanes or more | 0.7 |

G. Live Loads (LRFR)

The moving loads for the rating shall be the HS-20 truck/lane loading (Figure 13.1-1), three legal trucks/ lane load (Figure 13.1-2), and two overload trucks. (Figure 13.1-3). The legal lane load shall be used to rate structures with spans over 200 feet. For the two overload trucks (OL-1 and OL-2), use only one overload truck occupying one lane in combination with one of the AASHTO legal trucks in each of the remaining lanes, when modeling the full section of the bridge or cross-beams. The number of lanes used shall be the actual striped lanes at the time of rating.
The three legal trucks and legal lane load, Type 3, Type 3S2, and Type 3-3, are to be used to determine posting limits. The two overload vehicles represent extremes in the limits of permitted vehicles in Washington State.
H. Rating Trucks

## Design Trucks



HS-20 Truck


## HS-20 Lane Load

* In negative moment regions of continuous spans, place an equivalent load in the other span to produce the maximum effect.

Figure 13.1-1

Legal Trucks


Type 3 Truck


Type 3S2 Truck


Type 3-3 Truck


Legal Lane Load
Figure 13.1-2

## Overload Trucks

$10 \mathrm{~K} \quad 21.5 \mathrm{~K} \quad 21.5 \mathrm{~K} \quad 21.5 \mathrm{~K} \quad 21.5 \mathrm{~K}$


## Overload 1



Overload 2
Figure 13.1-3

### 13.1.2 NBI Rating (LFR)

Ratings shall be performed per the latest AASHTO Manual for Condition Evaluation of Bridges. All bridges, except timber, shall be rated based on the Load Factor method. The HS20 Truck/ Lane shall be used to calculate the Inventory and Operating Ratings.
A. Strength Method (LFR)

The basic equation shall be:
R.F. $=\frac{\Phi \mathrm{R}_{\mathrm{n}}-\gamma_{\mathrm{DL}} \mathrm{D} \pm \mathrm{S}}{\gamma_{\mathrm{L}} \mathrm{L}(1+\mathrm{I})}$

Where:
R.F. $=$ Rating Factor (Ratio of Capacity to Demand)
$\mathrm{R}_{\mathrm{n}}=$ Nominal Capacity of the Member
$\Phi=$ Resistance Factor (Per AASHTO Standard Specs.)
D = Unfactored Dead Load
L = Unfactored Live Load
S = Unfactored Prestress Secondary Moment or Shear
I = Impact Factor, Span dependant (Per AASHTO Standard Specs.)
$\gamma_{\mathrm{DL}}=1.3$ (Dead Load Factor)
$\gamma_{\mathrm{L}}=2.17$ for Inventory (Live Load Factor)
$=1.30$ for Operating
Truck/Lane shall be used to calculate the Inventory and Operating Ratings.
B. Service Method (LFR)

1. Prestressed and Post-tensioned Members

Prestressed and post-tensioned members in positive moment regions, and where post-tensioning is continuous over the supports, shall also be rated based on allowable stresses at service loads. The lowest rating factor between Service and Load Factor methods shall be the governing Inventory rating. The Operating rating shall be based on the load factor method using a Live Load factor of 1.30. Service ratings for the HS20 shall be the same as stated in Section 13.1.1.B, except the impact factor shall be span dependant.
2. Timber Members
R.F. $=\frac{F_{A}-F_{D}}{F_{L}}$
R.F. $=$ Rating Factor (Ratio of Capacity to Demand)
$\mathrm{F}_{\mathrm{A}}=$ Allowable bending stress
$\mathrm{F}_{\mathrm{D}}=$ Dead Load Stress
$\mathrm{F}_{\mathrm{L}}=$ Stress due to Live Load, does not include Impact

* $\mathrm{F}_{\mathrm{A}}$, for Inventory rating, shall be per AASHTO Standard Specifications. For Operating Ratings, $\mathrm{F}_{\mathrm{A}}$ shall be per AASHTO Standard Specifications with a $33 \%$ increase in the allowable stress.
C. Resistance Factors (LFR)

The resistance factors for NBI ratings shall be per the latest AASHTO Standard Specifications. Following are the NBI resistance factors:

| Steel Members: | 1.00 (Flexure) |
| :--- | :--- |
|  | 1.00 (Shear) |
| Prestressed Concrete | 1.00 (Flexure, Positive moment) |
|  | 0.90 (Shear) |
| Post-tensioned, Cast in place: | 0.95 (Flexure, Positive moment) |
|  | 0.90 (Shear) |
| Reinforced Concrete: | 0.90 (Flexure) |
|  | 0.85 (Shear) |

For prestressed and post-tensioned members, where reinforcing steel is used to resist negative moment, the resistance factors for reinforced concrete section shall be used in the ratings.
D. Live Loads

The HS-20 truck or lane shall be used to load rate bridge members. The number of lanes shall be per AASHTO Standard Specifications, Section 3.6. When multiple lanes are considered, apply the appropriate multilane reduction factor given in Section 13.1.2.F. Load distribution methods are discussed under specific bridge types. Do not consider sidewalk live loads in rating analysis.
E. Impact (LFR)

Impact is expressed as a fraction of the live load stress, and shall be determined by the following formula:
$I=\frac{50}{125+L}$
I = Rating Factor (Ratio of Capacity to Demand)
$\mathrm{L}=$ Length in feet of the portion of the span that is loaded to produce the maximum stress in the member.
*AASHTO Standard Specifications for Highway Bridges 3.8.2.1.
F. Live Load Reduction Factors (LFR)

| Number of Loaded Lanes | Reduction Factor |
| :---: | :---: |
| One or two lanes | 1.0 |
| Three lanes | 0.9 |
| Four lanes or more | 0.75 |

### 13.2 Special Rating Criteria

### 13.2.1 Dead Loads

Dead Loads shall be as defined in the AASHTO Standard Specifications for Highway Bridges, except concrete weight shall be 155 pcf .

### 13.2.2 Live Load Distribution Factors

Live Load distribution factors shall be per Chapter 3 of the AASHTO Standard Specifications for Highway Bridges. Distribution factors are selected assuming one traffic lane where the roadway is less than 20 feet wide or two or more traffic lanes where the roadway is 20 feet or wider.

### 13.2.3 Reinforced Concrete Structures

For conventional reinforced concrete members of existing bridges, checking of serviceability shall not be part of the rating evaluation.
Rating for shear in the longitudinal direction shall begin at a distance ${ }^{h} / 2$ from the centerline of the bearing or face of integral cross beams ( $\mathrm{h}=$ total depth).

### 13.2.4 Concrete Decks

For all concrete bridge decks, except flat slab bridges, that are designed per current AASHTO criteria for HS-20 loading or heavier, loading will be considered structurally sufficient and need not be rated. However, for existing bridge decks having any of the following conditions, rating of the deck is required:

1. Deck was designed for live loads lighter than HS-20.
2. Deck overhang is more than half the girder spacing.
3. Bridge Inspection Report Code is 4 or below.
4. When the original traffic barrier(s) or rail have been replaced by heavier barrier.

When rating of the deck is required, live load shall include all vehicular loads as specified in Section 13.1.1.H. Live load moments for the HS20 truck shall be per Section 3.24.3.1 of the AASHTO Standard Specifications. Live load moments for the legal and overload trucks shall be per the AASHTO Manual for Maintenance Inspection of Bridges.

### 13.2.5 Concrete Crossbeams

Live loads can be applied to the crossbeam as moving point loads at any location between curbs that produce the maximum effect.

When rating for shear in crossbeams, current AASHTO Design Specifications requires shear design to be at the face of support if there is a concentrated load within a distance "d" from the face of support. This requirement is new relative to earlier editions of AASHTO Design Specifications that allowed shear reinforcement design to be at a distance " d " from the face of support. When rating existing crossbeams that show no indication of distress on the latest inspection report, but have a rating factor of less than one (1.0), a more detailed/accurate shear analysis should be performed. One acceptable method is the "Strut and Tie" model analysis. For existing box girders and T-beams integral with the crossbeams, in lieu of this detailed analysis, dead and live loads can be assumed as uniformly distributed and the shear rating performed at a distance "d" from the face of support.

### 13.2.6 In-Span Hinges

For in-span hinges, rating for shear and bending moment should be performed based on the reduced cross-sections at the hinge seat. Diagonal hairpin bars are part of this rating as they provide primary reinforcement through the shear plane.

### 13.2.7 Concrete Box Girder Structures

Bridges with spread box girders shall be rated on a per box basis. Otherwise, the rating shall be on the per bridge basis for all applied loads.

### 13.2.8 Prestressed Concrete Girder Structures

Rate on a per member basis.

### 13.2.9 Concrete Slab Structures

Rate cast-in-place solid slabs on a per foot of width basis. Rate precast panels on a per panel basis. Rate cast-in-place voided slabs based on a width of slab equal to the predominant center-to-center spacing of voids.

When rating flat slabs on concrete piling, assume pin-supports at the slab/pile interface of interior piers and the slab continuous over the supports. If ratings using this assumption are less than 1.0 , the piles should be modeled as columns with fixity assumed at 10 feet below the ground surface.

Pile caps are to be rated if deemed critical by the engineer.

### 13.2.10 Steel Structures

On existing bridges, checking of fatigue and serviceability shall not be part of the rating evaluation.

### 13.2.11 Steel Floor Systems

Floorbeams and stringers shall be rated as if they are simply supported. Assume the distance from outside face to outside face of end connections as the lengths for the analysis. Live loads can be applied to the floorbeam as moving point loads at any location between curbs, which produce the maximum effect.

Rating of connections is not required unless there is evidence of deterioration.

### 13.2.12 Steel Truss Structures

Rate on a per truss basis or perform a 3-D analysis or simplified distribution methods. Assume nonredundancy of truss members and pinned connections.

In general, rate chords, diagonals, verticals, end posts, stringers, and floorbeams. Do not rate connections unless there is evidence of deterioration, except connections with structural pins. For pin-connected trusses, analyze pins for shear, and the side plates for bearing capacity.

For truss members that have been heat-straightened three or more times, deduct 0.1 from $\phi(\mathrm{Phi})$.

### 13.2.13 Timber Structures

Unless the species and grade is known, assume Douglas fir, select structural for members installed prior to 1955 and Douglas fir, No. 1 after 1955. The allowable stresses for beams and stringers shall be as listed in the AASHTO Standard Specifications.
The nominal dimensions should be used to calculate dead load, and the net dimensions to calculate section modulus. If the member is charred, it may be assumed that $1 / 4$-inch of material is lost on all surfaces. Unless the member is notched or otherwise suspect, shear need not be calculated.

When calculating loads, no impact is assumed.

### 13.2.14 Widened or Rehabilitated Structures

For widened bridges, rate crossbeams in all cases.
For existing bridges, a load rating shall be performed if the load carrying capacity of the longitudinal members is altered, or the dead and live loads have increased due to the widening.
Longitudinal rating for the widened portion will be required only when the width of the widened portion on one side of the structure is greater than or equal to $10^{\prime}-0^{\prime \prime}$ or more throughout the length of the structure.

For rehabilitated bridges, a load rating will be required if the load carrying capacity of the structure is altered by the rehabilitation.

### 13.3 Load Rating Software

Rating of State bridges shall be performed using the BRIDG for Windows software, latest version.

For more complex structures such as Steel Curved girders and Arches, different software may be used to analyze the loads after obtaining approval from the Load Rating Engineer.

