WSDOT's Development of Standard Plans for Buried Structures in Support of Fish Passage



### WILLIAM J. MILLER III









Photo Credit: scenicwa.com/ road-trips



Photo Credit: Meegan M. Reid / Kitsap Sun, File

### Problem Statement

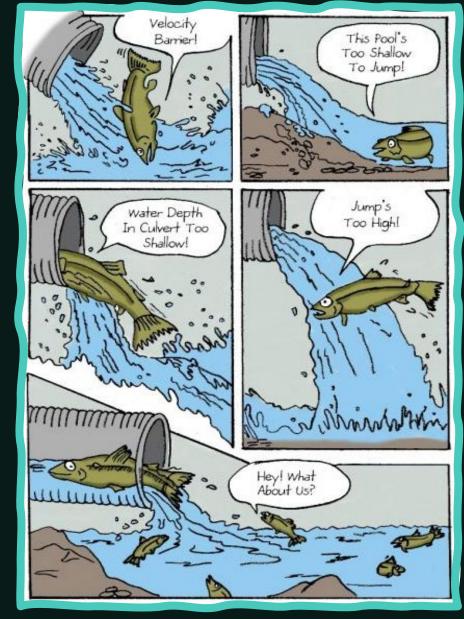


- State highways cross streams & rivers throughout Washington State.
- Substandard pipes & Culverts impede fish migration.
- Fish barriers block access to important spawning & rearing habitat.

### Problem Statement

Fish Passage Barriers (Culverts):

- Hinder fish from moving upstream or downstream.
- Allow water flow, but don't always allow fish to swim through.
- The flow is too swift, too shallow, or has a waterfall at the inlet or outlet.





### Problem Statement

- In 1991, WSDOT created a dedicated fish passage program.
- Correcting hundreds of barriers, restoring miles of habitat.
- Fish barrier correction has created an opportunity to employ Buried
   Structures.

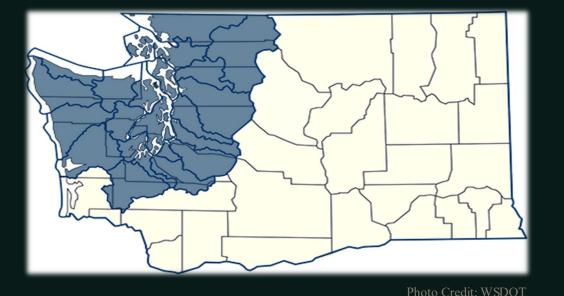


Photo Credit: wildsalmoncenter.org





Photo Credit: www.jvib.com.au





March 2013's Federal Court Injunction:

- Tribes reserved "the right of taking fish" under the Stevens Treaties.
- Requires increased efforts for removing barrier Culverts by 2030.
- Concentrated most of WSDOT's fish passage work within western WA.

Problem Statement



### Project Description

- WSDOT has a significant number of fish barrier removal projects to deliver.
- Many involve replacing existing substandard **Culverts** with new fish-friendly **Buried Structures**.
- To reduce design and construction costs, WSDOT has develop Standard Plans.

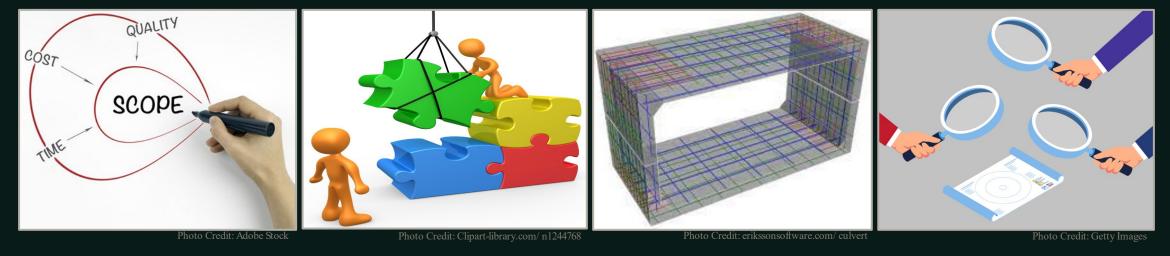


Photo Credit: Johnny Armstrong, wildsalmoncenter.org



# Buried Structure Standard Plans

Scope of Work Basis of Analysis Development Quality Reviews Publication & Beyond



WESTERN BRIDGE ENGINEERS' SEMINAR



# Scope of Work

Analysis Phase Design Phase

Deliverables & Schedule

### Analysis Phase

WSDOT conducted initial parametric studies, prescribing feasible deign ranges.

WSP then preformed the structural and load rating analyses.

Hydrology – Geology – Seismic Hazard – Settlement – Burial Depth – Span Length



### Design Phase

WSDOT then selected what spans and cover to develop **Standard Plans** for. WSP then developed the necessary **Standard Plan** details. WSDOT simultaneously revised agency publications and specs.



### Deliverables

### Standard Plans

Design Calculations

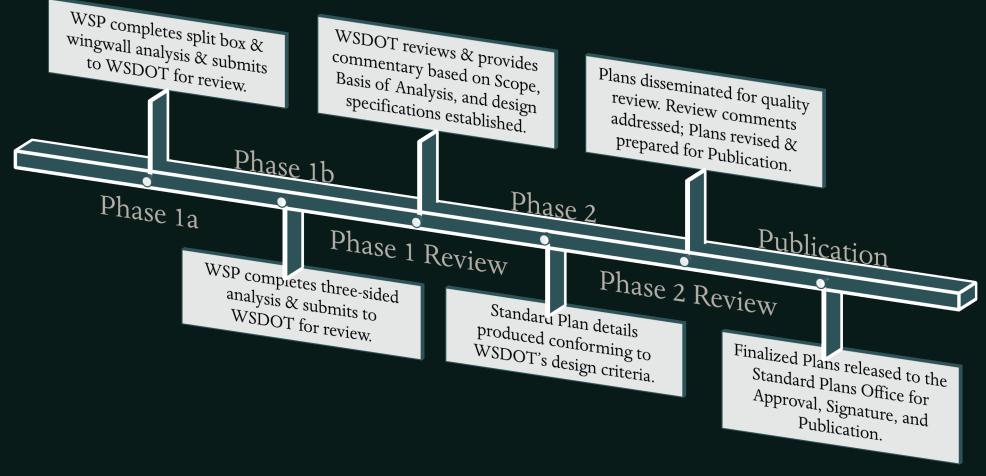
Design Examples

### Load Rating Calculations





### Schedule





# Basis of Analysis

Split Box Three-Sided Wingwalls

### WSDOT Provided Recommendations

### HYDROLOGY GEOTECHNICAL

### MATERIAL



Photo Credit: interfluve.com



Photo Credit: centralgeotech.com

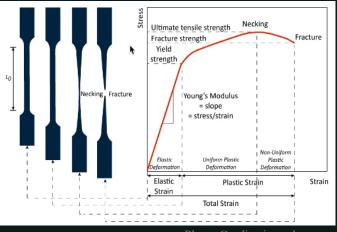


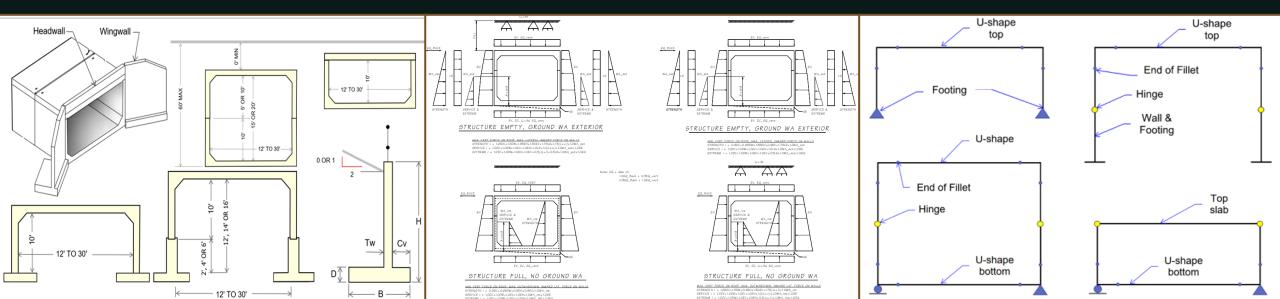
Photo Credit: simscale.com

### Basis of Analysis

Defines the design criteria used for developing **Standard Plans** for split box and three-sided **Buried Structures**, including wingwall and headwall elements.

Geometrics – Materials – Loads – Factors – Combinations – Structural Analysis

Modeling – Limit States – Resistance Factors – Principals of Design





# Development

Eriksson Software

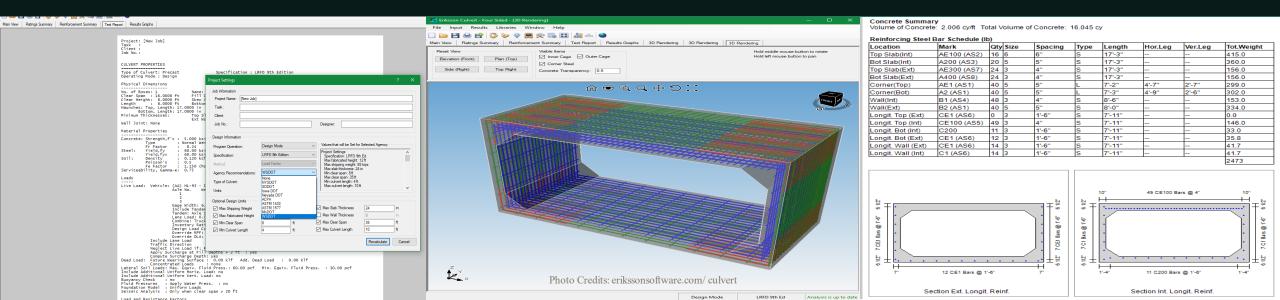
Coordination Efforts

Technical Challenges

### Eriksson Software

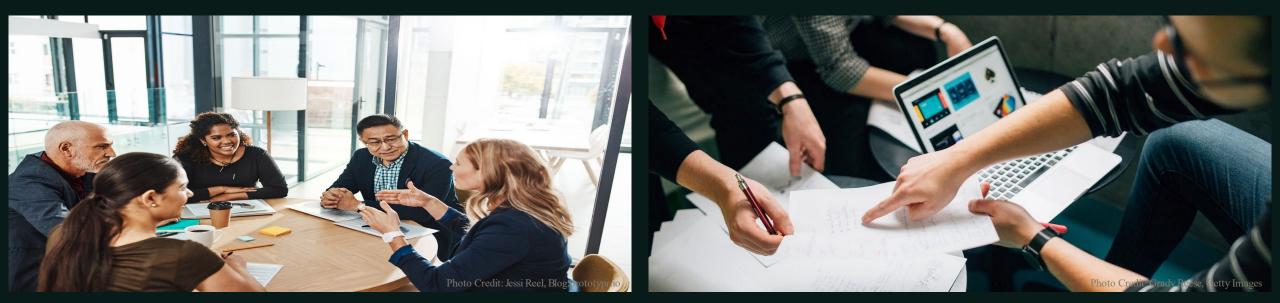
The Bridge Office worked with Eriksson's software development team to incorporate WSDOT's "wish-list" into their product *Culvert*.

This effort provided us with a specialized design tool catered to WSDOT's specific design criteria.



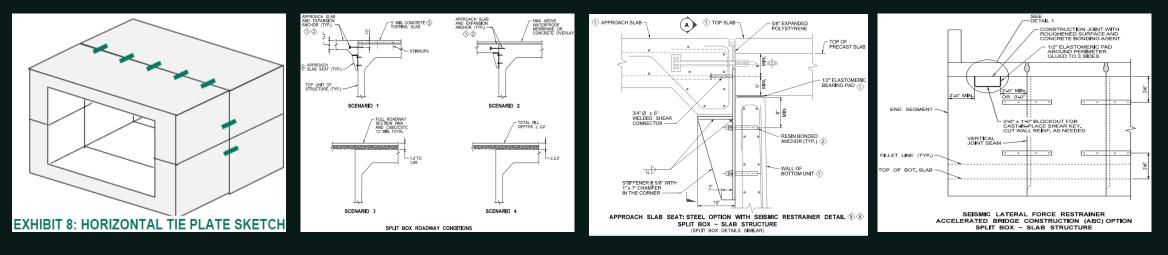
### Development

# WSDOT held roundtable meetings with our Geotechnical Office & hosted weekly check-in meetings with WSP.



# Spotlighting Technical Challenges

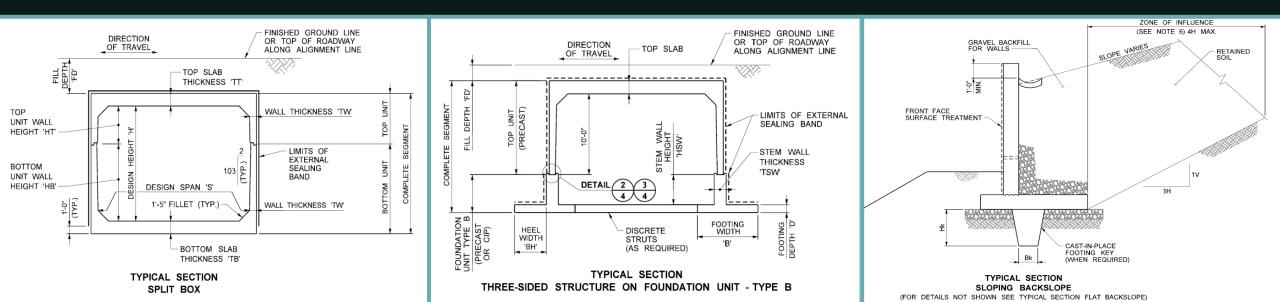
- Tie Plates
- Shear Transfer
- Approach Slab Seats
- Seismic Requirements





### WSDOT's NEW Standard Plans:

- E-20.10-00 Buried Structure Split Box
- E-20.20-00 Buried Structure Three-Sided
- D-20.10-00 Precast Reinforced Concrete Retaining Wall (for wingwalls)





# Quality Reviews

Industry – Constructability Statewide – Agency and Regional Federal – FHWA

### Quality Reviews



### **Internal Review**

Colleagues S.M.E.'s Technical Committees

### Industry Review

Manufacturers AGC Teams: Roadway & Structures



### Statewide Review

Headquarters Region Local Agencies



U.S. Department of Transportation Federal Highway Administration

FHWA Review

Federal Evaluation



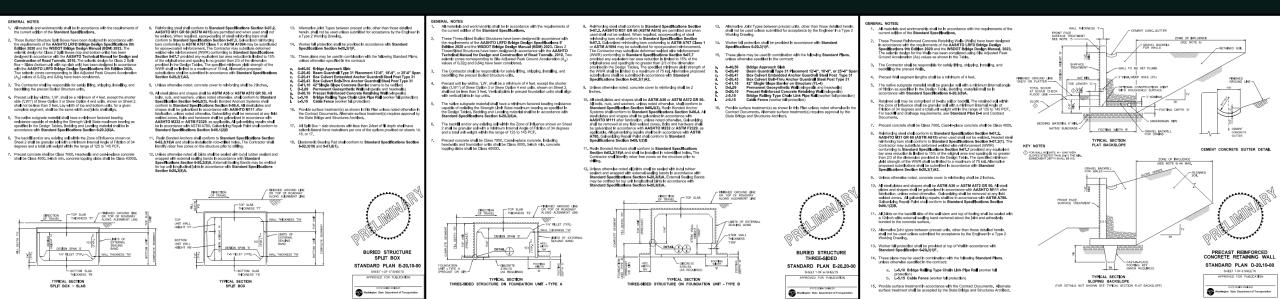
## Publication & Beyond

Remaining Timeline Approval & Publishing What's Next

### Publication

- FHWA approval is received on Plans
- HQ-Bridge release to Standard Plans Office for final preparations
- Approval and signatures from the appropriate appointed authorities requested.

### These new Standard Plans are scheduled to be published this September!





### What's Next

Questions - Training - Education - Lessons Learned - Reactionary Updates





### In Summary

- Facilitates Delivery of a Large Fish Program
- Streamlines Design Efforts
- Establishes Consistency for Design & Fabrication
- Reduces Design & Review of Design Timelines
- The culmination of over three decades of effort
- Allows versatility in navigating summer month's weather, events, and design challenges.





### GENERAL NOTES

- All materials and workmanship shall be in accordance with the requirements of the current edition of the Standard Specifications.
- 2. These Buried Structure Split Boxes have been designed in accordance with the requirements of the AASHTO LRFD Bridge Design Specifications 9th Edition 2020 and the WSDOT Bridge Design Manual (BDM) 2023. The seismic design for Class 2 Split Boxes (top and bottom units) has been designed in accordance with the AASHTO Technical Manual for Design and Construction of Road Tunnels, 2010. The seismic design for Class 2 Split Box ~ Slabs (bottom unit with top slab unit) has been designed in accordance with the AASHTO LRFD Bridge Design Specifications 9th Edition 2020. Two seismic zones corresponding to Site Adjusted Peak Ground Acceleration (A<sub>e</sub>) values of 0.32g and 0.64g have been considered.
- 3. The Contractor shall be responsible for safely lifting, shipping, installing, and backfilling the precast Buried Structure units.
- 4. Precast unit lay widths, 'LW', shall be a minimum of 4 feet, except the shorter side ('LW1') of Skew Option 3 or Skew Option 4 end units, shown on Sheet 2. shall not be less than 3 feet. Lay width of top and bottom units, for a given complete segment, shall be the same width and joints shall align.
- The native subgrade material shall have a minimum factored bearing resistance capable of resisting the Strength Limit State maximum bearing as specified in the Design Tables. Bedding and Leveling material shall be in accordance with Standard Specifications Section 6-20.3(6)A
- 6. The backfill and/or any existing soil within the Zone of Influence shown on Sheet 2 shall be granular soil with a minimum Internal Angle of Friction of 34 degrees and a total unit weight within the range of 120 to 145 PCF.
- 7. Precast concrete shall be Class 7000. Headwalls and cast-in-place concrete shall be Class 4000, 5-inch min, concrete topping slabs shall be Class 4000D

- Reinforcing steel shall conform to Standard Specifications Section 9-07.2. 8 AASHTO M31 GR 60 (ASTM A615) are permitted and when used shall not be welded. When required, epoxy-coating of steel reinforcing bars shall conform to Standard Specification Section 9-07.3. Galvanized reinforcing bars conforming to ASTM A767 Class 1 or ASTM A1094 may be substituted for epoxy-coated reinforcement. The Contractor may substitute deformed welded wire reinforcement (WWR) conforming to Standard Specifications Section 9-07.7 provided any equivalent bar area reduction is limited to 15% of the original area and spacing is no greater than 2/3 of the dimension provided in the Design Tables. The specified minimum yield strength of the WWR shall be limited to a maximum of 75 ksi. Alternative proposed substitutions shall be submitted in accordance with Standard Specifications Section 6-20.3(1)A2.
- Unless otherwise noted, concrete cover to reinforcing shall be 2 inches.
- 10. All steel plates and shapes shall be ASTM A36 or ASTM A572 GR 50. All bolts, nuts, and washers, unless noted otherwise, shall conform to Standard Specification Section 9-06.5(3). Resin Bonded Anchors Systems shall conform to Standard Specifications Section 9-06.4. All steel plates and shapes shall be galvanized in accordance with AASHTO M111 after fabrication, unless noted otherwise. Galvanizing shall be removed at any field welded zones. Bolts and hardware shall be galvanized in accordance with AASHTO M232 or ASTM F2329, as applicable. All galvanizing repairs shall be in accordance with ASTM A780. Galvanizing Repair Paint shall conform to Standard Specifications Section 9-08.1(2)B
- 11. Resin Bonded Anchors shall conform to Standard Specifications Section 6-02,3(18)A and shall be installed in roto-drilled holes. The Contractor shall identify rebar free zones on the structure prior to drilling.
- 12. Unless otherwise noted all joints shall be sealed with Butyl Rubber Sealant and wrapped with External Sealing Bands in accordance with Standard Specifications Section 6-20.3(8)A.

- 13. Alternative Joint Types between precast units, other than those detailed herein, shall not be used unless submitted for acceptance by the Engineer in a Type 2 Working Drawing.
- 14. Worker, Pedestrian and Bicycle Fall Protection shall be provided in accordance with Standard Specifications Section 6-20.3(1)F.
- These plans may be used in combination with the following Standard 15. Plans, unless otherwise specified in the contract:
- A-40.50 Bridge Approach Slab a.
- C-20.40 Beam Guardrail Type 31 Placement 12'-6", 18'-9", or 25'-0" Span b.
- c. C-20.41 Box Culvert Embedded Anchor Guardrail Steel Post Type 31
- d. C-20.43 Box Culvert Bolt-Thru Anchor Guardrail Steel Post Type 31
- C-81.10 42"Single Slope Barrier on Structure (TL-4) e.
- D-3.09 Permanent Geosynthetic (wingwall and headwalls) f.
- D-20.10 Precast Reinforced Concrete Retaining Wall (wingwalls) g. L-5.10 Bridge Railing Type Chain Link Pipe Rail (worker fall protection) h.
- Cable Fence (worker fall protection) i., L-5.15
- Provide surface treatment(s) as shown in this Plan unless noted 16. otherwise in the Contract Documents. Alternate surface treatment(s) requires approval by the State Bridge and Structures Architect.
- 17. All Split Box ~ Slab structures with less than 2 feet of Fill Depth shall have seismic lateral force restrainers per one of the options provided on sheets 14, 16, or 17.
- 18. Elastomeric Bearing Pad shall conform to Standard Specifications Section 6-02.3(19) and 9-31.8(1).
- 19 For Structure Free Zone, freeboard, and maintenance clearance, see Contract Documents.

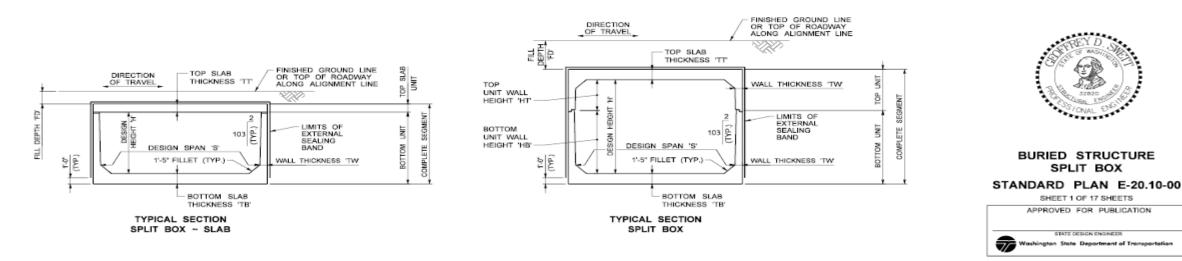
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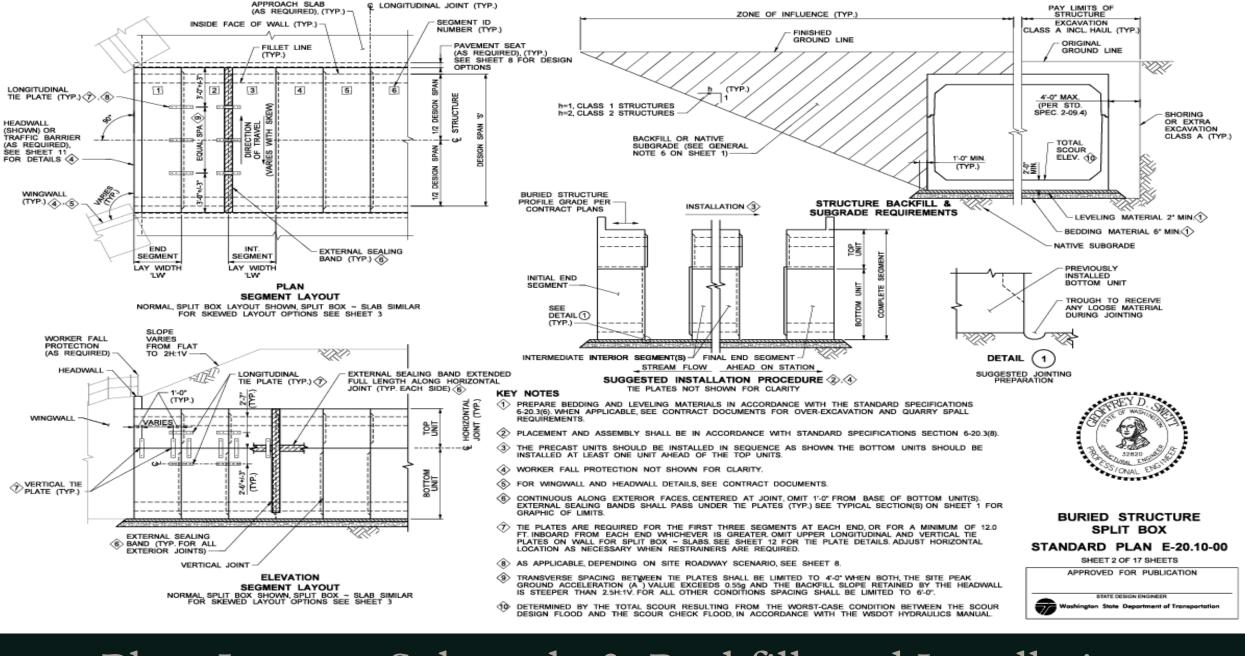
SPLIT BOX

SHEET 1 OF 17 SHEETS

STATE DESIGN ENGINEER

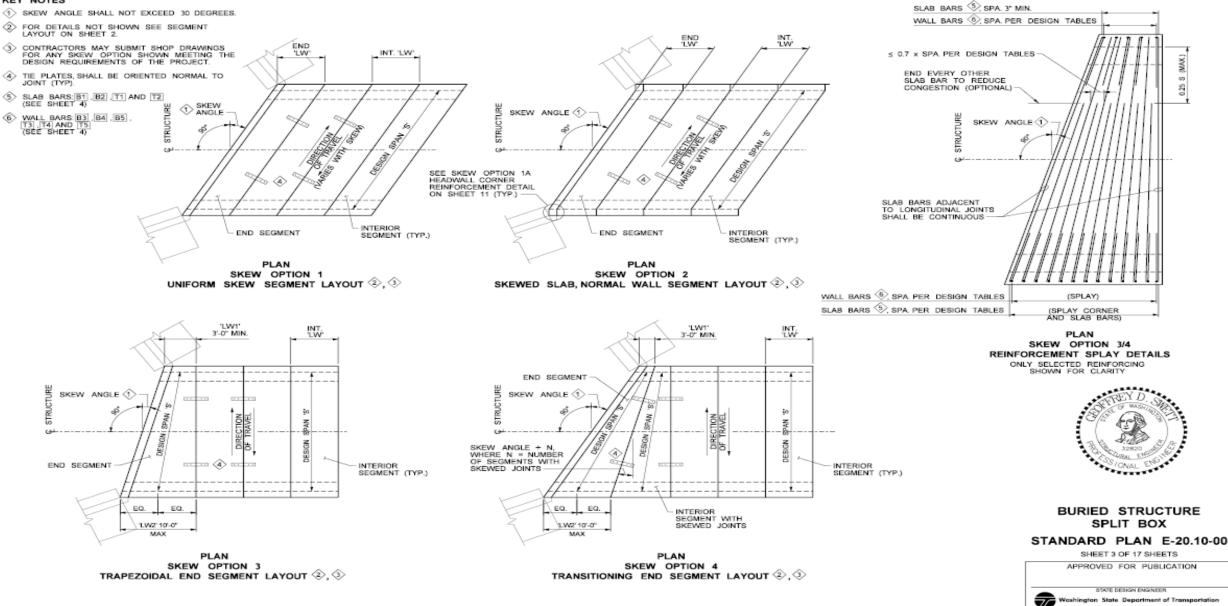


General Notes & Typical Section

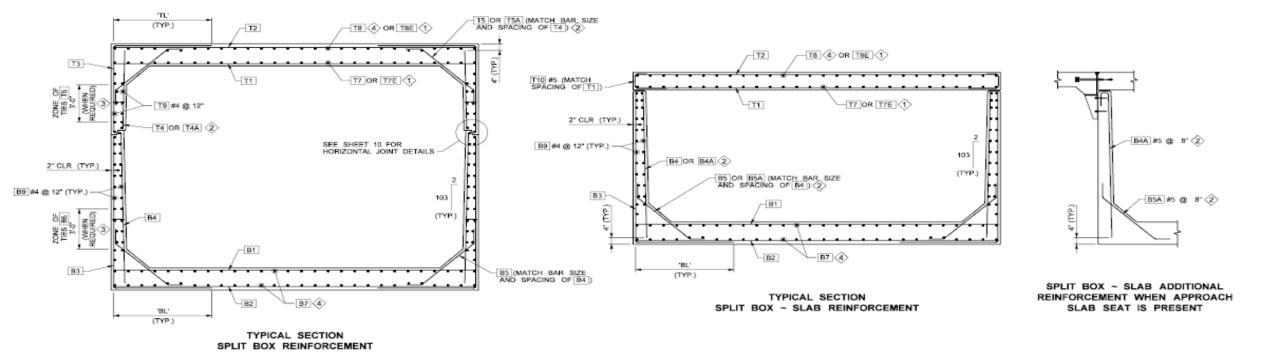


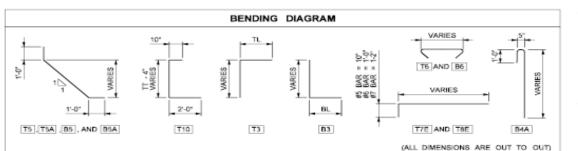
Plan, Layout, Subgrade & Backfill, and Installation

### KEY NOTES









### KEY NOTES

- BARS TTE AND THE SHALL BE INSTALLED IN THE END SEGMENTS. ROTATE 90° HOOK AS
   NECESSARY TO PROVIDE THE SPECIFIED CLEARANCE.
  - SIZE AND SPACING OF BARS T/E SHALL MATCH T/
  - BARS THE SHALL BE AS FOLLOWS:
  - END SEGMENT WITHOUT HEADWALL OR TRAFFIC BARRIER: #5 @ 12" END SEGMENT WITH UP TO 2-0" HEADWALL: #6 @ 12" END SEGMENT WITH UP TO 4-0" HEADWALL: #6 @ 6" END SEGMENT WITH TRAFFIC BARRIER: #7 @ 6" FOR ADDITIONAL END SEGMENT DETAILS SEE SHEET 11.
- WHEN AN APPROACH SLAB SEAT IS PRESENT, ADDITIONAL REINFORCEMENT IS REQUIRED AS FOLLOWS:
- FOR SPLIT BOX SLAB STRUCTURES: ADD B4A #5 @ 8' AND B5A #5 @ 8'. BUNDLE WITH TYPICAL B4 AND B5 RESPECTIVELY.
- FOR SPLIT BOX STRUCTURES: ADD T4A #5 @ 8" AND T5A #5 @ 8". BUNDLE WITH TYPICAL T4 AND T5 RESPECTIVELY.
- TIES T8 #4 AND B6 #4 SHALL BE SPACED AT 6" MAX. VERTICALLY AND AT 2"-0" MAX. HORIZONTALLY. EACH TIE SHALL BE HOOKED AROUND LONGITUDINAL BARS [T9] OR [89]. ADDITIONAL BARS [T9] AND [89] MAY BE ADDED TO FACILITATE PLACEMENT OF TIES AS REQUIRED.
- (4) BARS[B7]AND [78]SHALL BE #4 @ 12" WHEN CORRESPONDING SLAB THICKNESS ≤ 20 INCHES, AND #4 @ 9" FOR THICKER SLABS.



### BURIED STRUCTURE SPLIT BOX

### STANDARD PLAN E-20.10-00

SHEET 4 OF 17 SHEETS

APPROVED FOR PUBLICATION

STATE DESIGN ENGINEER Washington State Department of Transportation

# Reinforcement Identity & Bending Diagram

### DESIGN HEIGHT MEMBER THICKNESS TOP UNIT REINFORCEMENT 3 BOTTOM UNIT REINFORCEMENT (3) MATERIAL QUANTITIES STR. I REQ'D T2 T4 B1 **B**2 DESIGN EII I 177 B3 T3 TOP BOT (SLAB (SLAB (WALL (SLAB (SLAB BOTTOM UNIT REARING HORIZ TOP BOI (WALL TOP UND SPAN DEPTH TOTAL UNIT UNIT WALLS (CORNER) T6 | (BOT.) (CORNER) B6 DEMAND JOINT INTERIOR) EXTERIOR INTERIOR INTERIORI EXTERIOR INTERIOR) SLAB SLAB s FD WALL WALL TW TIES) TIES (PSF) TYPE Π TB CONC. STEEL CONC. STEEL HT HB SIZE SPA SIZE SPA SIZE SPA. SIZE SPA SIZE SPA. SIZE SPA SIZE SPA SIZE SPA. SIZE SPA TL BL $\hat{\mathcal{D}}$ $\hat{2}$ $\hat{\mathcal{D}}$ $\langle 4 \rangle$ 6 CY/FT) (LBS/FT) (CY/FT) (LBS/FI $0' \leq FD \leq 2$ 10" 12 10' #7 6" #5 12 #4 8 #5 10' #6 6\* #7 5" #7 5" 3-2 24 8 0.58 106.1 1.06 322.5 2397 2 10\* 12 10 #7 6 #5 12 #4 12\* #8 6\* #7 #7 5 3-2 24 8 0.58 98.4 1.06 322.5 2490 $2 \le FD \le 4$ 5 2 8 67 12' 10 N/A 10' 4 < FD ≤ 6 12\* 12 12 #8 87 #5 12 N/A #4 N/A #44 12 67 665 57 #7 4-3 814 8 NIA 0.59 112.8 1.28 318.9 2901 8 #6 2 6'< FD < 8' 12\* 12 12 #8 6" #5 12 #4 8 #4 12 #6 6\* #7 5 #7 5" 3'-4' 214 8 0.59 112.8 1.28 327.7 3255 2 12" 12\* #9 #5 12" #4 #6 10\* 67 #7 57 57 0.59 150.3 1.28 382.2 3631 8'< FD ≤ 10 6" 8 #7 部 3-8 #4 8\* 2 0' ≤ FD < 2' 10" 12 10\* #9 6" #5 12 #4 8" #4 12' #8 6\* #6 5" #7 5\* 3'-11 #4 8 0.69 157.2 1.15 361.0 2269 2 10 NZA 10 2'≤ FD ≤ 4' 107 12 10 #8 6 #5 12 #44 12' #8 67 #8 57 #7 57 5'-1' 214 8 0.69 138.3 1.15 378.8 2313 8 N/A N/A N/A #5 10\* 12\* #7 57 121 12 #9 6" #4 81 #4 67 #8 57 4-1 163.6 2 $4 \le FD \le 8$ 14' #9 #44 8 0.81 1.39 399.5 3147 #6 #6 8'< FD ≤ 10' 12" 16' 14\* #9 67 12' <u>#4</u> 87 #5 10\* #8 67 57 #8 157 3.7 #14 8 0.91 183.0 1.50 422.7 3625 $0' \leq FD < 2'$ 10" 12 10 #9 6" #6 7\* #6 3'-0" #4 8" #5 9" #8 67 #5 10\* #6 57 4.4 #4 8 0.99 272.1 1.15 301.1 2030 7" 1 $2 \le FD \le 4$ 10\* 12 10" #9 6" #6 7\* #6 7\* 3'-0" #4 8 #4 12\* #8 6\* #5 12\* 前日 6\* 4-9 #4 8 0.99 260.1 1.15 282.2 1992 4 < FD ≤ 8 10\* 14" 12\* #9 6" #5 10' #5 5" 5'-2" 114 8" #4 12\* #9 6\* #5 10\* #6 5\* 3'-9" #4 8 1.09 244.9 1.26 315.9 2792 N'A **N/A** 15 12 8'< FD < 12' 12" 16' 14 #10 6" #6 12 #5 6" 3'-10' #4 8 #4 12\* #9 6\* 12 #7 6" 3'-5' 214 8 1.27 273.3 1.50 342.9 3739 57 12< FD < 16 167 #10 81 46 12\* 6\* #44 24.4 12\* 67 10/ #7 3.7 81 375.3 TO TO 181 **BR** 31-91 R #19 105 #14 1.38 292.3 1.60 4436 15 #10 #5 12' 6\* 1.71 417.2 10' 16'< FD ≤ 20' 12" 20' 18' 6" 6\* #6 6" 3'-9" #4 æ #4 #10 #6 12 #8 6\* 3-9 #4 8 1.48 303.5 5372 20'< FD ≤ 24 12\* 22 22 #10 6" #6 10' #6 57 3-11 #4 8 #44 12' #10 67 #6 90 #8 6\* 3'-11 214 8 1.59 327.1 1.92 443.4 6342 1 #4 12" 22 22" #11 #6 10\* #7 5\* 8" #4 12" #10 67 #6 10\* 5' 8" 1.59 387.9 1.92 473.0 24'< FD ≤ 28' 6" 3'-11' $\sim$ #8 3'-11 214 7209 28'< FD ≤ 32' 12" 24' 24\* #11 6" #7 10\* #7 5" 4'-1" #4 8" v #4 12\* #11 6\* #7 10\* #8 5\* 4-1 #4 8 1.69 402.5 2.02 522.3 8145 121 24 24\* #11 5 #7 10\* **#8** 57 45.12 #4 8 22.6 12\* #11 67 #7 10\* #8 57 4.1 22.4 8 1.69 470.2 2.02 522.3 32'< FD ≤ 38' 9445 0' ≤ FD < 2' 10\* 16 12 #8 6" #6 12 #14 8 44.4 12' #10 107 105 57 #7 5\* 3-2 #4 8 1.04 164.2 1.37 422.3 2259 2 25 FD 5 4 10\* 14' 12 #9 6' #5 10' #4 8 #4 12' #9 6\* #6 5\* #7 5\* 3-2 #4 8 0.92 188.0 1.37 420.7 2348 2 12\* N/A 12\* 6\* 10\* 5\* 195.9 10 NVA 10' $4 \le FD \le 6$ 12" 16' 14" #9 6" #6 ±4. 8" N/A #4 #10 #7 #7 4-3 #14 8" **N/A** 1.06 1.63 449.0 2731 6'< FD ≤ 8' 12" 18' 16\* #9 6" #6 12 #4 8 #4 12\* #9 6\* #7 10\* #7 5\* 3'-10' #4 87 1.18 196.3 1.75 412.6 3165 2 12" 18 16\* #10 6" #6 12\* 244 12\* 6\* 5\* 57 8 196.3 8'< FD < 10 #4 8 #9 #6 #18 3-6 214 1.18 1.75 483.8 3576 2 10\* #6 6\* 0' ≤ FD < 2 14'#9 6" 9" #6 9" 3'-1" #4 8. #5 8 #8 #6 10' #6 5 3-1 #4 8 1.22 290.0 1.37328.2 1877 1 18 10\* 14' 12' #9 6" #5 #6 8" 4'-0" 8" #4 12' #9 6\* #6 10' #6 5" 3 - 18 1.22 272.9 1.37 356.4 2001 $2 \le FD \le 4$ 8 #4 224 12 4< FD ≤ 6 10\* 16 14" #9 6" #5 #5 6" 3'-8" #4 8 N/A #44 12' #9 67 #5 10\* #7 5\* 3-6 214 8 NIA 1.34 261.4 1.49 381.6 2349 то 6'< FD ≤ 10' 10\* 18 16\* #10 6" #6 12 #6 6" 3'-5" #4 8" #4 12" #10 6\* #6 10/ #7 57 3-5 #4 81 1.47316.1 1.61 428.4 3198 TO 15 10'< FD ≤ 14' 12" 20 18 #11 6" #5 6\* #5 6" 3'-9" #4 8 #4 12' #10 67 #6 10" #7 57 3-9 #4 1.67 360.8 1.87 444.3 3984 10 81 14 < FD < 18 12\* 22 #11 6" #5 7\* #6 7\* #4 81 #4 12' #10 67 #6 10\* #7 57 234 179 380.4 461.9 4973 22 3'-11'3-11 8 2.12 22\* #6 #44 12\* 10\* 57 18'< FD ≤ 22' 12\* 22 #11 151 10' ±6 R\* 3'-11' #4 8. #11 6\* #6 #8 3'-11' #14 8" 1.79 443.9 2.12 548.0 5841 22'< FD ≤ 30' 12" 24" 24\* #10 41 #7 10" #6 57 #4 #4 12\* #10 47 #7 10\* #8 57 4-11 224 1.92 462.7 610.4 7643 4'-1" 8. 8\* × 2.24

RIGGING LINES

MAY BE VERTICAL

### KEY NOTES

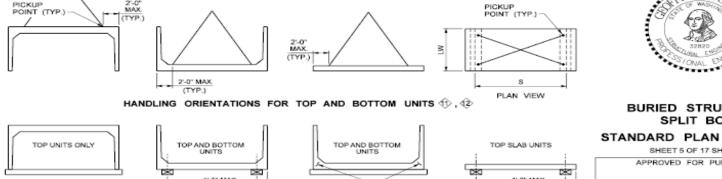
- (1) DESIGN SPAN 'S', SHALL BE TAKEN EQUAL TO THE HORIZONTAL DISTANCE BETWEEN INSIDE FACE. OF WALLS AT THE CORNER BETWEEN THE FILLET AND THE WALL AS SHOWN ON SHEET 1. FOR SEGMENTS WITH A SKEW SEE GRAPHICAL CLARIFICATION OF DESIGN SPAN ON SHEET 3. IF THE DESIGN SPAN FALLS IN BETWEEN A DESIGN SPAN VALUE IN THE TABLES, USE REINFORCEMENT FOR THE LONGER SPAN. CLASS 1 STRUCTURES WITH SPANS GREATER THAN 18 FEET AND LESS THAN 20 FEET SHALL USE GEOMETRY AND REINFORCEMENT FOR 21 FOOT SPAN CLASS 2 STRUCTURES WITH A PGA = 0.32G
- 2 THE MAXIMUM FILL DEPTH OVER THE ENTIRE BURIED STRUCTURE SHALL BE USED WHEN SELECTING DESIGN FILL DEPTH
- (3) FOR REINFORCING DETAILS SEE SHEET 4.
- A MAXIMUM REQUIRED BEARING RESISTANCE FOR STRENGTH LIMIT STATE.
- THESE STRUCTURES HAVE BEEN DESIGNED FOR A TRAVERSE DIFFERENTIAL SETTLEMENTS DISPLACEMENT EQUAL TO 2 INCHES PER 100 FEET OF STRUCTURAL SPAN (DESIGN SPAN + 1.0 FOOT)
- (6) FOR HORIZONTAL JOINT TYPE DETAILS SEE SHEET 10.

DESIGN TABLE ~ CLASS I STRUCTURES ~ SPANS 12', 15' AND 18'

- WALL TIES TE AND BE ARE REQUIRED WHEN INDICATED BY LETTER 'Y'.
- (8) MATERIAL QUANTITIES ARE FOR A TYPICAL INTERIOR SEGMENT. STEEL WEIGHT DOES NOT INCLUDE ADDITIONAL REINFORCING REQUIRED FOR APPROACH SLAB SEAT.
- (9) SINGLE BARS SPACED AT 4 INCHES MAY BE SUBSTITUTED BY TWO-BAR BUNDLES SPACED AT 8".
- (1) QUANTITIES OF BOTTOM UNIT CORRESPOND TO 'HB' = 10'-0'
- TEINFORCING OF PRECAST UNITS HAVE BEEN DESIGNED FOR HANDLING AND SHIPPING ORIENTATIONS PRESENTED ON THIS SHEET. ALTERNATE SHIPPING OR HANDLING ORIENTATIONS SHALL BE ANALYZED BY THE CONTRACTOR.
- CONCRETE COMPRESSIVE STRENGTH SHALL BE AT LEAST F'CI = 3.5 KSI FOR HANDLING AND F'C = 7.0 KSI FOR SHIPPING.

### MAX Ν (TYP.) ONIAL -----2'-0" MAX (TYP.) PLAN VIEW HANDLING ORIENTATIONS FOR TOP AND BOTTOM UNITS 12, 12 BURIED STRUCTURE SPLIT BOX STANDARD PLAN E-20.10-00 TOP UNITS ONLY TOP AND BOTTOM TOP SLAB UNITS TOP AND BOTTOM UNITS SHEET 5 OF 17 SHEETS UNITS APPROVED FOR PUBLICATION 歯 1'-6" MAX. 1561 MAX J' SHAPED UNITS STATE DESIGN ENGINEER (TYP. (TYP.) MAY BE SHIPPED Vashington State Department of Transportation ON THIS FACE SHIPPING ORIENTATIONS 10.42

# Class 1 Design Tables w/Shipping & Handling



DESIGN TABLE ~ PGA = 0.32g ~ CLASS II STRUCTURES ~ SPANS 21', 24', 27' AND 30'

	DESIGN HEIGHT MEMBER THICKNESS					TOP UNIT REINFORCEMENT												BOT	TOM UN	IT REIN	FORCE	MENT <	3>		M	ATERIAL	QUANTITI	DESIGN VALUES								
DESIGN SPAN S	TOTAL H	TOP UNIT WALL	BOT. UNIT WALL	FILL DEPTH FD	WALLS	TOP SLAB TT	BOT. SLAB TB	(51	AB RIOR)	T2 (SLAB EXTERIOR)		(CORNER)		( ovi	T4 ALL RIOR)	(TIES)		(BOT.)		(SLAB INTERIOR)		(SLAB EXTERIOR)		B3 CORNER	4)	(07)	ALL RIOR)	(TIES)			49		STR. I BEARING DEMAND (PSF)		REQ'D HORIZ JOINT TYPE	
$\langle 1 \rangle$		нт	нв	⊘				SIZE	SPA.	SIZE	SPA.	SIZE	SPA.	π.	SIZE	SPA.	Ŷ	SIZE	SPA.	SIZE	SPA.	SIZE	SPA.	SIZE	SPA.	BL.	SIZE	SPA.	1	CONC. (CY/FT)	STEEL (LBS/FT)	CONC. (CY/FT)	STEEL (LBS/FT)	٠	\$	۵
				0' ≤ FD < 2'	12*	16*	14"	#9	6*	#6	12*		N/A		,	ψA.	NA	#6	12"	#9	6*	#5	6*	#6	6*	3'-4"	#4	8*	N/A	1.21	250.9	1.76	382.2	2177	N/A	2
	10'	N/A	10'	$2^\circ \le FD \le 4^\circ$	12*	16"	14"	#9	6"	#6	12*		N/A		,	WA.	NA	#4	12"	#9	6*	#5	6*	#7	6"	4'-4"	#4	8*	N/A.	1.21	230.9	1.76	421.5	2365	N/A.	2
				$4^{\circ}$ FD $\leq 6^{\circ}$	12*	18"	16*	#10	6*	#6	12*		N/A			WA.	NA	#4	12*	#10	6*	#7	10*	#7	5*	3'-5"	#4	8"	N/A.	1.35	272.2	1.90	488.9	2777	N/A.	2
21'				0' ≤ FD < 2'	12*	14"	12*	#10	6*	#6	8"	#5	8"	3'-4"	#4	8*	N/A	<b>#6</b>	9*	#9	6*	#5	6*	#7	6*	3'-7"	#4	8"	N/A.	1.43	376.7	1.61	413.5	1762	0.16"	1A.
				$2^{\circ} \le FD \le 4^{\circ}$	12*	16*	14"	#10	6*	#6	8"	#5	8.	3*-5*	#4	8.	NA	#4	12"	#9	6*	#5	6*	#7	6*	3'-7"	#4	8*	N/A.	1.57	347.4	1.76	415.4	2015	0.18"	1A.
	12' TO 15'	67	7 TO 10	4'≤ FD ≤ 8'	12*	18"	16"	#11	6"	#5	7"	#5	7*	3.7*	#4	8*	NA	#4	12"	#10	6*	#7	10*	#7	5"	3'-7"	#4	8"	N/A.	1.71	388.5	1.90	490.6	2767	0.21"	1
				8'< FD ≤ 12"	12*	20"	20"	#11	6"	#5	6"	#5	6"	38.	#4	8"	NA	#4	12"	#11	6*	#6	6"	#8	6"	3'-9"	#4	8"	N/A.	1.86	403.0	2.18	566.2	3660	0.25"	1
				12 × FD ≤ 16"	12*	22"	22"	#11	57	#6	10*	#6	5"	354117	#4	8*	NA	#4	9"	#11	6*	#6	101	#8	5"	4'-0"	#4	8*	N/A.	2.00	492.9	2.32	624.2	4455	0.28"	1
	17 TO 20	7' TO 10'	10'	0′ ≤ FD ≤ 2″	12*	14"	14"	#9	6*	#6	5*	#8	5*	5'-0"	#4	8*	NA	#6	12"	#9	6*	#6	5*	#8	5"	4'-9"	#4	8*	N/A.	1.76	553.5	1.76	530.3	1830	0.27"	1
				$0' \leq FD \leq 2'$	12*	18"	16*	#9	6*	#6	12*		N/A		,	WA.	NA	<b>#</b> 6	12*	#9	6*	#5	6*	#7	6*	3'-5"	#4	8*	N/A.	1.52	282.7	2.05	446.5	2137	N/A.	2
	10'	N/A	10'	$2^{\circ} \leq FD \leq 4^{\circ}$	12*	18"	16*	#10	6*	#6	12*		N/A		,	WA.	NA	#4	12"	#10	6*	#5	6*	#7	6*	3'-5"	#4	8*	N/A.	1.52	306.5	2.05	492.9	2350	N/A.	2
				4'≤ FD ≤ 6'	12*	18"	18"	#11	6*	#6	12*		N/A		,	WA.	NA	#4	12"	#10	6*	#7	10*	#7	5*	3'-7"	#4	8*	N/A.	1.52	358.4	2.21	528.2	2733	N/A.	2
				$0' \leq FD \leq 2'$	12*	18"	16*	#10	6"	#6	8"	#5	8"	3.7*	#4	8*	NA	#6	10"	#8	6*	#7	10*	#6	5"	3.7*	#4	8"	N/A.	1.88	415.5	2.05	405.6	1773	0.17"	1
24'				$2^{\circ} \leq FD \leq 4^{\circ}$	12*	18"	16*	#10	6"	#6	8"	#5	8"	3"-7"	#4	8"	NA	24	12*	#9	6*	#7	101	#7	5"	3'-7"	#4	8"	N/A.	1.88	385.5	2.05	481.4	1984	0.18"	1
	12' TO 15'	57	7" TO 10"	4'< FD ≤ 8'	12*	20"	18"	#11	6*	#6	8"	#6	8"	38.	#4	8*	NA	#4	12"	#10	6*	#5	6*	#8	6*	3'-10"	#4	8*	N/A.	2.04	452.8	2.21	536.1	2776	0.22"	1
				8'< FD ≤ 10°	12*	22"	22"	#11	6*	#6	8"	#6	8.	3'-11"	#4	8*	NA	#4	9"	#11	6*	#7	10*	87	5*	3'-11"	#4	8*	N/A.	2.20	470.8	2.53	637.9	3260	0.24"	1
				10'< FD ≤ 14"	12*	24"	24"	#10<	9> 4°	#6	7*	#6	7*	4'-1"	#4	8*	NA	24	9"	#10<	9> 4°	#7	101	#7	5*	4'-1"	#4	8*	N/A.	2.36	546.5	2.69	747.5	4150	0.27"	1
	17' TO 20'	7' TO 10'	10'	0' ≤ FD < 2'	12*	16"	16*	99	6*	#6	5*	#8	5*	3'-10"	#4	8*	NA	<b>P</b> 6	12"	#9	6*	#6	5*	#8	5*	3'-11"	#4	8*	N/A.	2.05	578.9	2.05	557.4	1817	0.25"	1
				$2^{\circ} \le FD \le 4^{\circ}$	12*	16*	16*	#10	6*	#6	5*	#8	5*	4'-3"	#4	8*	NA	#4	12"	#10	6*	#6	5*	#8	5*	4'-3"	#4	8*	N/A.	2.05	608.0	2.05	608.0	2028	0.29"	1
				0' ≤ FD < 2'	12*	18"	16"	#10	6"	#6	12"		N/A			WA.	NA	#6	10"	#10	6*	#6	6.	#6	6"	3.6.	#4	8"	N/A.	1.68	374.9	2.19	525.6	2107	N/A.	2
	10'	N/A	10'	$2^{\circ} \le FD \le 4^{\circ}$	12*	16"	18"	#11	6*	#6	12*		N/A		1	WA.	NA	#4	12"	#10	6*	#6	6*	#7	6*	3'-9"	#4	8*	N/A.	1.68	398.8	2.37	558.5	2401	N/A.	2
				$4 \le FD \le 6$	12*	22"	20"	#11	67	#6	10*		N/A		1	WA.	NA	#4	9"	#11	67	#7	6.	#8	6.	2.8.	#4	8.	N/A.	2.04	420.1	2.55	688.8	2855	N/A.	2
				$0' \leq FD \leq 2'$	12*	18"	16"	#10	6"	#7	8"	#5	8"	3.7*	#4	8*	NA	#6	10"	#9	6*	#8	10*	#7	5"	3.7	#4	8"	N/A.	2.05	479.4	2.19	534.7	1679	0.17"	1
27	12' TO 15'	5	7 TO 10	2' ≤ FD ≤ 4'	12*	20"	18"	#11	6"	#7	8"	#6	8"	3-9"	#4	8"	NA	#4	12*	#10	6*	#8	10*	#7	5"	3.9.	#4	8"	N/A.	2.23	518.7	2.37	590.2	1974	0.19"	1
				4'< FD ≤ 6'	12*	22"	20*	#11	6*	#7	8*	#6	8.	3%11*	#4	8*	N/A	#4	9"	#10	6*	#8	10*	87	5*	3-11*	#4	8*	N/A	2.40	538.0	2.55	594.0	2394	0.21"	1
				6 × FD ≤ 10°	12*	24"	24"	<u> </u>	9> 4"	#7	9*	#6	9"	4'-1"	#4	8*	NA	#4	9"	#11	5*	#8	10*	87	5*	4'-1"	#4	8*	N/A	2.58	590.3	2.91	770.4	3266	0.24"	1
	17' TO 20'	7' TO 10'	10'	0' ≤ FD < 2'	12*	18"	18*	#10	7*	#8	10*	#8	5"	3'-8"	#4	8"	NA	#6	12*	#9	6*	#8	10*	#8	5*	3'-10"	#4	8"	N/A.	2.37	622.1	2.37	582.7	1782	0.28"	1
				$2^{\prime}$ FD $\leq 4^{\prime}$	12*	18"	18"	#10	6*	#8	10*	#8	5*	4'-0"	#4	8*	N/A	#4	12"	#10	6*	#8	10*	#8	5*	4'-0"	#4	8"	N/A	2.37	636.6	2.37	636.6	2009	0.3*	1
				0' ≤ FD < 2'	12*	20"	18"	#10	6"	#6	11*		N/A			4/A.	N/A	#6	10"	#11	6*	#6	5*	#8	6*	3.6.	#4	8"	N/A.	2.05	416.4	2.64	751.6	2101	N/A.	2
	10'	N/A	10'	$2' \le FD \le 4'$	12*	20"	18"	#11	6"	#6	11*		N/A			NA.	NA	#4	12"	#11	6*	#7	÷.	27	6"	3.6.	#4	8"	N/A.	2.05	443.8	2.54	696.9	2322	N/A.	2
				4'< FD ≤ 6'	12*	22"	20*	#11	5*	#6	10*		N/A			UA.	NA	#4	9*	#11	5*	#7	6*	#8	6*	4'-0"	#4	8"	N/A.	2.25	531.8	2.74	806.9	2737	N/A	2
				0' ≤ FD < 2'	12*	20"	18*	#11	6*	#7	7*	#5	7*	38.	#4	8*	NA	#6	9*	#10	6*	#6	5*	87	5*	3-9*	#4	8*	N/A.	2.41	610.8	2.54	642.3	1713	0.15"	1
30'	12' TO 15'	67	7 TO 10	$2^{\circ} \le FD \le 4^{\circ}$	12*	22"	20*	#11	6*	#7	7*	#5	7*	35111	#4	8.	NA	#4	9*	#10	6*	#6	5*	#7	6*	3-11*	#4	8"	N/A.	2.61	588.7	2.74	646.1	1999	0.19"	1
				4'< FD ≤ 6'	12*	24"	22*	#11	5*	#7	7*	#6	7*	4'-1"	#4	8*	NA	24	9*	#11	6*	#6	5*	#8	5*	4'-1"	#4	8*	N/A.	2.81	674.5	2.93	817.7	2414	0.21"	1
				6'< FD ≤ 8'	12*	24"	24"	#10<	<u>9&gt; 4"</u>	#7	7*	#6	7*	4'-1"	#4	8*	NA	#4	9*	#11	5*	#6	5*	#8	5*	4'-1"	#4	8*	N/A	2.81	679.5	3.13	885.4	2821	0.23"	1
	17' TO 20'	7' TO 10'	10'	0' ≤ FD < 2'	12*	18"	18"	#10	6"	#6	6"	#8	6"	4'-2"	#4	8.	NA	#6	10"	#10	6*	#6	D**	#8	5"	3.6.	#4	8"	N/A.	2.64	675.6	2.54	685.5	1743	0.26"	1
				$2^\circ \le FD \le 4^\circ$	12*	20"	20"	#11	6"	粨	67	#8	5"	3'-9"	#4	8"	NA	#4	12"	#11	6*	#6	5*	#8	5"	31-91	#4	8"	N/A.	2.74	752.1	2.74	752.1	2028	0.3*	1

### KEY NOTES

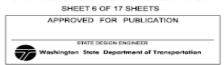
- OESIGN SPAN 'S', SHALL BE TAKEN EQUAL TO THE HORIZONTAL DISTANCE BETWEEN INSIDE FACE OF WALLS AT THE CORNER BETWEEN THE FILLET AND THE WALL AS SHOWN ON SHEET 1. FOR SEGMENTS WITH A SKEW SEE GRAPHICAL CLARIFICATION OF DESIGN SPAN ON SHEET 3. IF THE DESIGN SPAN FALLS INBETWEEN A DESIGN SPAN VALUE IN THE TABLES, USE REINFORCEMENT FOR THE LONGER SPAN.
- 2 THE MAXIMUM FILL DEPTH OVER THE ENTIRE BURIED STRUCTURE SHALL BE USED WHEN SELECTING DESIGN FILL DEPTH.

(3) FOR REINFORCING DETAILS SEE SHEET 4.

- (4) MAXIMUM REQUIRED BEARING RESISTANCE FOR STRENGTH LIMIT STATE.
- THE STRUCTURE HAS BEEN DESIGNED FOR THE RACKING DISPLACEMENTS PRESENTED HERE. THESE DESIGN VALUES ARE DETERMINED BASED ON THE DESIGN CRITERIAAS OUTLINED IN THE BDM. THESE STRUCTURES HAVE BEEN DESIGNED FOR A TRAVERSE DIFFERENTIAL SETTLEMENT DISPLACEMENT EQUAL TO 2 INCHES PER 100 FEET OF STRUCTURAL SPAN (DESIGN SPAN + 1.0 FOOT).
- (6) FOR HORIZONTAL JOINT TYPE DETAILS SEE SHEET 10.
- WALL TIES TE AND BE ARE REQUIRED WHEN INDICATED BY LETTER 'Y'.
- MATERIAL QUANTITIES ARE FOR TYPICAL INTERIOR SEGMENT. STEEL WEIGHT DOES NOT INCLUDE ADDITIONAL REINFORCING REQUIRED FOR APPROACH SLAB SEAT.
- SINGLE BARS SPACED AT 4 INCHES MAY BE SUBSTITUTED BY TWO-BAR BUNDLES SPACED AT 8".
- QUANTITIES OF BOTTOM UNIT CORRESPOND TO 'HB' = 10'-0".
- SEE SHEET 5 FOR HANDLING AND SHIPPING ORIENTATIONS.



### BURIED STRUCTURE SPLIT BOX STANDARD PLAN E-20.10-00



Class 2 (0.32g) Design Tables

DESIGN TABLE ~ PGA = 0.64g ~ CLASS II STRUCTURES ~ SPANS 21', 24', 27' AND 30'

	DESIGN HEIGHT MEMBER THICKNESS				KNESS	TOP UNIT REINFORCEMENT 3												BOT	TOM UN	IT REIN	FORCE	MENT <	3		MATERIAL QUANTITIES				DESIGN VALUES							
DESIGN SPAN S	TOTAL H	TOP UNIT WALL	BOT. UNIT WALL	FILL DEPTH FD	WALLS TW	TOP SLAB TT	BOT. SLAB TB	(SLA INTER)	B		AB RIOR)		T3 (CORNE		(w)	T4 ALL RIOR)	(TIES)		т7 от.)	(5	B1 LAB RIOR)	(9	B2 ILAB ERIOR)		B3 CORNER	<b>R</b> )	(W	B4 ALL RIOR)	(TIES)		UNIT			STR. I BEARING DEMAND (PSF)	RACKING DISPL.	REQ'D HORIZ JOINT TYPE
<⇒		нт	HB	⊘		···		SIZE :	IPA.	SIZE	SPA.	SIZE	SPA.	n.	SIZE	SPA.	$\Rightarrow$	SIZE	SPA.	SIZE	SPA	. SIZE	SPA.	SIZE	SPA.	BL.	SIZE	SPA.	$\Rightarrow$	CONC. (CY/FT)	STEEL (LBS/FT)	CONC. (CY/FT)	STEEL (LBS/FT)	4	\$	6>
				0' ≤ FD < 2'	12"	16*	14"	#9	6"	#6	12"		N/A.		1	₩A.	N/A.	#6	12"	#9	6"	#6	6"	#7	6"	4'-8"	#4	8"	N/A	1.21	250.9	1.76	445.0	2177	N/A	2
	10	NA	10'	$2' \le FD \le 4'$	12"	16*	14"	#9	6*	#6	12"		N/A		,	WA.	NA	#4	12"	#9	6*	#6	5"	#7	5"	3'-4"	#1	8"	N/A	1.21	230.9	1.76	471.2	2365	N/A	2
				4'< FD ≤ 6'	12"	18"	16"	#10	6"	<b>#</b> 6	12"		N/A.		,	e/A.	N/A.	#4	12"	#10	6"	87	10*	#7	51	3'-5"	#4	8"	N/A	1.35	272.2	1.90	488.9	2777	N/A	2
21'				0' ≤ FD < 2'	12"	14"	12"	#10	6*	#6	8"	#5	8"	3'-4"	#4	8"	NA	#6	9"	#9	6*	#5	6"	#7	6*	3'-7"	#1	8"	N/A	1.43	376.7	1.61	413.5	1762	0.5'	1A
				$2^{\circ} \leq FD \leq 4^{\circ}$	12"	16"	14"	#10	6"	#6	8"	#5	8"	3'-5"	#4	8"	NA	#4	12"	#9	6"	#5	6"	#7	67	3'-7"	#4	8"	N/A	1.57	347.4	1.76	415.4	2015	0.56*	1A.
	12 TO 15'	5	7' TO 10'	4'< FD ≤ 8'	12"	18"	16"	#11	6*	#5	7"	#5	7*	3'-7"	24	8"	NA	#4	12"	#10	6*	#7	10*	#7	5"	3'-7"	#1	8"	N/A	1.71	388.5	1.90	490.6	2767	*30.0	1
				$8^{\prime}\!\!<\!FD\leq 12^{\prime}$	12"	20"	20"	#11	6"	#5	6"	#5	6"	3'-9"	#5	9"	Y	#4	12"	#11	6"	#6	6"	#8	6"	3'-9"	#5	9*	Y	1.96	425.9	2.18	593.0	3660	0.77*	1
				$12^{\circ}$ FD $\leq 16^{\circ}$	12"	22"	22"	W11	5"	#6	10"	<i>0</i> 6	5"	3-11"	#5	8"	Y	#4	9"	W11	6"	#6	10"	#8	51	4'-0"	N5	8"	Y	2.00	520.4	2.32	658.6	4455	0.85*	1
	17' TO 20'	7" TO 10'	10'	$0' \leq FD \leq 2'$	12"	14"	14"	#9	6"	#6	67	#8	67	57-07	#4	8"	NA	#6	12"	#9	6*	#6	57	#8	67	4'-9"	#1	8"	N/A	1.76	553.5	1.76	530.3	1830	0.84"	1
				$0' \leq FD \leq 2'$	12*	18"	16"	#9	6"	#6	12"		N/A.		1	₩A.	N/A.	#6	12"	49	6"	#7	10"	#7	6"	3'-9"	#4	8"	N/A	1.52	282.7	2.05	458.6	2137	N/A	2
	10'	NA	10'	$2^{\circ} \leq FD \leq 4^{\circ}$	12"	18"	16"	#10	6"	#6	12"		N/A		1	A.	N/A	#4	12"	#10	6*	#7	10"	#7	67	3'-5"	#1	8"	N/A	1.52	306.5	2.05	525.1	2350	N/A	2
				4'< FD ≤ 6'	12"	18"	18"	#11	6"	<b>#</b> 6	12"		N/A.		•	₩A.	N/A.	44	12"	#10	6"	87	10"	87	51	3'-7"	#4	8"	N/A	1.52	358.4	2.21	528.2	2733	N/A	2
				$0' \leq FD < 2'$	12"	18"	16"	#10	6*	#6	8"	#5	8"	3'-7"	24	8"	NA	#6	10"	#8	6*	#7	10*	#6	5"	3'-7"	#1	8"	N/A	1.88	415.5	2.05	405.6	1773	0.51*	1A
24'				$2^{\circ} \le FD \le 4^{\circ}$	12"	18"	16"	#10	6"	#6	8"	#5	8"	3'-7"	#4	8"	N/A.	#4	12"	49	6"	#7	10*	#7	5*	3'-7"	#4	8"	N/A	1.88	385.5	2.05	481.4	1984	0.57*	1A.
	12 TO 15	5	7' TO 10'	4'< FD ≤ 8'	12"	20*	18"	#11	6"	#6	8"	#6	8"	3-9"	#4	8"	NA	#4	12"	#10	6"	#5	6"	#8	6*	3"-10"	#1	8"	N/A	2.04	452.8	2.21	536.1	2776	0.66*	1
				8'< FD ≤ 10'	12"	22*	22"	#11	6"	#6	8"	#6	8"	3'-11"	#5	9"	Y	#4	9"	#11	6"	#7	10"	#7	5"	3-11*	#5	9*	Y	2.20	493.9	2.53	666.2	3260	0.73*	1
				10'< FD ≤ 14'	12"	24"	24"	#10.9	4*	#6	7*	#7	7*	4'-1"	#5	8"	N/A	#4	9*	#10<	<u>9&gt; 4"</u>	#7	10*	#8	5*	4'-1"	#5	8"	N/A	2.36	580.9	2.69	767.5	4150	0.84*	1
	17' TO 20'	7" TO 10'	10'	$0' \leq FD \leq 2'$	12"	16"	16"	#9	6"	#6	57	#8	57	3'-10"	#4	8"	NA	#6	12"	#9	6*	#6	57	#8	57	3'-11"	#1	8"	N/A	2.05	578.9	2.05	557.4	1817	0.75*	1
				2' ≤ FD ≤ 4'	12"	16*	16"	#10	6*	#6	5"	#8	5"	4'-3"	#4	8"	NA	#4	12"	#10	6*	#8	8"	#8<	9>4"	3'-7"	#1	8"	N/A	2.05	608.0	2.05	656.5	2028	0.92*	1
				$0' \leq FD \leq 2'$	12"	18"	16"	#10	6"	#6	12"		N/A.		,	A/A	NA	#6	10"	#10	6*	#6	6"	#7	6"	3'-9"	#1	8"	N/A	1.68	374.9	2.19	558.0	2107	NVA	2
	10"	NA	10'	2' ≤ FD ≤ 4'	12"	18"	18"	#11	6"	#6	12"		N/A.			4/A	N/A	#4	12"	#10	6*	#6	5*	#7	5*	3.9.	#	8"	N/A	1.68	391.9	2.37	600.1	2401	NVA	2
				4' < FD ≤ 0'	12"	22*	20*	#11	67	46	10**		NVA.			WA .	N/A	#4	9*	#11	67	67	67	40	67	31-91	#4	0*	N/A	2.04	400.1	2.55	660.0	2055	NVA	2
				0' ≤ FD < 2'	12"	18"	16"	#10	6"	67	8"	#5	8"	3'-7"	84	8"	N/A	#6	10"	#9	6"	#8	10"	07	5"	3'-7"	#4	8"	N/A	2.05	479.4	2.19	534.7	1679	0.52*	1A
27'	12 TO 15	57	7 TO 10	$2' \leq FD \leq 4'$	12"	20*	18"	#11	6"	#7	8"	#6	8"	3'-9"	#4	8"	N/A	#4	12"	#10	6"	#8	10"	#7	67	3'-9"	#1	8"	N/A	2.23	518.7	2.37	590.2	1974	0.58*	1A.
				4'< FD ≤ 6'	12"	22*	20"	#11	6*	67	8"	#6	8"	3-11"	84	8"	N/A	84	9*	W10	6°	#8	10*	07	5° 5°	3-11*	#1	8"	N/A	2.40	538.0	2.55	594.0	2394	0.64*	1
	478 700 000	7 70 401	401	6'< FD ≤ 10'	12"	24*	24"	#10.9	4"	#7	9"	#6	9"	4'-1"	#4		NA	#4	9*	#11		#8	10*	#8	-	4'-1"	#1	· ·	N/A	2.58	594.0	2.91	822.9	3266	0.75*	
	17 TO 20'	F 10 10	10'	0' ≤ FD < 2'	12"	18"	18"	#10		#8	10"	#8	5"	3'-8"	84	8° 8°	N/A	#6	12"	#9	6*	#8	10*	#8	5° 5°	3"-10"	#4	8"	N/A	2.37	622.1	2.37	582.7	1782	0.87*	1
				2< FD ≤ 4	12"	18*	18"	#10	6°	#5	10"	#8	5*	4'-0"	#4	-	N/A	#4	12"	#10	6*	#8	10*	#5	-	4'-0"	#1	-	N/A	2.37	636.6	2.37	636.6	2009	0.94*	
				0' ≤ FD < 2'	12"	20*	18"	#10	6"	#6	11"		N/A			₩A.	N/A	#6	10"	W11	6"	87	5	#8	5° 5°	3'-9"	#1	8° 8°	N/A	2.05	416.4	2.54	751.6	2101	N/A	2
	10'	NA	10'	2' ≤ FD ≤ 4'	12"	20*	18"	#11	-	#6	11"		N/A			₩A.	NA	#4	12"	#11	6*	#6	5		-	3'-9"	#1	-	N/A	2.05	443.8	2.54	706.3	2322	N/A	2
				4'< FD ≤ 6'	12"	22*	20"	#11	5°	#5	10"	45	N/A	20.05	-	WA.	NA	#4	9"	#11	57	#5	5	#8	57	4'-0"	#1	8"	N/A	2.25	518.5	2.74	824.7	2737	N/A	2
~~~	478 700 477		7 TO 10	0' ≤ FD < 2'	12"	20*	18"	#11	67	#7	<i>r</i>	#5	7	3'-9"	#4	8" 8"	N/A	201	9°	#10	6*	#6	57	#7	5"	3'-9"	#1	8" 8"	N/A	2.41	610.8	2.54	642.3	1713	0.48*	1A
30'	12 TO 15	5	7 10 10	2'≤ FD ≤ 4'	12"	22"	20"	#11	57	#7	7	#5	7	3-11"	#4		N/A	#4	9"	#10	6"	#5	57	27	57	3-11"	#		N/A	2.61	588.7	2.74	646.1	1999	0.55*	
				4'< FD ≤ 6'	12"	24"	22"	#11	~	#7	<i>r</i>	#6	T	4-1*	#4	8" 8"	N/A	#4	9.	#11	6° 57	#6	57		57	4'-1"		8" 8"	N/A	2.81	667.9	2.93	817.7	2414	0.65*	
	17 TO 20'	7 70 10	10'	6'< FD ≤ 8' 0' ≤ FD < 2'	12"	18"	18"	#10(9)	6*		6"	#6	6"	4-1*	#4	8"	N/A N/A	#4	10"	#11	6"	#6	5	#8	5	3'-9"	#	8"	N/A	2.81	679.5	3.13	685.5	2821	0.71	+
	17 10 20	1.10.10	10			20"	20"	#10	6"	#6	57	#8	57	3-9	#4	8"	N/A	#6	10"	#10	6"	#6	5	#8	-	3'-9"	#1	8"	N/A N/A	2.54	752.1	2.54	752.1	2028	0.8	
				$2' \le FD \le 4'$	12"	20	20	#11	0	+6	5	+#8	5	3-8	- 44	8	N/A	44 4	12	#11	6	90	5.	#8	5	3-9	- #4	8	re/A	2.74	7:52.1	2.14	732.1	2028	0.90	

### KEY NOTES

- (1) DESIGN SPAN 'S', SHALL BE TAKEN EQUAL TO THE HORIZONTAL DISTANCE BETWEEN INSIDE FACE OF WALLS AT THE CORNER BETWEEN THE FILLET AND THE WALL AS SHOWN ON SHEET 1. FOR SEGMENTS WITH A SKEW SEE GRAPHICAL CLARIFICATION OF DESIGN SPAN ON SHEET 3. IF THE DESIGN SPAN FALLS INBETWEEN A DESIGN SPAN VALUE IN THE TABLES, USE REINFORCEMENT FOR THE LONGER SPAN.
- 2 THE MAXIMUM FILL DEPTH OVER THE ENTIRE BURIED STRUCTURE SHALL BE USED WHEN SELECTING DESIGN FILL DEPTH.
- (3) FOR REINFORCING DETAILS SEE SHEET 4.
- MAXIMUM REQUIRED BEARING RESISTANCE FOR STRENGTH LIMIT STATE.
- (b) THE STRUCTURE HAS BEEN DESIGNED FOR THE RACKING DISPLACEMENTS PRESENTED HERE. THESE DESIGN VALUES ARE DETERMINED BASED ON THE DESIGN CRITERIAAS OUTLINED IN THE BDM. THESE STRUCTURES HAVE BEEN DESIGNED FOR A TRAVERSE DIFFERENTIAL SETTLEMENT DISPLACEMENT EQUAL TO 2 INCHES PER 100 FEET OF STRUCTURAL SPAN (DESIGN SPAN + 1.0 FOOT).
- FOR HORIZONTAL JOINT TYPE DETAILS SEE SHEET 10.
- WALL TIES TE AND BE ARE REQUIRED WHEN INDICATED BY LETTER 'Y'.
- (8) MATERIAL QUANTITIES ARE FOR TYPICAL INTERIOR SEGMENT. STEEL WEIGHT DOES NOT INCLUDE ADDITIONAL REINFORCING REQUIRED FOR APPROACH SLAB SEAT.
- SINGLE BARS SPACED AT 4 INCHES MAY BE SUBSTITUTED BY TWO-BAR BUNDLES SPACED AT 8".
- QUANTITIES OF BOTTOM UNIT CORRESPOND TO 'HB' = 10'-0".
- ♦ SEE SHEET 5 FOR HANDLING AND SHIPPING ORIENTATIONS.



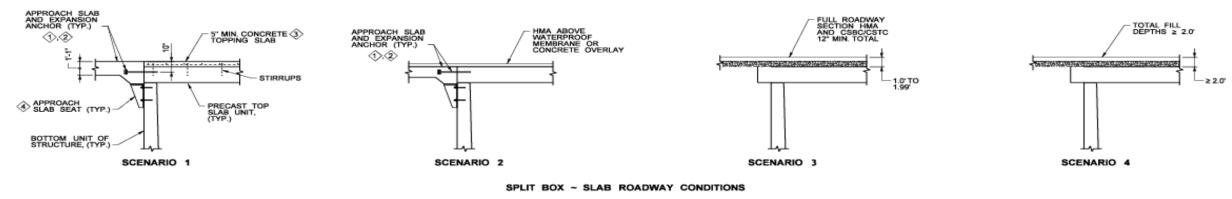
BURIED STRUCTURE SPLIT BOX

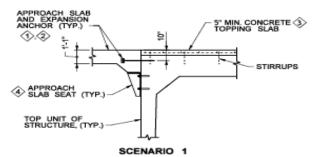
### STANDARD PLAN E-20.10-00

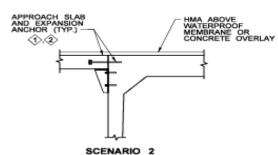


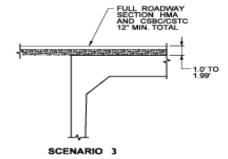
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Washington State Department of Transportation

### Class 2 (0.64g) Design Tables









PROVIDE APPROACH SLAB WHEN REQUIRED IN THE CONTRACT

③ SEE SHEET 11 FOR 5" MIN. CONCRETE TOPPING SLAB DETAILS.

5 SEE SHEET 9 FOR TYPES AND DETAILS OF TOP SLAB

APPROACH SLAB AND EXPANSION ANCHOR SHALL BE PER STANDARD PLAN A-40.50 AND PER ADDITIONAL DETAILS ON SHEET

FOR APPROACH SLAB SEAT DETAILS SEE SHEETS 13, 14, 15, AND 17.

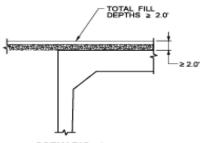
KEY NOTES

13.

⊘

DOCUMENTS.

LONGITUDINAL JOINTS.



SCENARIO 4



BURIED STRUCTURE SPLIT BOX

### STANDARD PLAN E-20.10-00

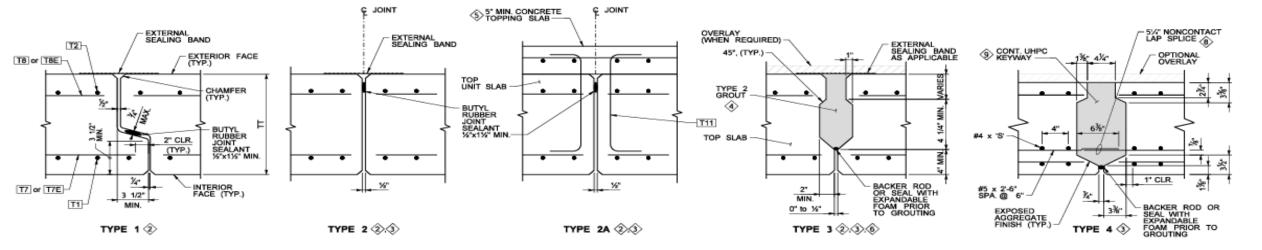
SHEET 8 OF 17 SHEETS APPROVED FOR PUBLICATION STATE DESIGN ENGINEER Washington State Department of Transportation

Roadway Scenario's	, Shear	Transfer,	and Top	Joint	Criteria
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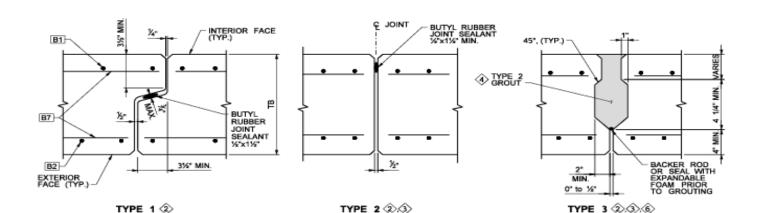
SPLIT BOX ROADWAY CONDITIONS

	DESIGN OPTIONS	
	APPROACH SLAB SEAT	
CONCR	ETE:	
	C.I.P.	SHEET 15
	C.I.P. END DIAPHRAGM	SHEET 17
STEEL:		
	W/O RESTRAINER	SHEET 13
	W/RESTRAINER	SHEET 14
	SEISMIC RESTRAINERS	
LONGIT	UDINAL:(REQ'D FOR SPLITE	BOX-SLABS)
	EXTENDED SEAT WIDTH	SHEET 10
	OR PROVIDE AN:	
	APPROACH SLAB	SHEET 13-15
TRANSV	ERSE:	
	STEEL APPR. SEAT	SHEET 14
	ACCEL. BRIDGE CONST.	SHEET 16
	C.I.P. END DIAPHRAGM	SHEET 17

	TOP U	NIT LONGITUDIN	AL JOINT SE	LECTION	CRITERIA 📀				
-1	ROADWAY CONDITION	SCENARIO 1	SCENA	RIO 2	SCENARIO 3	SCENARIO 4			
	SCENARIO DESCRIPTION	5" MIN CONCRETE TOPPING SLAB	HMA OR CO OVER		12" MIN. FULL ROADWAY SECTION (HMA & CSBC)	ROADWAY SECTION AND/OR BACKFILL			
- 1	FILL DEPTH 'FD'	TOPPING SLAB	OVER	LAY	1" TO 1.99'	≥ 2.0′			
	VERTICAL SHEAR TRANSFER ACROSS JOINTS OF ADJACENT SEGMENTS	NOT REQUIRED	REQU	RED	NOT REQUIRED	NOT REQUIRED			
- 1	ACCEPTABLE JOINT TYPE	TYPE 2A	TYPES	3&4	TYPES 1 & 3	TYPES 1, 2 & 3			
	EPOXY COATED REINF. REQUIRED IN TOP SLAB	NO	YE	s	YES	Ю			
15	CLEAR COVER TO TOP MAT OF REINF.	2"	HMA 2.5"	CONC. 2*	2"	2*			
	LONG. CONNECTION AT TOP SLAB BETWEEN FIRST THREE SEGMENTS AT EACH END	NOT REQUIRED	WELD (SEE SHE		LONGITUDINAL TIE PLATES (SEE SHEETS 2 AND 12)				



ELEVATION TOP SLAB LONGITUDINAL JOINTS ALTERNATIVES



ELEVATION BOTTOM SLAB LONGITUDINAL JOINTS ALTERNATIVES 🕅

### KEY NOTES

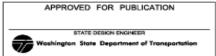
- SEE SHEET 8 FOR JOINT TYPE SELECTION CRITERIA
- THIS JOINT CAN BE USED IN COMBINATION WITH WELD TIES. SEE SHEET 12 FOR DETAILS.
- SEE JOINT TYPE 1 FOR TYPICAL REINFORCING AND DETAILS NOT SHOWN.
- GROUT SHALL CONFORM TO STANDARD SPEC. 9.20.3(2) AND SHALL ACHIEVE A MINIMUM COMPRESSIVE STRENGTH OF 2,500 PSI BEFORE BACKFILL PLACEMENT
- SEE SHEET 11 FOR 5" MIN. CONCRETE TOPPING SLAB DETAILS.
- MANUFACTURER VARIATIONS OR NOMINAL ADJUSTMENTS TO THE DETAILED JOINT GEOMETRICS SHALL BE SHOWN IN THE FABRICATION SHOP DRAWINGS.
- BOTTOM SLAB LONGITUDINAL JOINT TYPE 1, TYPE 2 OR TYPE 3 ARE PERMISSIBLE. THE SAME JOINT TYPE SHALL BE USED FOR BOTH TOP AND BOTTOM UNITS FOR EACH STRUCTURE EXCEPT TYPE 4 IS ONLY REQUIRED FOR TOP JOINT. JOINT TYPE SHALL NOT BE INTERCHANGED WITHIN THE STRUCTURE.
- STAGGER EXTENDED #5 BAR BETWEEN TOP UNIT SLABS TO PROVIDE 3" CENTER-TO-CENTER SPACING.
- REFER TO SPECIAL PROVISIONS FOR UHPC REQUIREMENTS.



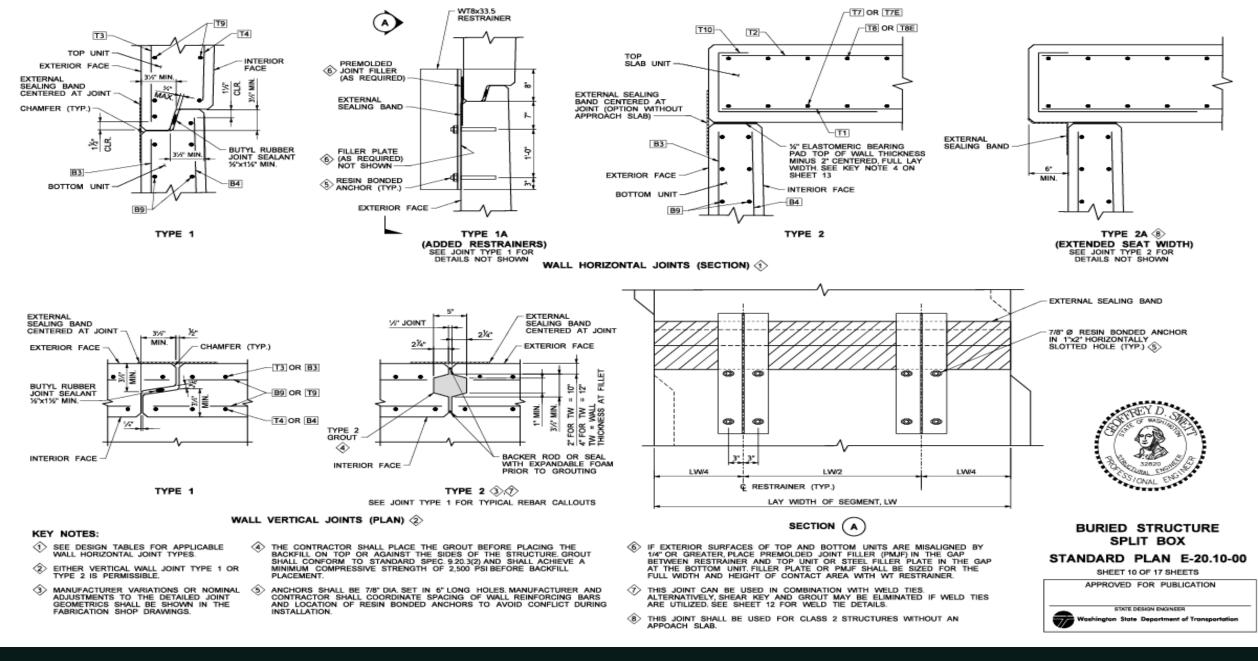
### BURIED STRUCTURE SPLIT BOX

### STANDARD PLAN E-20.10-00

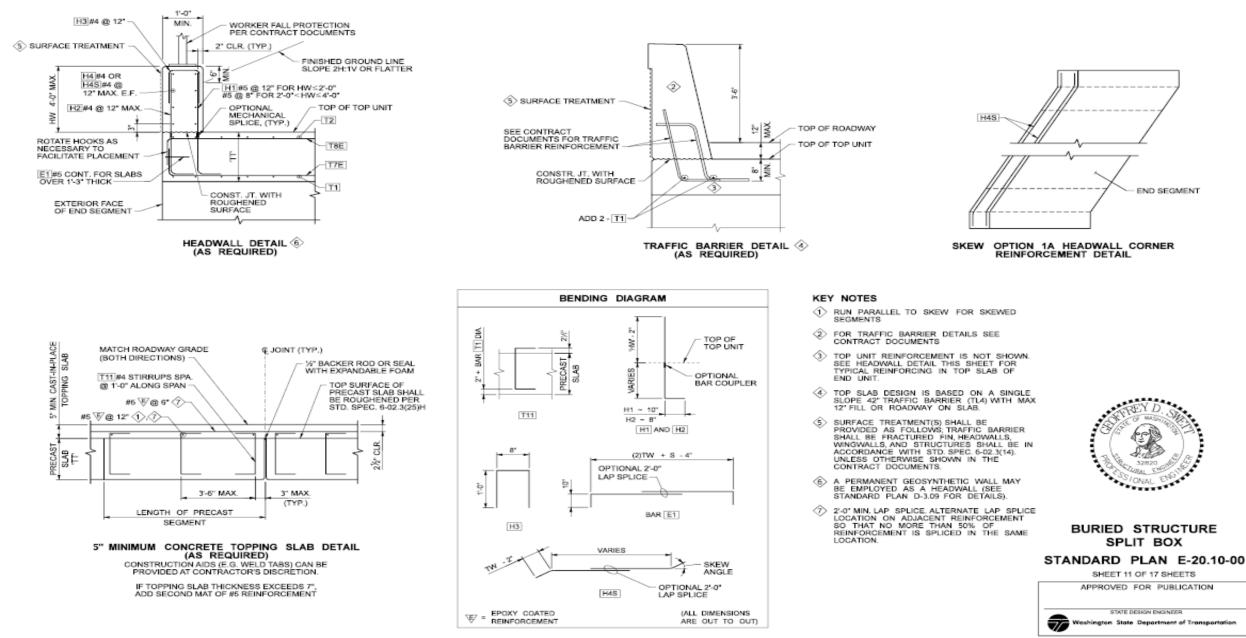
SHEET 9 OF 17 SHEETS



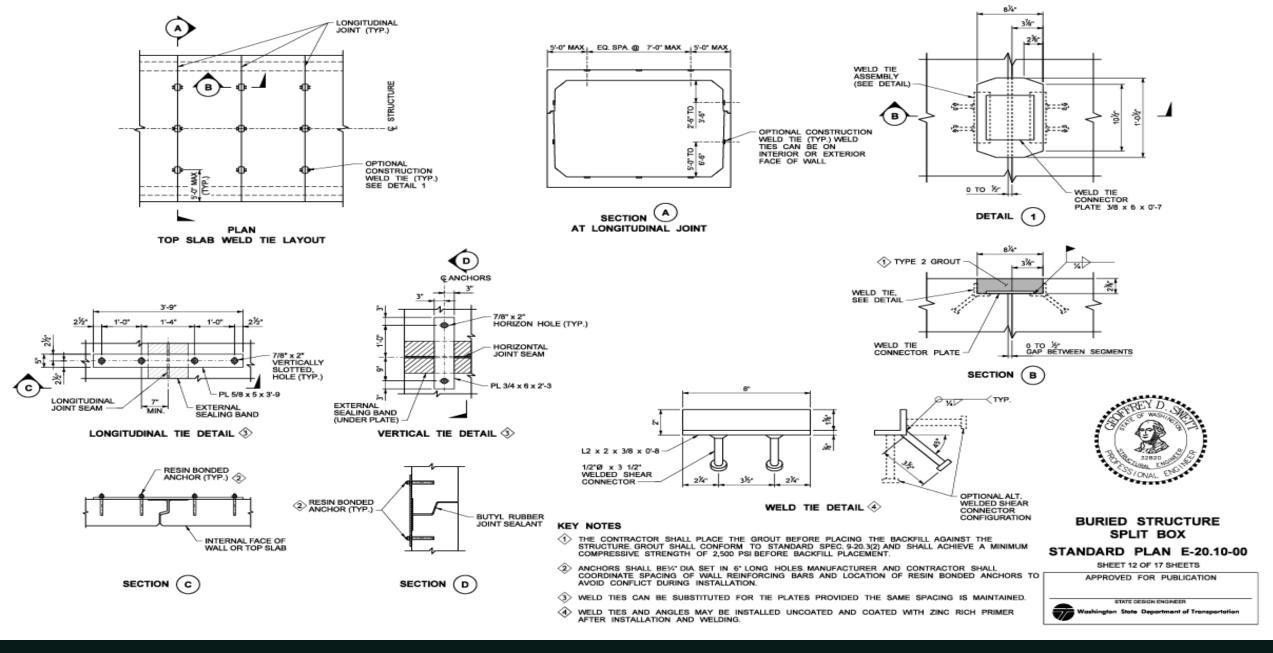
# Top & Bottom Slab Longitudinal Joint Types



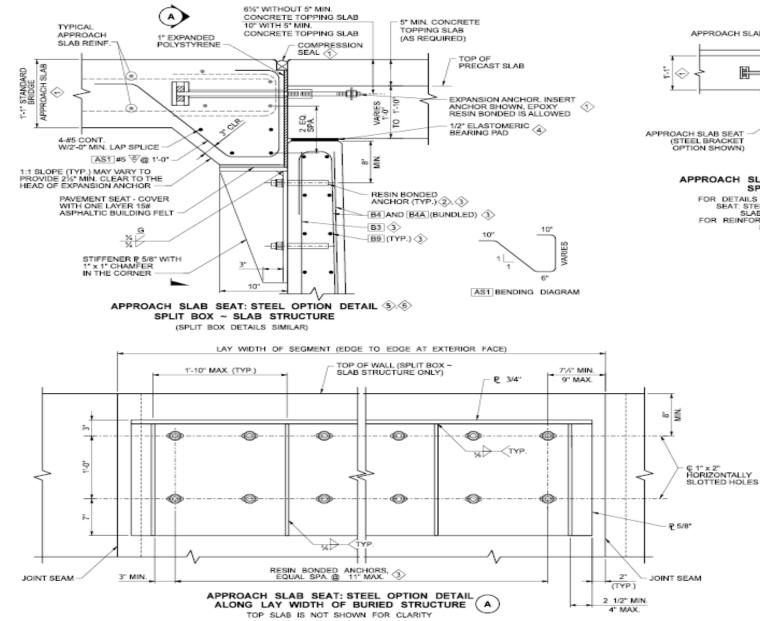
Wall Joints (Horizontal & Vertical) and Restrainers

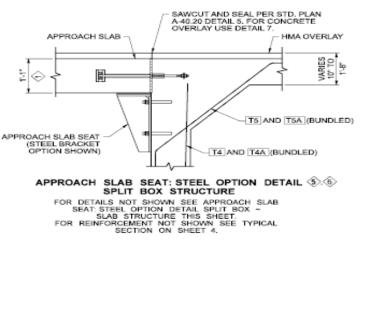


Headwall, Traffic Barrier, & Topping Slab Details



### Tie Plate & Optional Constr. Weld Tie Details





### KEY NOTES

- FOR APPROACH SLAB DETAILS INCLUDING REINFORCING, EXPANSION ANCHOR, COMPRESSION SEAL, AND OTHER, SEE STANDARD PLAN A 40.50.
- ANCHORS SHALL BE 7/8' DIA. SET IN 6-INCH LONG HOLES.
- MANUFACTURER AND CONTRACTOR SHALL COORDINATE SPACING OF WALL REINFORCING BARS AND LOCATION OF RESIN BONDED ANCHORS TO AVOID CONFLICT DURING INSTALLATION.
- THE CONTRACTOR MAY ADD A 1\* MINIMUM THICK GROUT PAD FOR LEVELING TOP OF BOTTOM UNIT PRIOR TO SETTING BEARING PAD ADJUST FINAL ELEVATIONS AS NEEDED. THE CONTRACTOR MAY SUBMIT ALTERNATE METHODS OF VERTICAL ADJUSTMENT TO THE ENGINEER FOR ACCEPTANCE.
- ADDITIONAL REINFORCEMENT IS REQUIRED FOR TOP AND BOTTOM UNITS, SEE SHEET 4 FOR DETAILS.
- FOR DETAILS OF STEEL APPROACH SLAB SEAT OPTION WITH SEISMIC RESTRAINER SEE SHEET 14. FOR DETAILS OF C.I.P. APPROACH SLAB SEAT OPTION SEE SHEET 15.

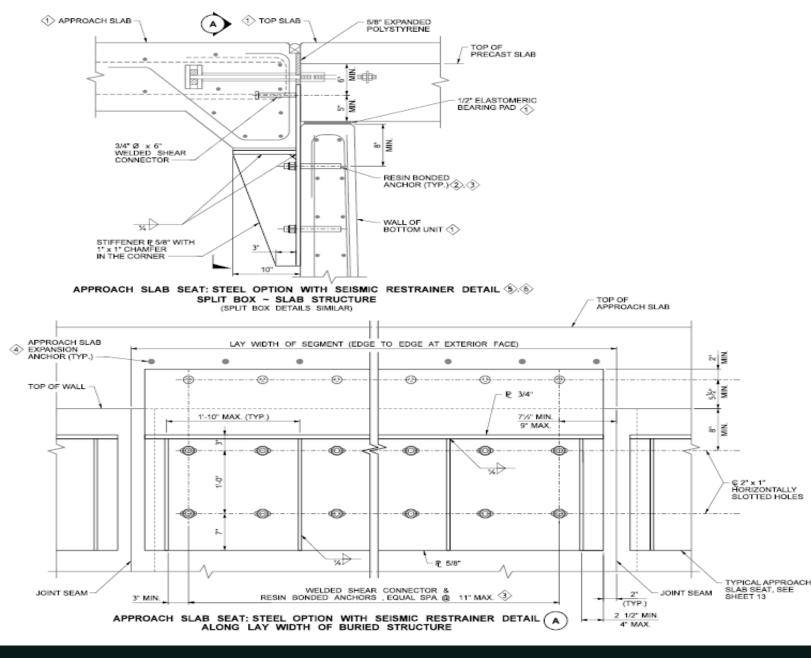


### BURIED STRUCTURE SPLIT BOX STANDARD PLAN E-20.10-00

SHEET 13 OF 17 SHEETS



### Approach Slab Seat ~ Steel Option



### SEISMIC LATERAL FORCE RESTRAINER SELECTION CRITERIA

- Seismic lateral force restraint is required for Split Box ~ Slab structures with less than 2 feet of Fill Depth. Options for Lateral Seismic Restraint are as follows:
  - a. Steel Option with Seismic Restrainer. See details this Sheet.
  - b. Accelerated Bridge Construction (ABC) Option. See details on Sheet 16.
  - c. C.I.P. End Diaphragm with Girder Stop Option. See Sheet 17.
- Seats with lateral restrainers shall be installed symmetrically in both walls of the segment. Minimum two segments with lateral restrainers are required along the length of buried structure. The total length (feet) of seats with lateral restrainers along each wall shall not be less than LR = w L PGA(2R), where:
  - w (kip/ft) Weight per linear foot of structure and roadway above the walls
  - L (ft) Total length of structure
  - PGA Effective Site Peak Ground Acceleration Coefficient

R = 10 kip/ft - Average shear resistance of anchors in the approach slab per foot length of bracket

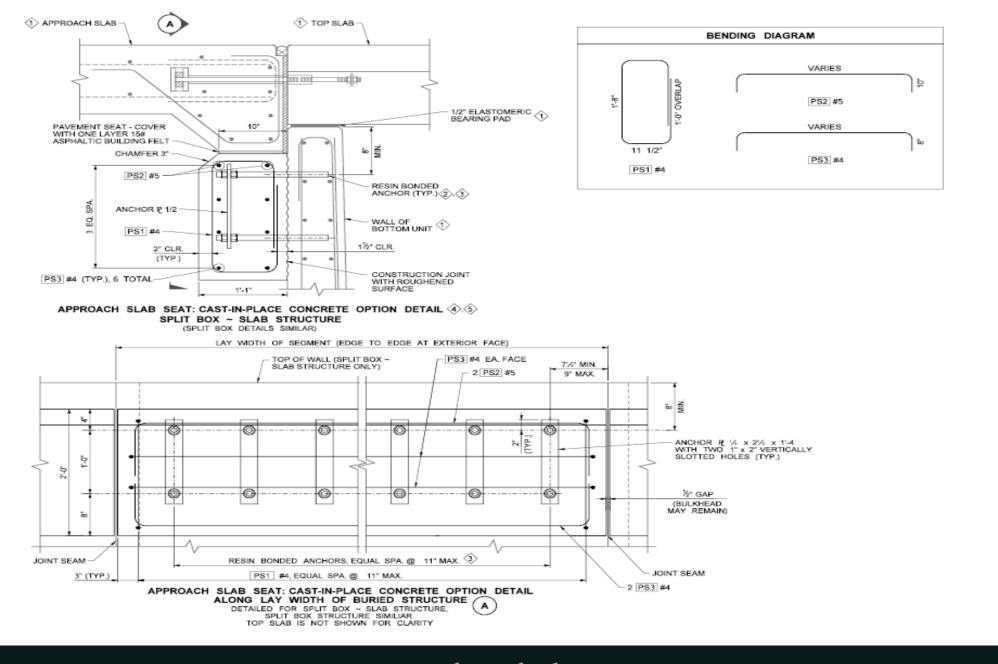
### KEY NOTES

- TO FOR DETAILS AND NOTATIONS NOT SHOWN SEE SHEET 13.
- ANCHORS SHALL BE 7/8" DIA. SET IN 6-INCH LONG HOLES.
- MANUFACTURER AND CONTRACTOR SHALL COORDINATE SPACING OF WALL REINFORCING BARS AND LOCATION OF RESIN BONDED ANCHORS TO AVOID CONFLICT DURING INSTALLATION.
- ARRANGE SPACING OF APPROACH SLAB EXPANSION ANCHORS AND WELDED SHEAR CONNECTORS TO PROVIDE MINIMUM 3 INCH DISTANCE BETWEEN.
- ADDITIONAL REINFORCEMENT IS REQUIRED FOR TOP AND BOTTOM UNITS, SEE SHEET 4 FOR DETAILS.
- FOR DETAILS OF STEEL APPROACH SLAB SEAT OPTION WITHOUT SEISMIC RESTRAINER SEE SHEET 13. FOR DETAILS OF C.I.P. APPROACH SLAB SEAT OPTION SEE SHEET 15.



### BURIED STRUCTURE SPLIT BOX STANDARD PLAN E-20.10-00 SHEET 14 OF 17 SHEETS APPROVED FOR PUBLICATION STATE DESIGN ENGINEER Weshington State Department of Transportation

# Approach Slab Seat ~ Steel Option w/Seismic Restrainer



### KEY NOTES

- FOR DETAILS AND NOTATIONS NOT SHOWN SEE SHEET 13.
- ANCHORS SHALL BE 7/8" DIA. SET IN 6-INCH LONG HOLES.
- MANUFACTURER AND CONTRACTOR SHALL COORDINATE SPACING OF WALL REINFORCING BARS AND LOCATION OF RESIN BONDED ANCHORS TO AVOID CONFLICT DURING INSTALLATION.
- ADDITIONAL REINFORCEMENT IS REQUIRED FOR TOP AND BOTTOM UNITS, SEE SHEET 4 FOR DETAILS.
- S FOR DETAILS OF STEEL APPROACH SLAB SEAT OPTION WITHOUT SEISMIC RESTRAINER SEE SHEET 13. FOR DETAILS OF STEEL APPROACH SLAB SEAT OPTION WITH SEISMIC RESTRAINER SEE SHEET 14.



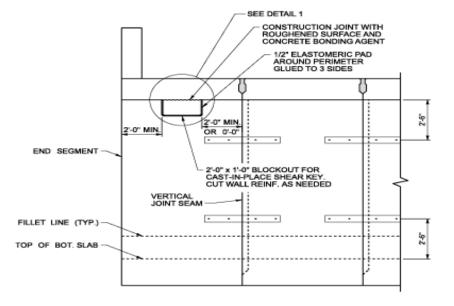
BURIED STRUCTURE SPLIT BOX

### STANDARD PLAN E-20.10-00

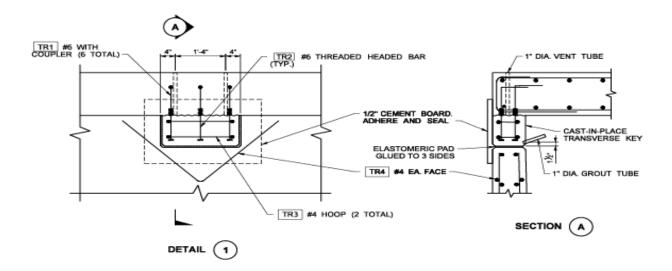
SHEET 15 OF 17 SHEETS APPROVED FOR PUBLICATION

STATE DESIGN ENGINEER Washington State Department of Transportation

### Approach Slab Seat ~ C.I.P. Option



SEISMIC LATERAL FORCE RESTRAINER ACCELERATED BRIDGE CONSTRUCTION (ABC) OPTION SPLIT BOX ~ SLAB STRUCTURE



### SEISMIC LATERAL FORCE RESTRAINER SELECTION CRITERIA:

- Seismic lateral force restraint is required for Split Box Slab structures with less than 2 feet of Fill Depth. Options for Lateral Seismic Restraint are as follows:
  - a. Accelerated Bridge Construction (ABC) Option. See details this Sheet.
  - b. Steel Option with Seismic Restrainer. See details on Sheet 14.
  - c. C.I.P. End Diaphragm with Girder Stop Option. See Sheet 17.
- 2. Two lateral restrainers shall be installed symmetrically in both walls of the segment. Minimum two segments with lateral restrainers are required along the length of buried structure. The number of segments with lateral restrainers can be calculated using formula: N = w L PGA I(2R) (rounded up to integer), where:
  - w (kip/ft) Weight per linear foot of structure and roadway above the walls
  - L (ft) Total length of structure
  - PGA Effective Site Peak Ground Acceleration Coefficient
  - R = 100 kips, shear key lateral resistance
- The lateral restrainers shall be installed in the end segments and spaced equally along the length of the structure.
- Shear key material shall be self-consolidating concrete placed using a 'bird feeder' technique, or a Type 2 Grout for Nonshrink Applications in accordance with Std. Spec. 9-20.3(2), placed via grout tubes.
- Shear keys can be installed after backfilling and open to traffic when applicable.
- This option not applicable with approach slabs.



### BURIED STRUCTURE SPLIT BOX

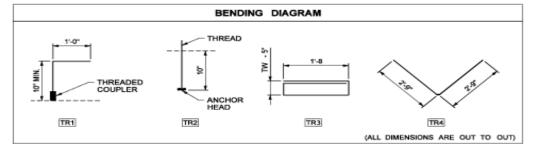
### STANDARD PLAN E-20.10-00

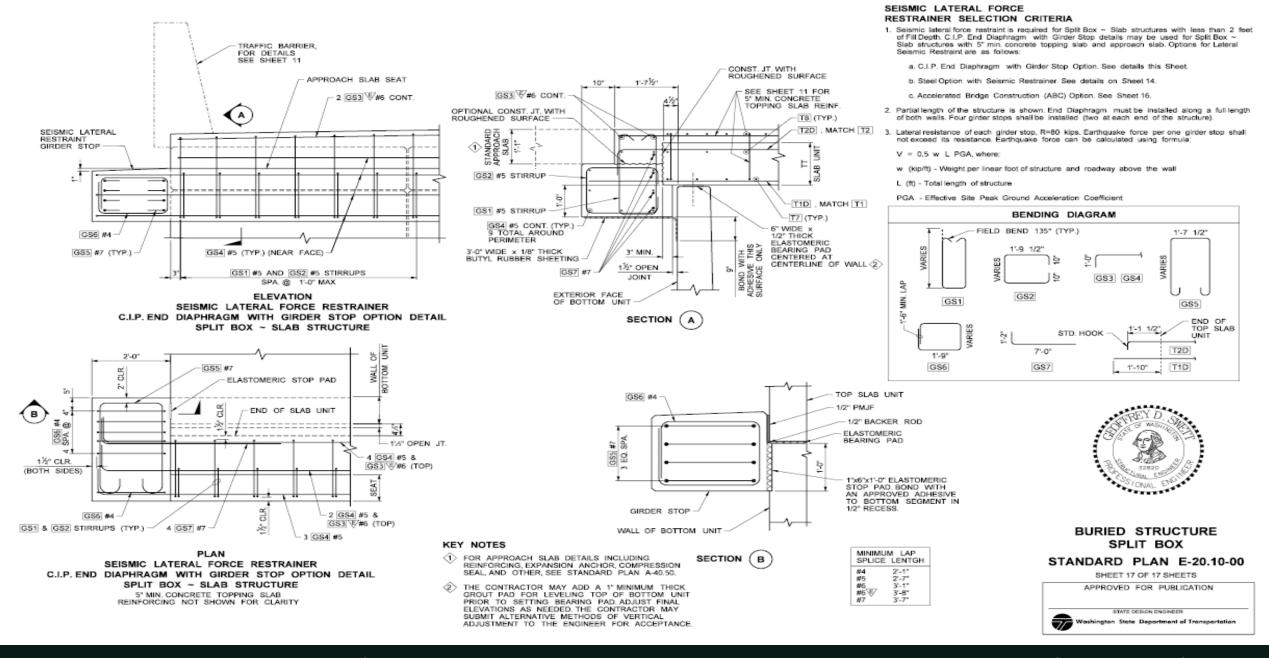
SHEET 16 OF 17 SHEETS

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### Seismic Lateral Force Restrainer ~ A.B.C. Option





### Seismic Lateral Force Restrainer ~ Semi-Integral Diaph.

# Thank you

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