

King County Roads Division  
Seattle Washington

# Proof Load Testing

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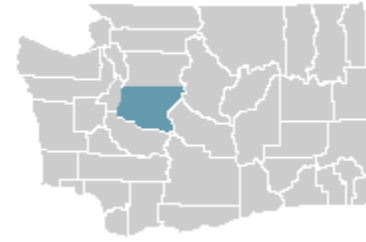
**Short Span Precast Channel Beam Bridges**



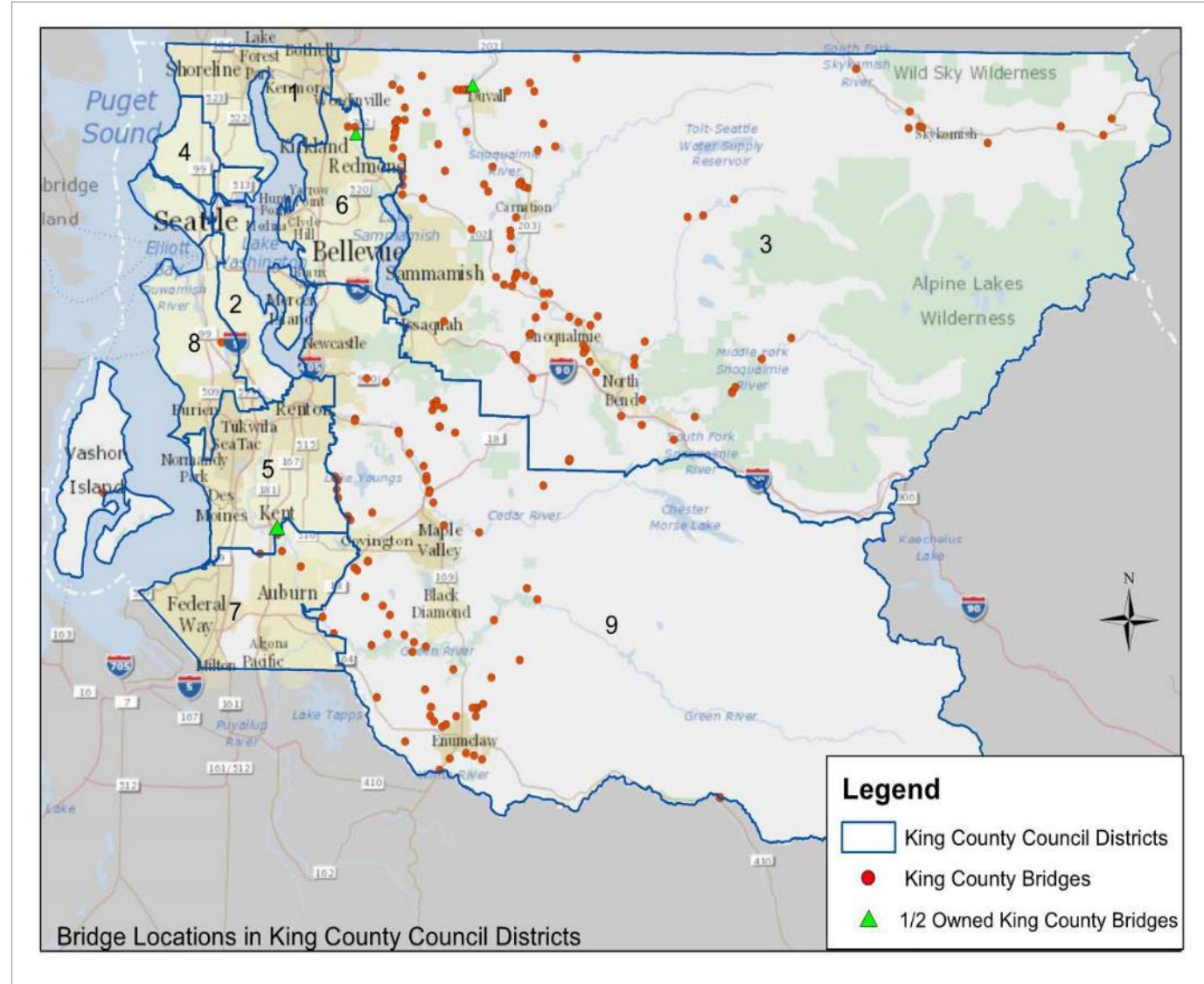
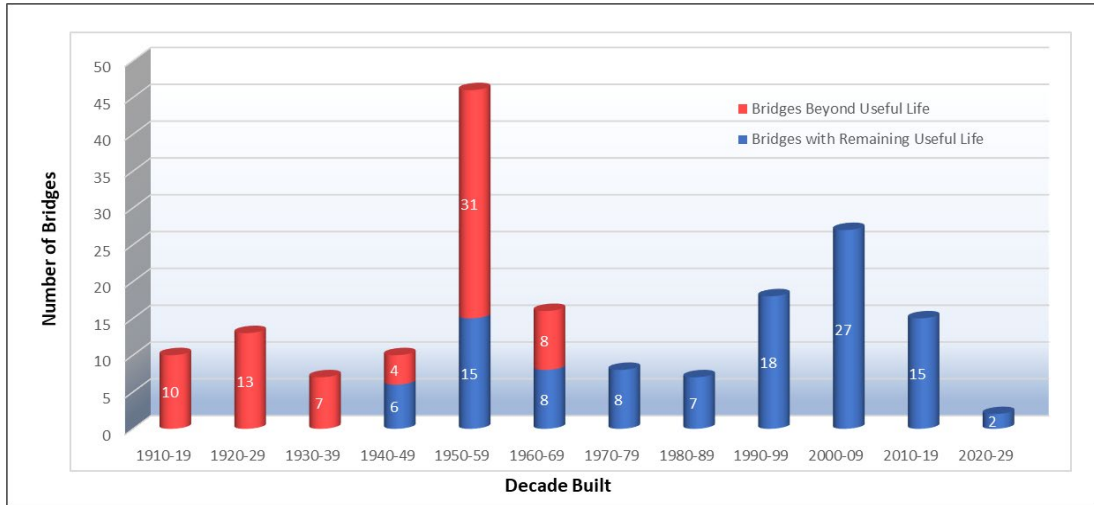
- Jason Lee, SE
- Senior Bridge Engineer
  - MSCE, University of Washington
    - Research assistant on CFST bridge piers
  - 10 years of bridge design as a consultant
  - 2 years at King County



# King County



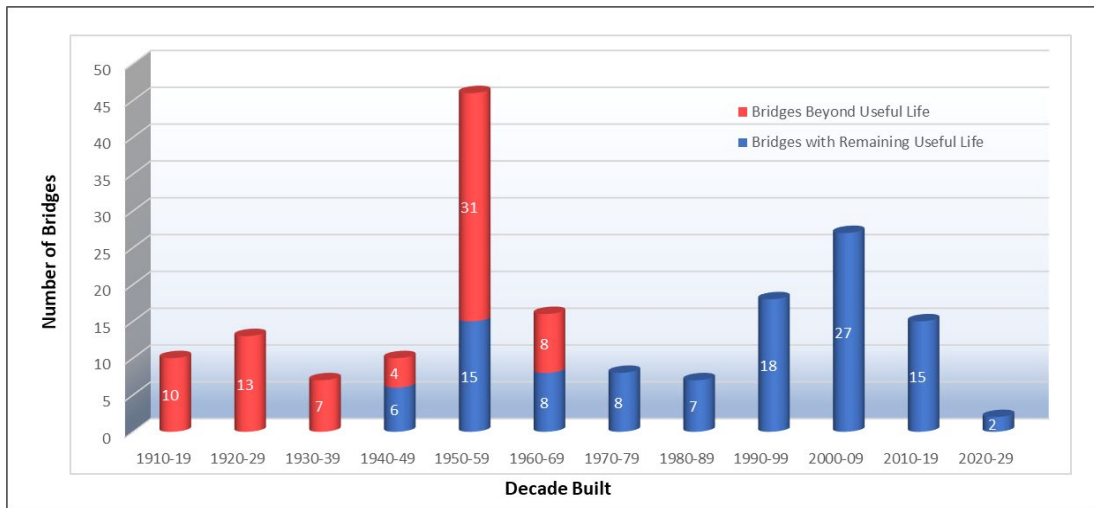
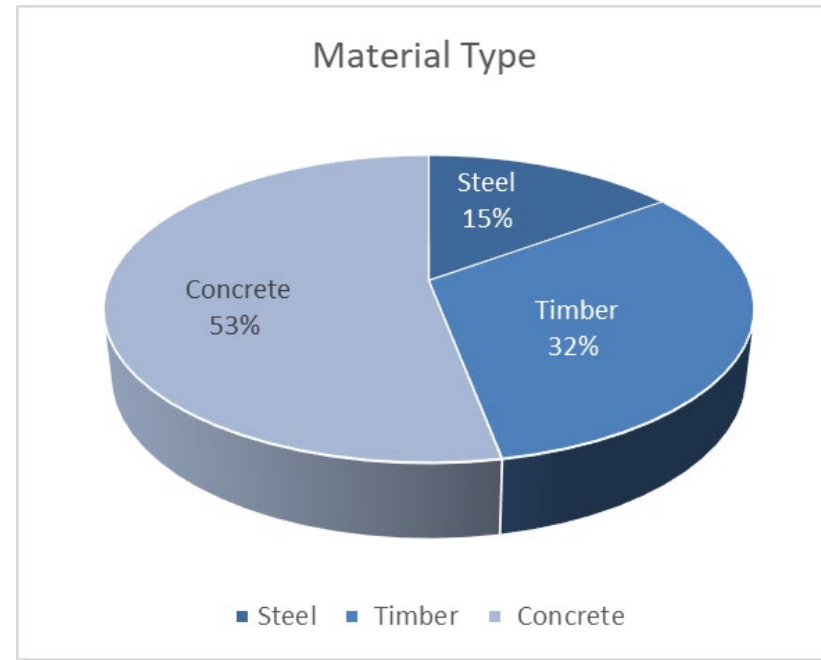
- 185 Bridges
  - 136 NBI Bridge
  - 45 short span bridges
  - 4 Pedestrian Bridges
  - Average bridge age = 52 years



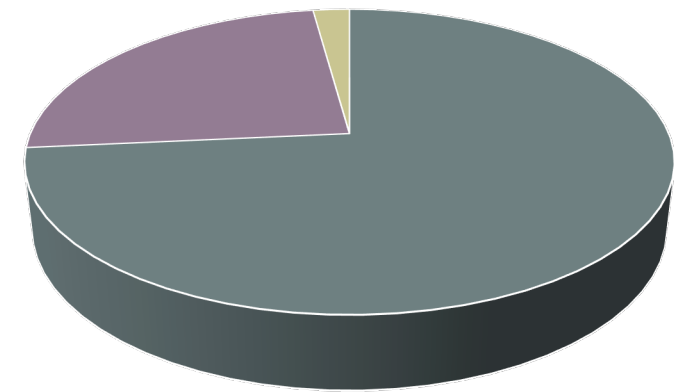


# King County

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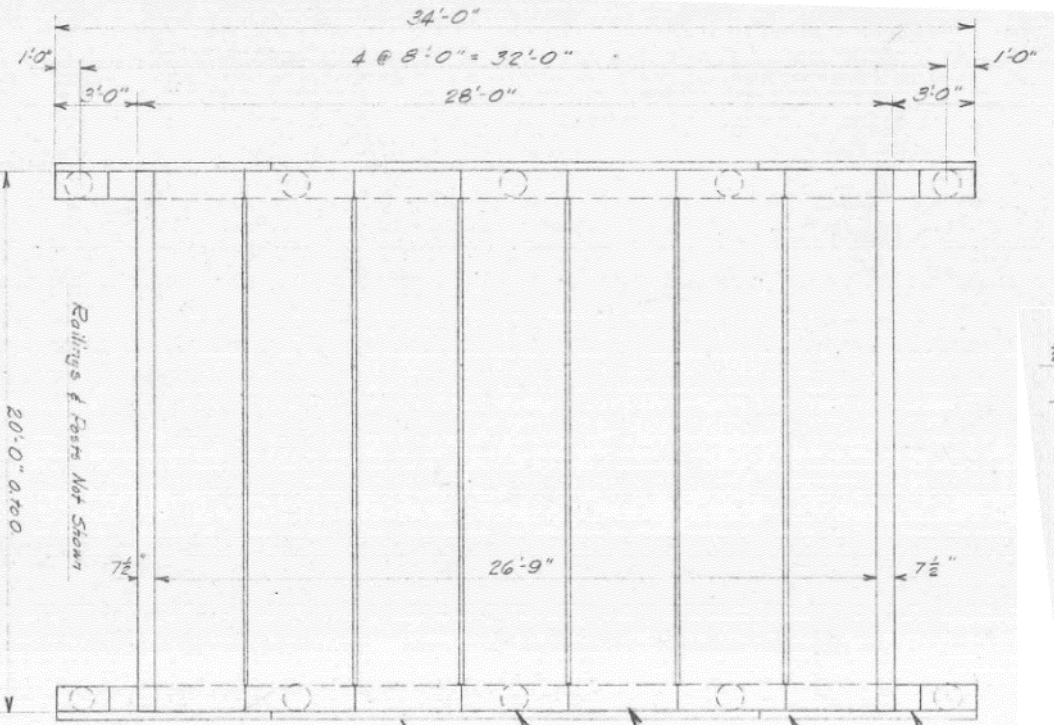
### King County Bridge Distribution



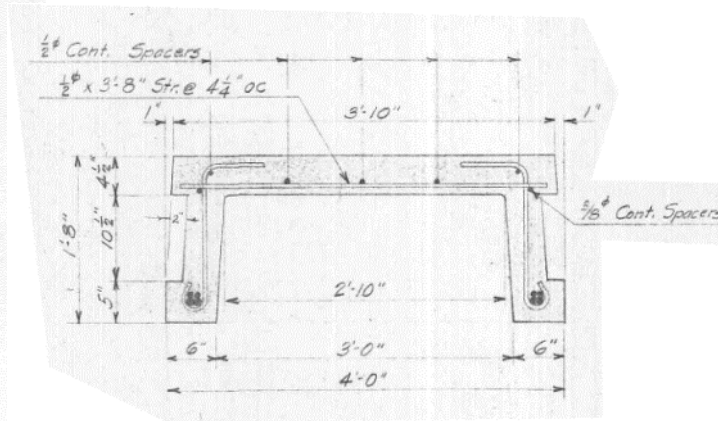
- NBI Bridges
- Short Span Bridges
- Pedestrian Bridges



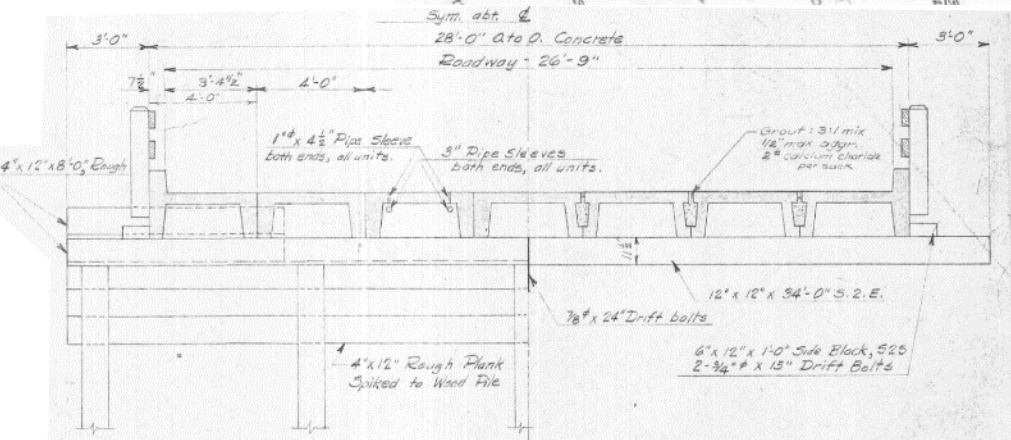
# Short Span Channel Bridges



Plan



Girder Section



Abutment View

Br No.	Bridge Name	Age	ADT	Percent Trucks	Span
240A	Cottage Lake Creek Bridge	72	14,759	4%	20'
3097	Dorre Don Way Bridge	64	95	1%	20'
3099	Maxwell Road Bridge	72	520	0%	20'
228F	312 <sup>th</sup> AVE SE Bridge	73	798	2%	20'
249C	C.W.Neal Bridge	72	99	2%	20'
578A	Evans Creek	73	170	5%	20'
916A	Pleasant Hill Rd	72	798	2%	20'
333A	Bear Creek Bridge	73	8,521	7%	20'
480A	Bear Creek Bridge	72	2,200	4%	20'
249B	C W Neal Road Bridge	72	99	3%	15.75'
909B	Clough Creek Bridge	72	1,328	3%	15.75'
3030	SE 380 St Bridge	73	760	2%	15.75'
3060	208th Ave SE Bridge	72	150	1%	15.75'
593C	May Creek Bridge	72	3,717	5%	15.75'
1086B	Coal Creek Bridge	73	459	1%	15.75'





# Short Span Channel Bridges

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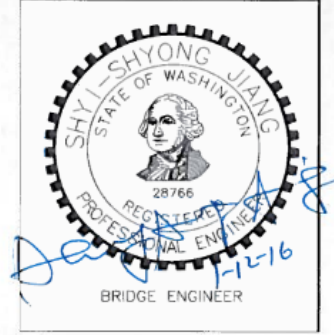
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**BRIDGE RATING SUMMARY**



**Bridge Name:** Clough Creek Bridge  
**Bridge Number:** 909B  
**Span Types:** Reinforced Concrete Multiple Web Girder  
**Bridge Length:** 15.75 feet  
**Design Load:** H15 **Year Built:** 1951  
**ADT/ADTT:** 1228/37  
**Rating by:** TTZ *TTZ*  
**Checked by:** ZZ *ZZ*  
**Date:** 11/9/2015

Inspect. Report Date	6/16/2015	Substructure Condition	6
Rating Method	LRFR	Deck Condition	5
Overlay Thickness	5.5	Superstructure Condition	5

Truck	RF	Tons	$\gamma$	Impact	Controlling Point
AASHTO 1 (Type 3)	0.91	23	1.30	0.33	Girder Shear
AASHTO 2 (Type 3S2)	1.04	38	1.30	0.33	Girder Shear
AASHTO 3 (Type 3-3)	1.20	48	1.30	0.33	Girder Shear
NRL	0.79	32	1.30	0.33	Girder Shear
SU-4	0.79	21	1.30	0.33	Girder Shear
SU-5	0.79	24	1.30	0.33	Girder Shear
SU-6	0.79	27	1.30	0.33	Girder Shear
SU-7	0.79	31	1.30	0.33	Girder Shear
OL-1	0.72	35	1.20	0.33	Girder Shear
OL-2	0.61	64	1.20	0.33	Girder Shear
UBIT-30	1.50	23	1.20	0.33	Girder Mid-Span Flexure
UBIT-60	0.97	32	1.20	0.33	Girder Shear

NBI Rating Truck	RF	Tons	$\gamma$	Impact	Controlling Point
Inventory (HL-93)	0.28	10	1.75	0.33	Girder Shear
Operating (HL-93)	0.41	15	1.35	0.33	Girder Shear

Note: Inventory and Operating tonnages are based on the rating factors multiply 36 tons (HS-20 Truck)





# Load Rating Toolbox



## Analytical Load Ratings

(MBE § 6, Part A/Part B)

- Analysis using design values and conventional assumptions.
- Can be enhanced with material testing

## Diagnostic Load Testing

(MBE § 8.8.2)

- Nondestructive testing to improve the engineers understanding of the bridge behavior.
- Typically uses gauges and other measuring devices to measure the behavior of the bridge.
- Analytical model used for final load rating built off the data created during testing.

## Proof Load Testing

(MBE § 8.8.3)

- Field load testing and observation used to determine if the bridge can carry specific loads without damage.



# Material Testing

## Concrete Strength Testing

- 2.75" Ø core through girder flange
- 8 cores from 16ft channel beams
- 8 cores from 20ft channel beams

## Reinforcing Steel Material Testing

- 6" coupons from flange and web
- 3 samples from 16ft channel beams
- 3 samples from 20ft channel beams

### SAMPLE NAME



### SAMPLE LOCATION







# Material Testing

- Concrete Strength Testing
  - 2.75" Ø core through girder flange
  - 8 cores from 16ft channel beams
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- Reinforcing Steel Material Testing
  - 6" coupons from flange and web
  - 3 samples from 16ft channel beams
  - 3 samples from 20ft channel beams

## Results

- Resulting Concrete Strength =
  - $F'_c = 4.5$  ksi
- Resulting Steel Strength =
  - $F_y = 55$  ksi
  - $F_u = 86$  ksi







## Why Proof Load Testing??

- The results of analytical methods and material testing did not show sufficient capacity.
- Diagnostic load testing was cost prohibitive.
- Routine inspections indicated the channel girders were in fair to satisfactory condition.
- Access to beams from decommissioned bridges we could test in our maintenance yard.







# Proof Load Testing

## Selecting a Test Method

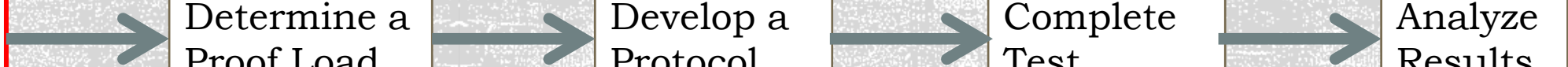
Select a Test Method

Determine a Proof Load

Develop a Protocol

Complete Test

Analyze Results



# Selecting a Testing Method

## Truck/Axle Loads



## Laboratory Setting



## Self Perform







# Selecting a Testing Method

## Why Self Perform?

### Pros

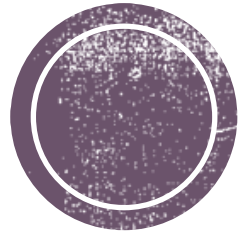
- Lowest cost
- Most control over schedule and process

### Cons

- Fewer data collection opportunities
- Limited monitoring
- Limited load capacity







# Proof Load Testing

## Determine the Proof Load

Select a Test Method

Determine a Proof Load

Develop a Protocol

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Analyze Results



# Proof Load Tests (MBE §8.8.3)

- Approach
  - Determine critical load demands on structure
  - Select a Target Proof Load
  - Apply Target Proof Load
    - Apply load in stages
    - Closely monitor structure at each stage of loading.
    - Incremental loading should continue until desired load is reached or bridge exhibits visible signs of distress.

- Selecting a Target Proof Load

$$X_{p,t} = X_p \left( 1 + \frac{\sum \%}{100} \right) \quad (8.8.3.3.2-1)$$

The target proof load  $L_T$  is then:

$$L_T = X_{p,t} L_R (1 + IM) \quad (8.8.3.3.2-2)$$

where:

$L_R$  = comparable unfactored live load due to the rating vehicle for the lanes loaded

$IM$  = dynamic load allowance

$X_{p,t}$  = target adjusted live-load factor

Table 8.8.3.3.1-1—Adjustments to  $X_p$

Consideration	Adjustment
One-Lane Load Controls	+15%
Nonredundant Structure	+10%
Fracture-Critical Details Present	+10%
Bridges in Poor Condition	+10%
In-Depth Inspection Performed	-5%
Rateable, Existing $RF \geq 1.0$	-5%
$ADTT \leq 1,000$	-10%
$ADTT \leq 100$	-15%





# Proof Load Tests (MBE §8.8.3)

- Example Target Proof Load
- Shear near support from NRL
  - $L_R = 20$  Kip
  - $X_p = 1.4$
  - $X_{pA} = X_p \left(1 + \frac{\sum \%}{100}\right) = 1.4 \left(1 + \frac{15\%}{100}\right) = 1.61$
  - $L_T = X_{pA} L_R (1 + IM) = 1.61 * 20 * (1.33) = 43$  Kip

## Capacity and Rating

- $OP = \frac{k_o L_p}{X_{pA}}$

Table 8.8.3.3.1—Values for  $k_o$

Terminated	$k_o$
Reached Target Load	1.00
Reached Distress Level	0.88

## Selecting a Target Proof Load

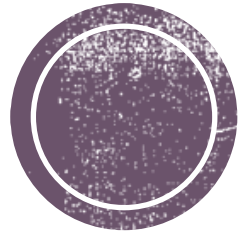
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# Proof Load Testing

## Develop a Protocol

Select a Test Method

Determine a Proof Load

Develop a Protocol

Complete Test

Analyze Results





# Developing a Protocol

Flexure Proof Load

Test Load	TL Magnitude	Total Moment	Notes
Proof Load (k-in)	2495	2890	Target Shear load
Stage 1	623.75	1019	0.25*proof load
Stage 2	1247.5	1643	0.5*proof load
Stage 3	1871.25	2266	0.75*proof load
Stage 4	2183.125	2578	0.875*proof load
Stage 5	2495	2890	target proof load
Stage 6	2744.5	3140	1.1*proof load
Stage 7	2994	3389	1.2*proof load
Stage 8	3243.5	3639	1.3*proof load
Stage 9	3628	4023	1.4*proof load

\*unfactored dead load demands = 395 k-in

Shear Proof Load

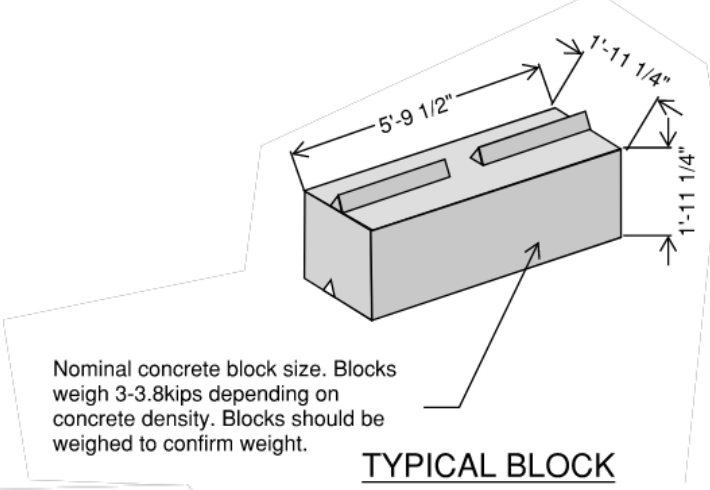
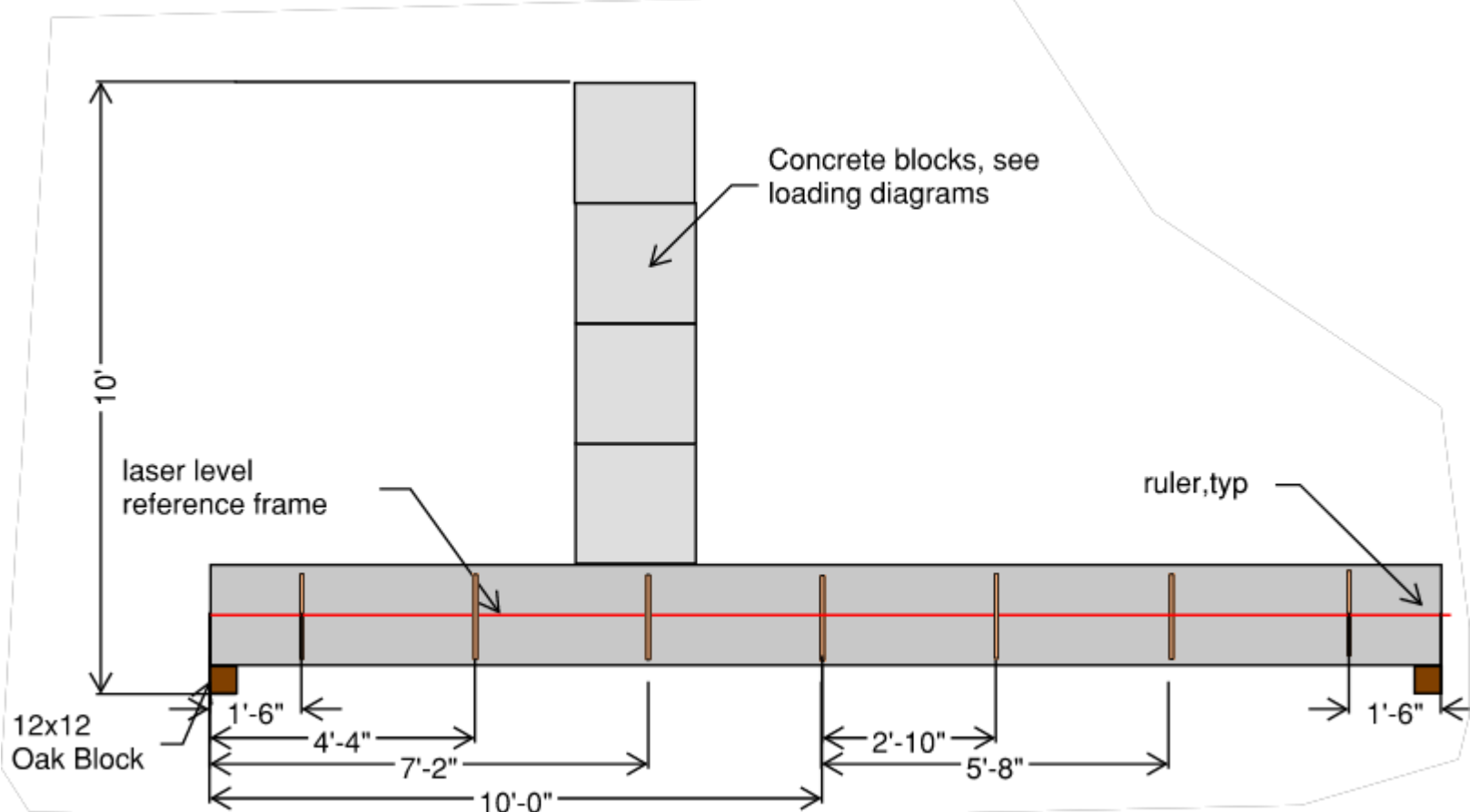
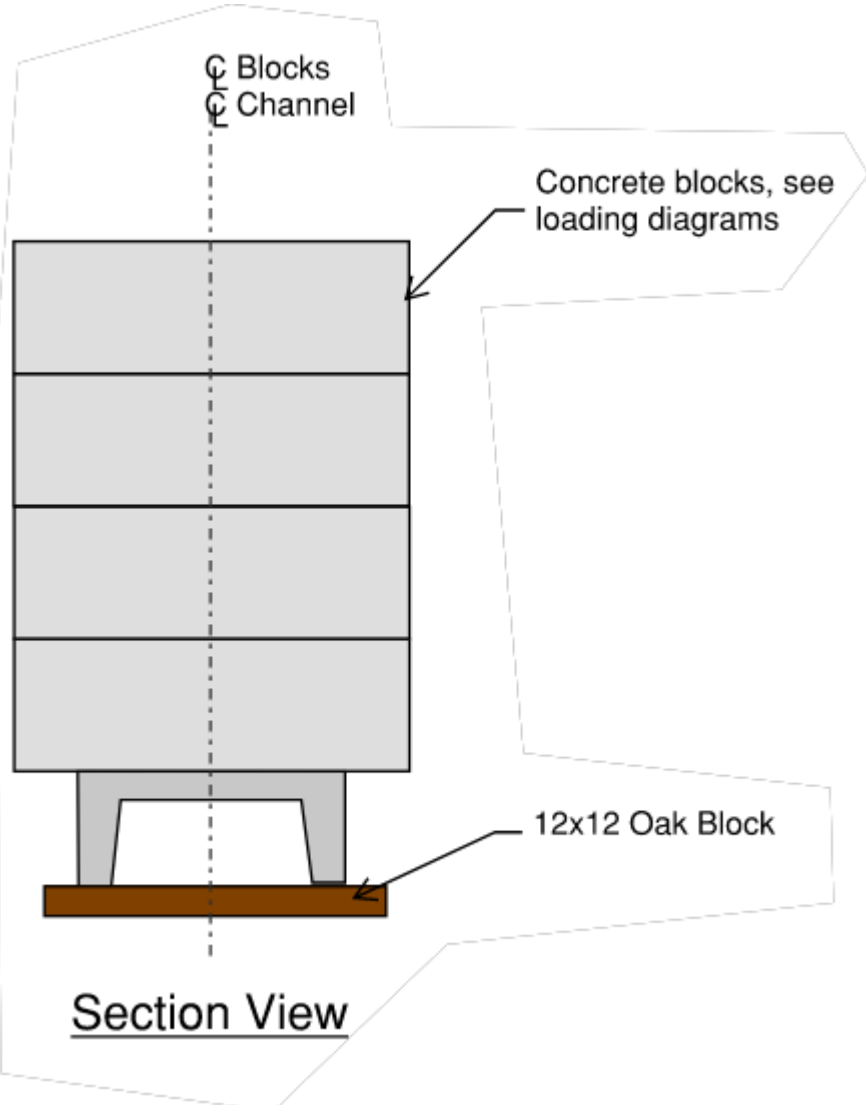
Test Load	TL Magnitude	Total Shear	Load
Proof Load (kip)	42	48	Target Shear load
Stage 1	10.5	16	0.25*proof load
Stage 2	21	27	0.5*proof load
Stage 3	31.5	37	0.75*proof load
Stage 4	36.75	42	0.875*proof load
Stage 5	42	48	target proof load
Stage 6	46.2	52	1.1*proof load
Stage 7	50.4	56	1.2*proof load
Stage 8	54.6	60	1.3*proof load
Stage 9	56.8	62	1.4*proof load

\*unfactored dead load demands = 5.5 kips

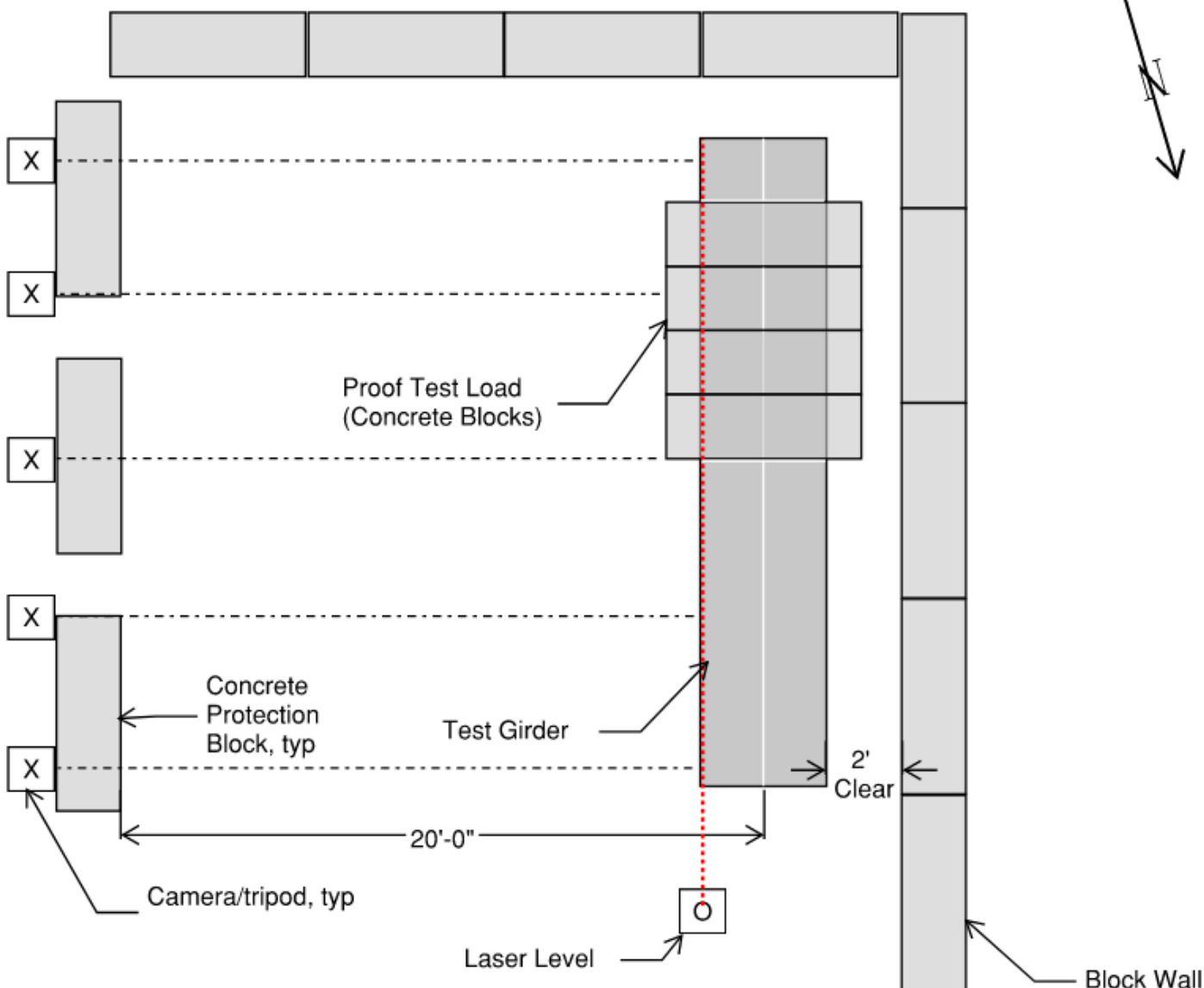




# Developing a Protocol



# Developing a Protocol

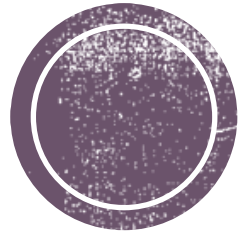


Plan View

- ❑ Cameras set for high resolution photos
- ❑ Rulers and reference line set for deflection measurements
- ❑ Beam set in loading area with access behind wall for adding loading blocks
- ❑ Staffing
  - ❑ Test Manager
  - ❑ Recorder 1
  - ❑ Recorder 1
  - ❑ Operator 1
  - ❑ Safety Officer







# Proof Load Testing

## Conduct Test

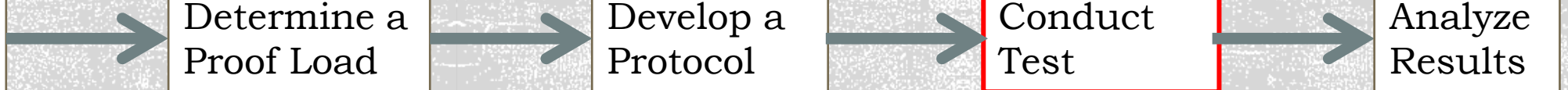
Select a Test Method

Determine a Proof Load

Develop a Protocol

Conduct Test

Analyze Results



## Test and Stage Detail

Specimen #: 20-B

Span Length: 20'-0"

Protocol: Flexure Proof Load

Stage: 1 (25% of Flexure Proof Load)

blocks: 4 blocks

Applied Weight: 17 k

Total Weight 24 k

Max Moment: 711.3 k-in

Approx shear @ dv: 9.3k

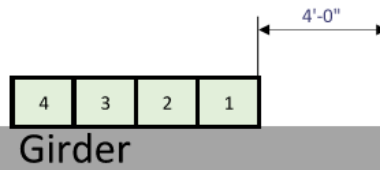
$M_n = 2868$  k-in

$V_n = 53.6$  kip

$M_{proof} = 2495$  k-in

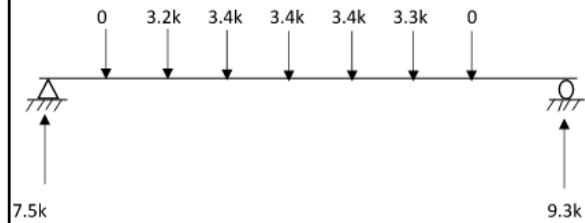
$V_{proof} = 42$  kip

## BLOCK CONFIGURATION

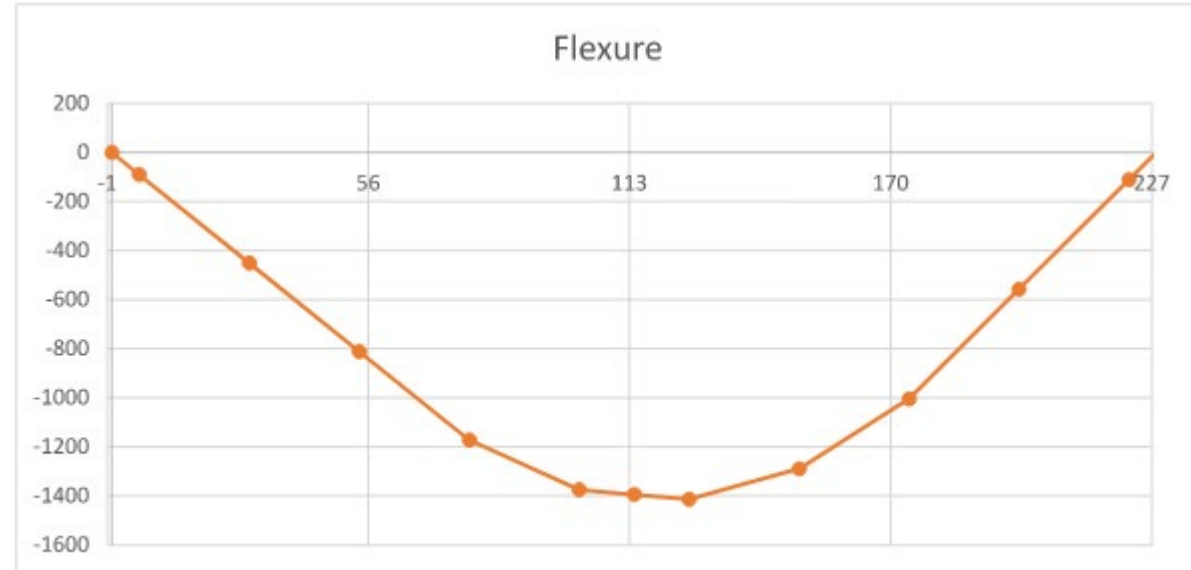
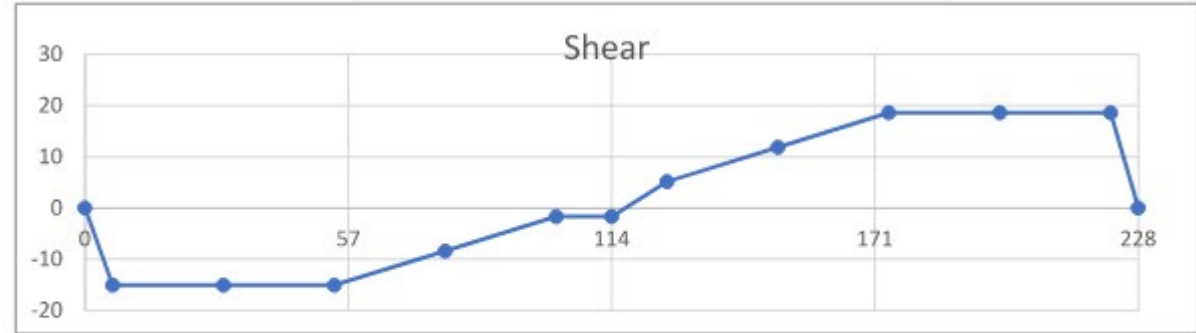


## NOTES:

## IDEALIZED LOAD DIAGRAM



$M_{mid span}$





## Test and Stage Detail

Specimen #: 20-B

Span Length: 20'-0"

Protocol: Flexure Proof Load

Stage: 1 (25% of Flexure Proof Load)

blocks: 4 blocks

Applied Weight: 17 k

Total Weight: 24 k

Max Moment: 711.3 k-in

Approx shear @ dv: 9.3k

$M_n = 2868 \text{ k-in}$

$V_n = 53.6 \text{ kip}$

$M_{\text{proof}} = 2495 \text{ k-in}$

$V_{\text{proof}} = 42 \text{ kip}$





## Test and Stage Detail

Specimen #: 20-B

Span Length: 20'-0"

Protocol: Flexure Proof Load

Stage: 1 (25% of Flexure Proof Load)

blocks: 4 blocks

Applied Weight: 17 k

Total Weight 24 k

Max Moment: 711.3 k-in

Approx shear @ dv: 9.3k

$M_n = 2868$  k-in

$V_n = 53.6$  kip

$M_{proof} = 2495$  k-in

$V_{proof} = 42$  kip





### Test and Stage Detail

Specimen #: 20-B

Span Length: 20'-0"

Protocol: Flexure Proof Load

Stage: 2 (50% of Flexure Proof Load)

blocks: 8 blocks

Applied Weight: 34 k

Total Weight 40 k

Max Moment: 1414.3 k-in

Approx shear @ dv: 18.6k

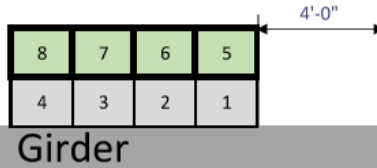
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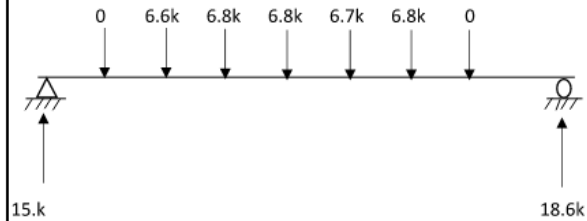
$V_{proof} = 42$  kip

### BLOCK CONFIGURATION

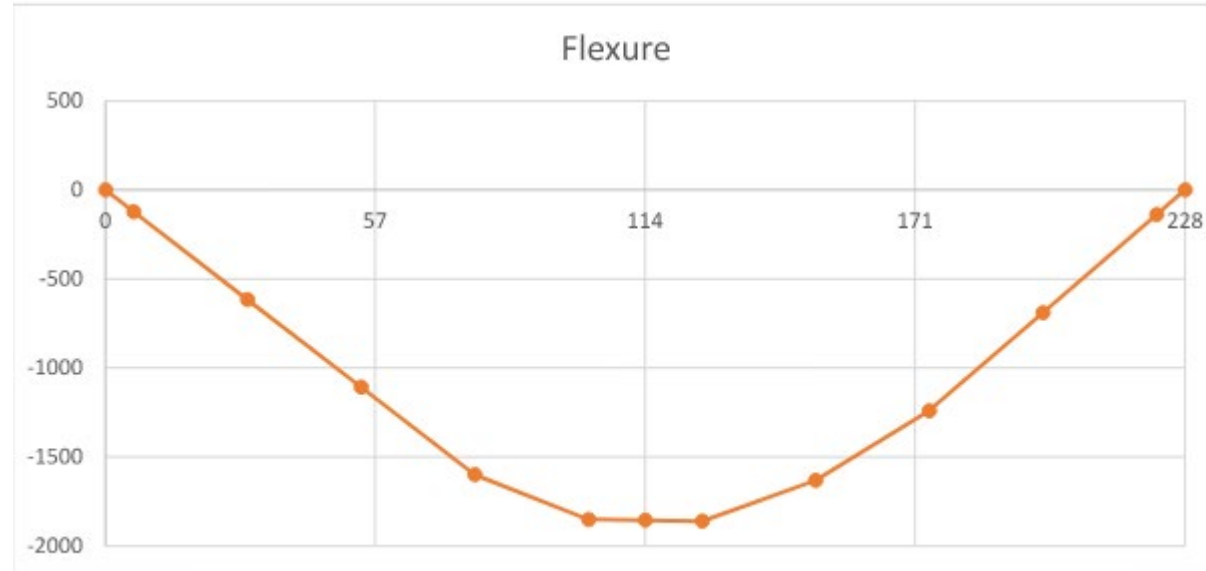


### NOTES:

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$M_{mid span}$



## Test and Stage Detail

Specimen #: 20-B

Span Length: 20'-0"

Protocol: Flexure Proof Load

Stage: 2 (50% of Flexure Proof Load)

blocks: 8 blocks

Applied Weight: 34 k

Total Weight 40 k

Max Moment: 1414.3 k-in

Approx shear @ dv: 18.6k

$M_n = 2868$  k-in

$V_n = 53.6$  kip

$M_{proof} = 2495$  k-in

$V_{proof} = 42$  kip





## Test and Stage Detail

Specimen #: 20-B

Span Length: 20'-0"

Protocol: Flexure Proof Load

Stage: 3 (75% of Flexure Proof Load)

blocks: 13 blocks

Applied Weight: 44 k

Total Weight 50 k

Max Moment: 1860.7 k-in

Approx shear @ dv: 23.k

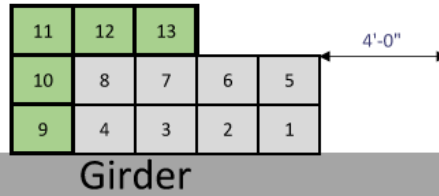
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$V_n = 53.6$  kip

$M_{proof} = 2495$  k-in

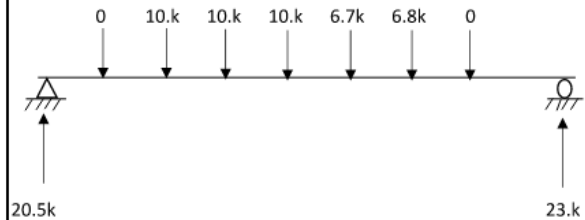
$V_{proof} = 42$  kip

## BLOCK CONFIGURATION

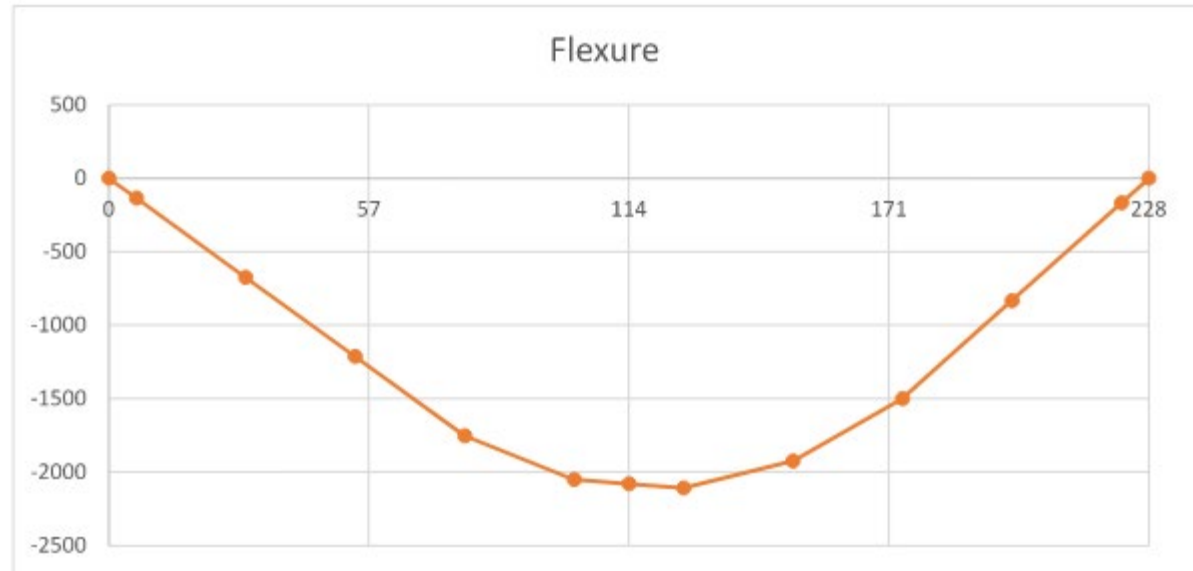


## NOTES:

## IDEALIZED LOAD DIAGRAM



$M_{mid}$  sp:



## Test and Stage Detail

Specimen #: 20-B

Span Length: 20'-0"

Protocol: Flexure Proof Load

Stage: 3 (75% of Flexure Proof Load)

blocks: 13 blocks

Applied Weight: 44 k

Total Weight 50 k

Max Moment: 1860.7 k-in

Approx shear @ dv: 23.k

$M_n = 2868$  k-in

$V_n = 53.6$  kip

$M_{proof} = 2495$  k-in

$V_{proof} = 42$  kip





## Test and Stage Detail

Specimen #: 20-B

Span Length: 20'-0"

Protocol: Flexure Proof Load

Stage: 4 (87.5% of Flexure Proof Load)

blocks: 15 blocks

Applied Weight: 50 k

Total Weight 57 k

Max Moment: 2107.8 k-in

Approx shear @ dv: 27.8k

$M_n = 2868 \text{ k-in}$

$V_n = 53.6 \text{ kip}$

$M_{proof} = 2495 \text{ k-in}$

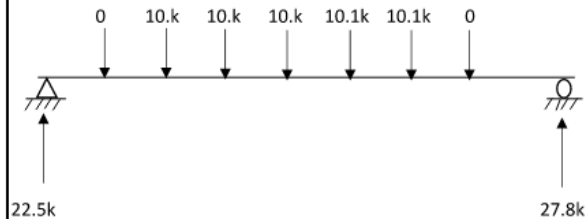
$V_{proof} = 42 \text{ kip}$

## BLOCK CONFIGURATION

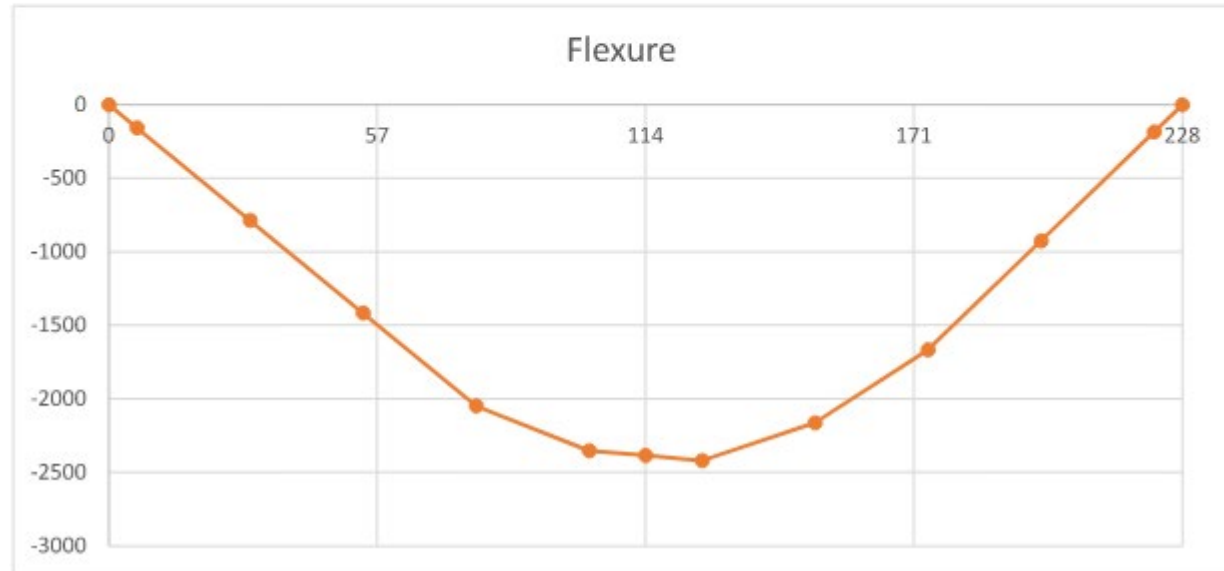


## NOTES:

## IDEALIZED LOAD DIAGRAM



$M_{mid span}$



# Test and Stage Detail

Specimen #: 20-B

Span Length: 20'-0"

Protocol: Flexure Proof Load

Stage: 4 (87.5% of Flexure Proof Load)

blocks: 15 blocks

Applied Weight: 50 k

Total Weight 57 k

Max Moment: 2107.8 k-in

Approx shear @ dv: 27.8k

$M_n = 2868 \text{ k-in}$

$V_n = 53.6 \text{ kip}$

$M_{proof} = 2495 \text{ k-in}$

$V_{proof} = 42 \text{ kip}$





### Test and Stage Detail

Specimen #: 20-B

Span Length: 20'-0"

Protocol: Flexure Proof Load

Stage: 5 (100% of Flexure Proof Load)

blocks: 17 blocks

Applied Weight: 57 k

Total Weight 64 k

Max Moment: 2419.5 k-in

Approx shear @ dv: 30.9k

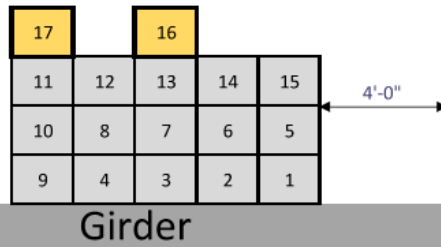
$M_n = 2868 \text{ k-in}$

$V_n = 53.6 \text{ kip}$

$M_{proof} = 2495 \text{ k-in}$

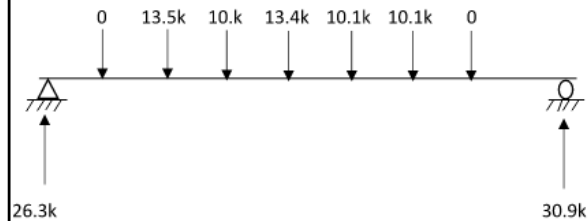
$V_{proof} = 42 \text{ kip}$

### BLOCK CONFIGURATION

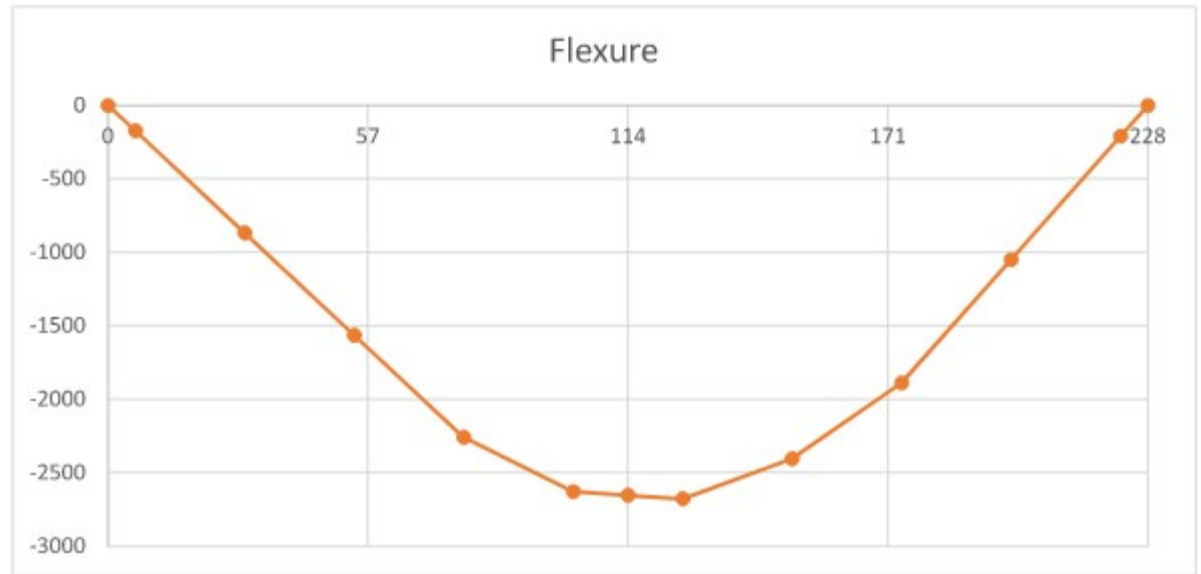


### NOTES:

### IDEALIZED LOAD DIAGRAM



$M_{mid span}$



## Test and Stage Detail

Specimen #: 20-B

Span Length: 20'-0"

Protocol: Flexure Proof Load

Stage: 5 (100% of Flexure Proof Load)

blocks: 17 blocks

Applied Weight: 57 k

Total Weight 64 k

Max Moment: 2419.5 k-in

Approx shear @ dv: 30.9k

$M_n = 2868$  k-in

$V_n = 53.6$  kip

$M_{proof} = 2495$  k-in

$V_{proof} = 42$  kip





## Test and Stage Detail

Specimen #: 20-B

Span Length: 20'-0"

Protocol: Flexure Proof Load

Stage: 6 (110% of Flexure Proof Load)

blocks: 19 blocks

Applied Weight: 64 k

Total Weight 71 k

Max Moment: 2677.9 k-in

Approx shear @ dv: 35.k

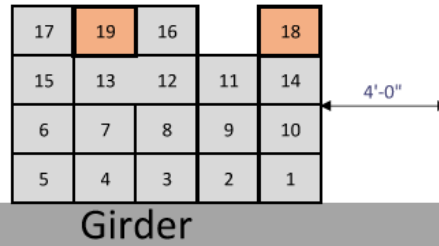
$M_n = 2868$  k-in

$V_n = 53.6$  kip

$M_{proof} = 2495$  k-in

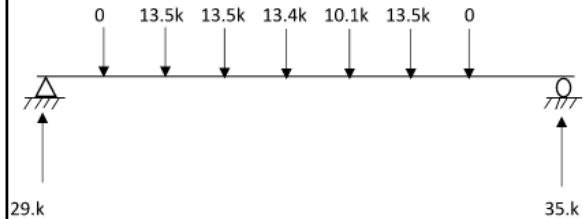
$V_{proof} = 42$  kip

## BLOCK CONFIGURATION

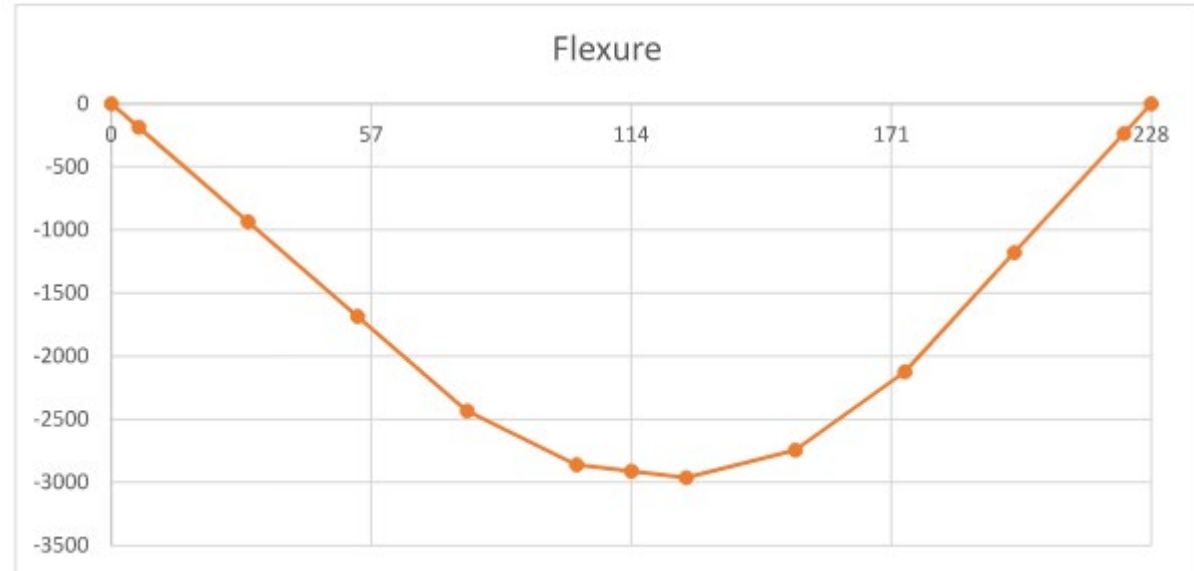


## NOTES:

## IDEALIZED LOAD DIAGRAM



$M_{mid span}$



## Test and Stage Detail

Specimen #: 20-B

Span Length: 20'-0"

Protocol: Flexure Proof Load

Stage: 6 (110% of Flexure Proof Load)

blocks: 19 blocks

Applied Weight: 64 k

Total Weight 71 k

Max Moment: 2677.9 k-in

Approx shear @ dv: 35.k

$M_n = 2868$  k-in

$V_n = 53.6$  kip

$M_{proof} = 2495$  k-in

$V_{proof} = 42$  kip





## Test and Stage Detail

Specimen #: 20-B

Span Length: 20'-0"

Protocol: Flexure Proof Load

Stage: 7 (120% of Flexure Proof Load)

blocks: 21 blocks

Applied Weight: 71 k

Total Weight 77 k

Max Moment: 2963.3 k-in

Approx shear @ dv: 39.3k

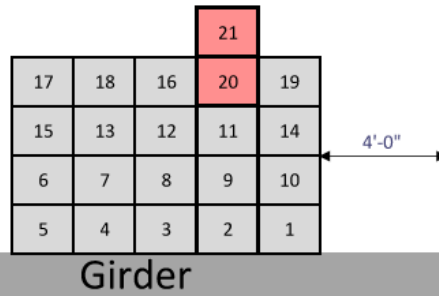
$M_n = 2868 \text{ k-in}$

$V_n = 53.6 \text{ kip}$

$M_{proof} = 2495 \text{ k-in}$

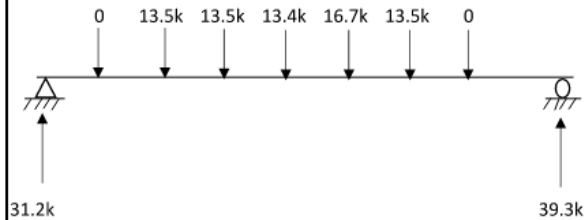
$V_{proof} = 42 \text{ kip}$

## BLOCK CONFIGURATION

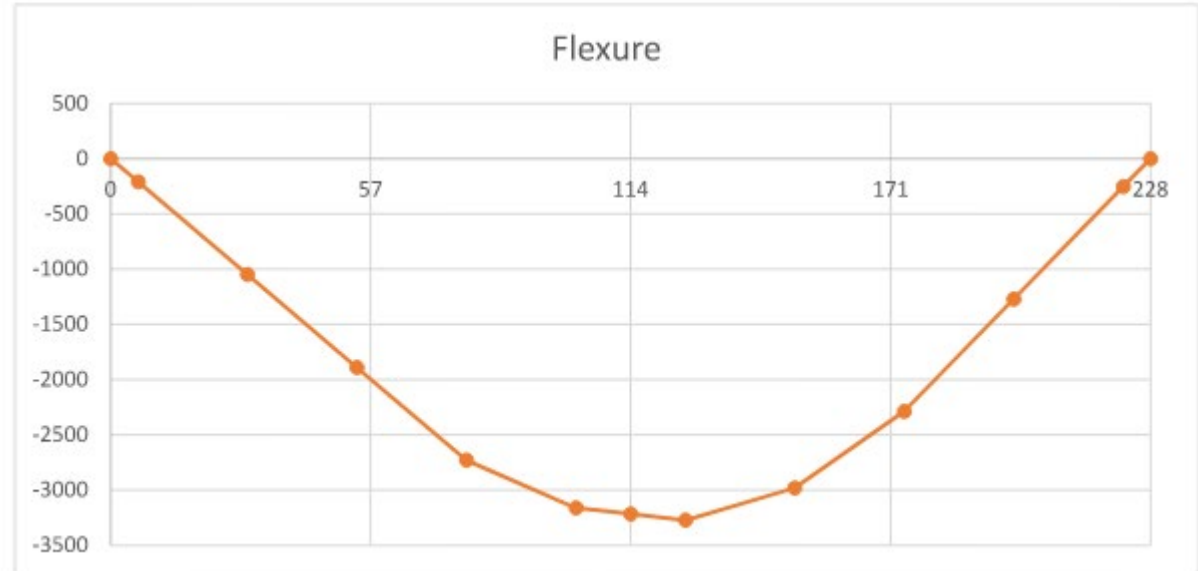
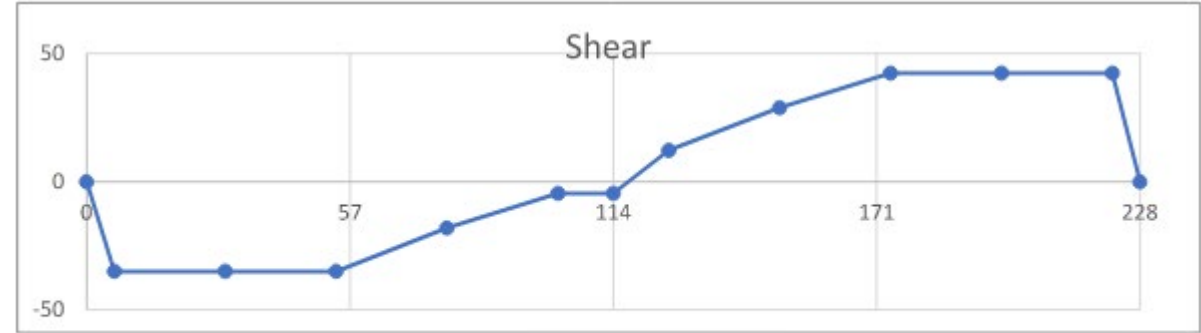


## NOTES:

## IDEALIZED LOAD DIAGRAM



$M_{mid span}$



# Test and Stage Detail

Specimen #: 20-B

Span Length: 20'-0"

Protocol: Flexure Proof Load

Stage: 7 (120% of Flexure Proof Load)

blocks: 21 blocks

Applied Weight: 71 k

Total Weight 77 k

Max Moment: 2963.3 k-in

Approx shear @ dv: 39.3k

Mn = 2868 k-in

Vn = 53.6 kip

M<sub>proof</sub> = 2495 k-in

V<sub>proof</sub> = 42 kip





## Test and Stage Detail

Specimen #: 20-B

Span Length: 20'-0"

Protocol: Flexure Proof Load

Stage: 8 (130% of Flexure Proof Load)

blocks: 23 blocks

Applied Weight: 77 k

Total Weight 84 k

Max Moment: 3273.9 k-in

Approx shear @ dv: 42.4k

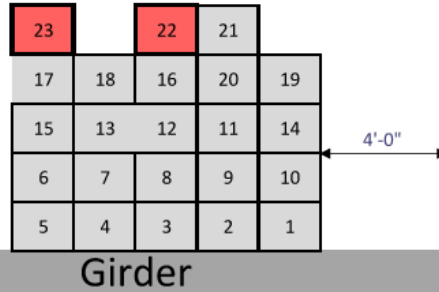
$M_n = 2868$  k-in

$V_n = 53.6$  kip

$M_{proof} = 2495$  k-in

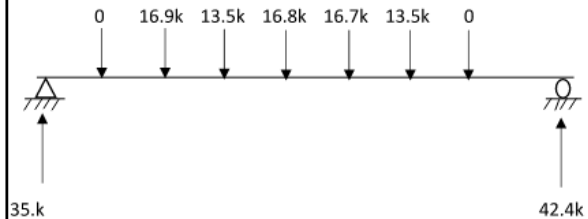
$V_{proof} = 42$  kip

## BLOCK CONFIGURATION

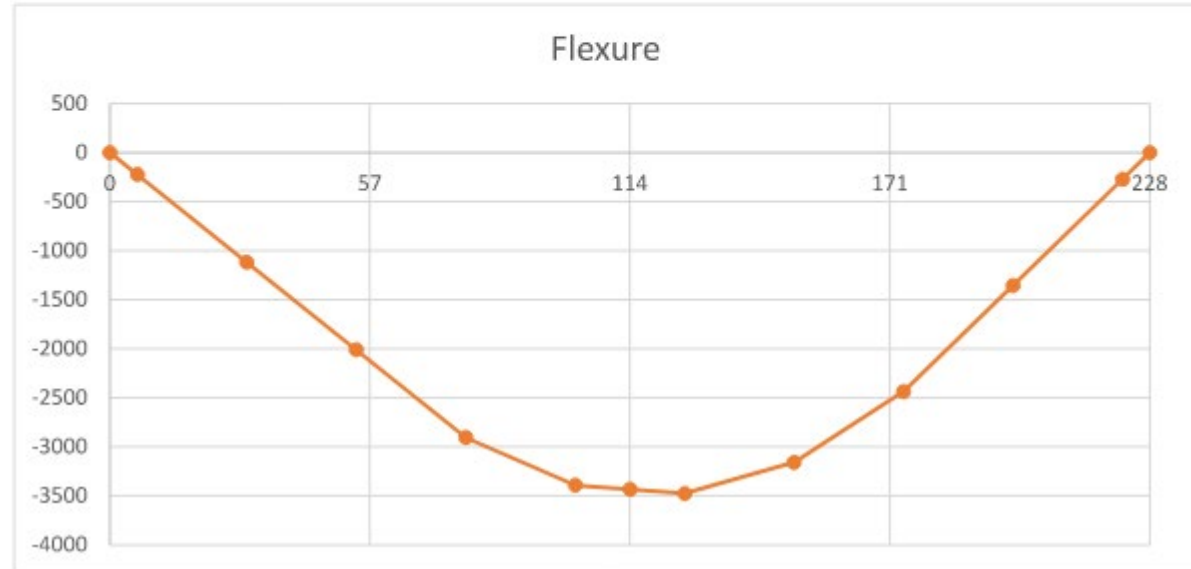
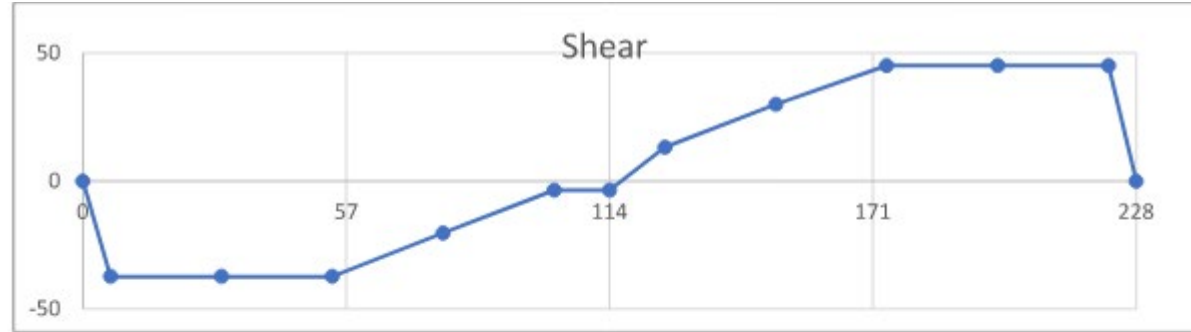


## NOTES:

## IDEALIZED LOAD DIAGRAM



$M_{mid span}$







### Test and Stage Detail

Specimen #: 20-B

Span Length: 20'-0"

Protocol: Flexure Proof Load

Stage: 9 (140% of Flexure Proof Load)

blocks: 25 blocks

Applied Weight: 82 k

Total Weight 89 k

Max Moment: 3477. k-in

Approx shear @ dv: 45.2k

$M_n = 2868$  k-in

$V_n = 53.6$  kip

$M_{proof} = 2495$  k-in

$V_{proof} = 42$  kip

### BLOCK CONFIGURATION

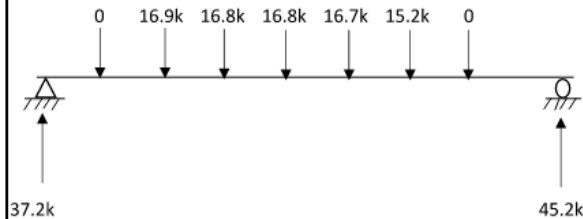
23	25	22	21	24
17	18	16	20	19
15	13	12	11	14
6	7	8	9	10
5	4	3	2	1

4'-0"

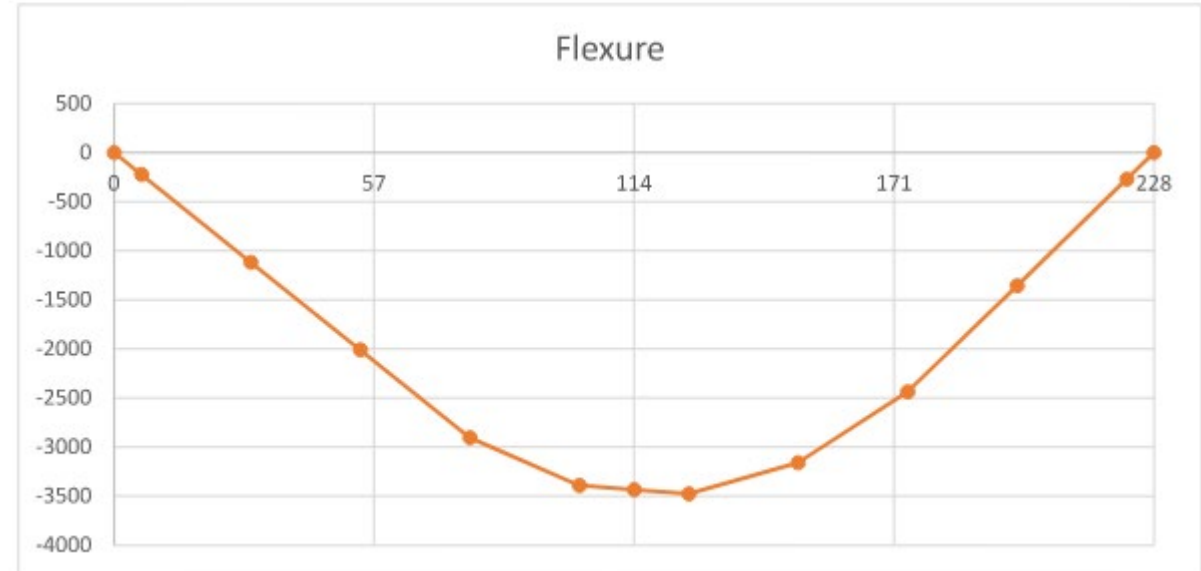
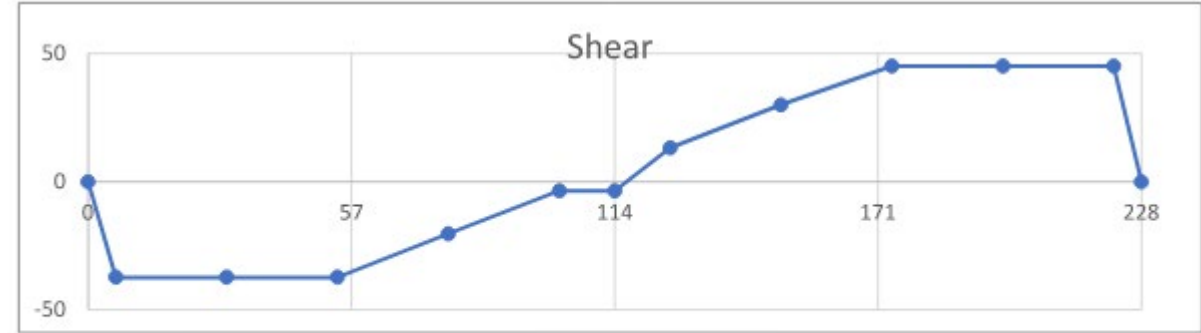
Girder

### NOTES:

### IDEALIZED LOAD DIAGRAM



$M_{mid span}$



## Test and Stage Detail

Specimen #: 20-B

Span Length: 20'-0"

Protocol: Flexure Proof Load

Stage: 9 (140% of Flexure Proof Load)

blocks: 25 blocks

Applied Weight: 82 k

Total Weight 89 k

Max Moment: 3477. k-in

Approx shear @ dv: 45.2k

$M_n = 2868$  k-in

$V_n = 53.6$  kip

$M_{proof} = 2495$  k-in

$V_{proof} = 42$  kip





### Test and Stage Detail

Specimen #: 20-B

Span Length: 20'-0"

Protocol: Flexure Proof Load

Stage: 10 (140% of Flexure Proof Load)

blocks: 30 blocks

Applied Weight: 82 k

Total Weight 89 k

Max Moment: 3610.6 k-in

Approx shear @ dv: 52.2k

$M_n = 2868$  k-in

$V_n = 53.6$  kip

$M_{proof} = 2495$  k-in

$V_{proof} = 42$  kip

### BLOCK CONFIGURATION

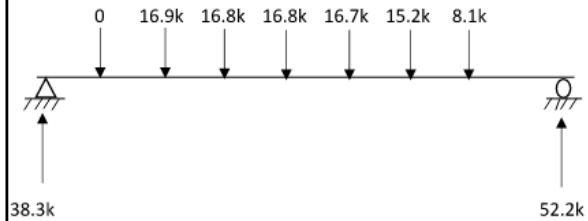
23	25	22	21	24	H
17	18	16	20	19	H
15	13	12	11	14	H
6	7	8	9	10	H
5	4	3	2	1	H

2'-0"

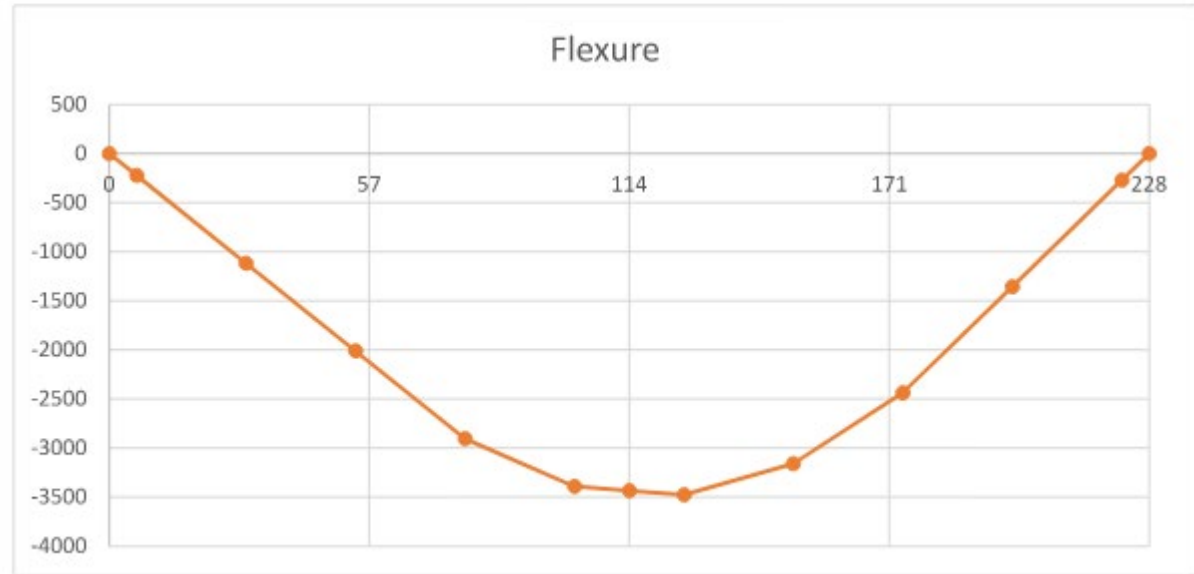
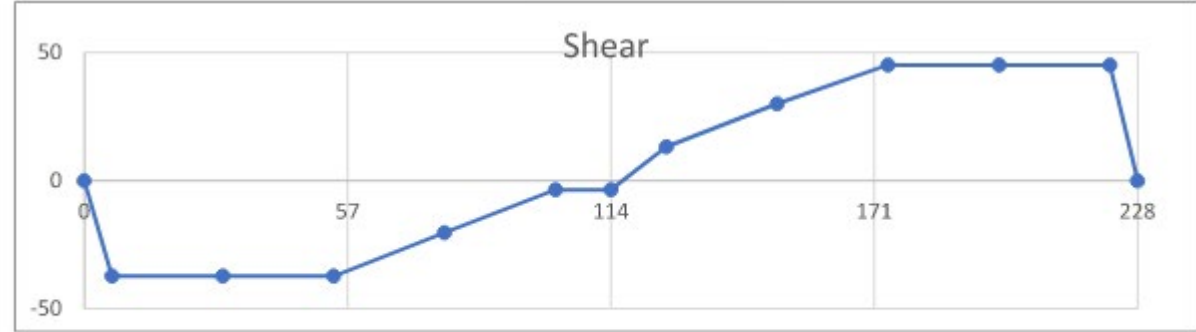
Girder

### NOTES:

### IDEALIZED LOAD DIAGRAM



$M_{mid span}$



# Test and Stage Detail

Specimen #: 20-B

Span Length: 20'-0"

Protocol: Flexure Proof Load

Stage: 10 (140% of Flexure Proof Load)

blocks: 30 blocks

Applied Weight: 82 k

Total Weight 89 k

Max Moment: 3610.6 k-in

Approx shear @ dv: 52.2k

$M_n = 2868 \text{ k-in}$

$V_n = 53.6 \text{ kip}$

$M_{proof} = 2495 \text{ k-in}$

$V_{proof} = 42 \text{ kip}$



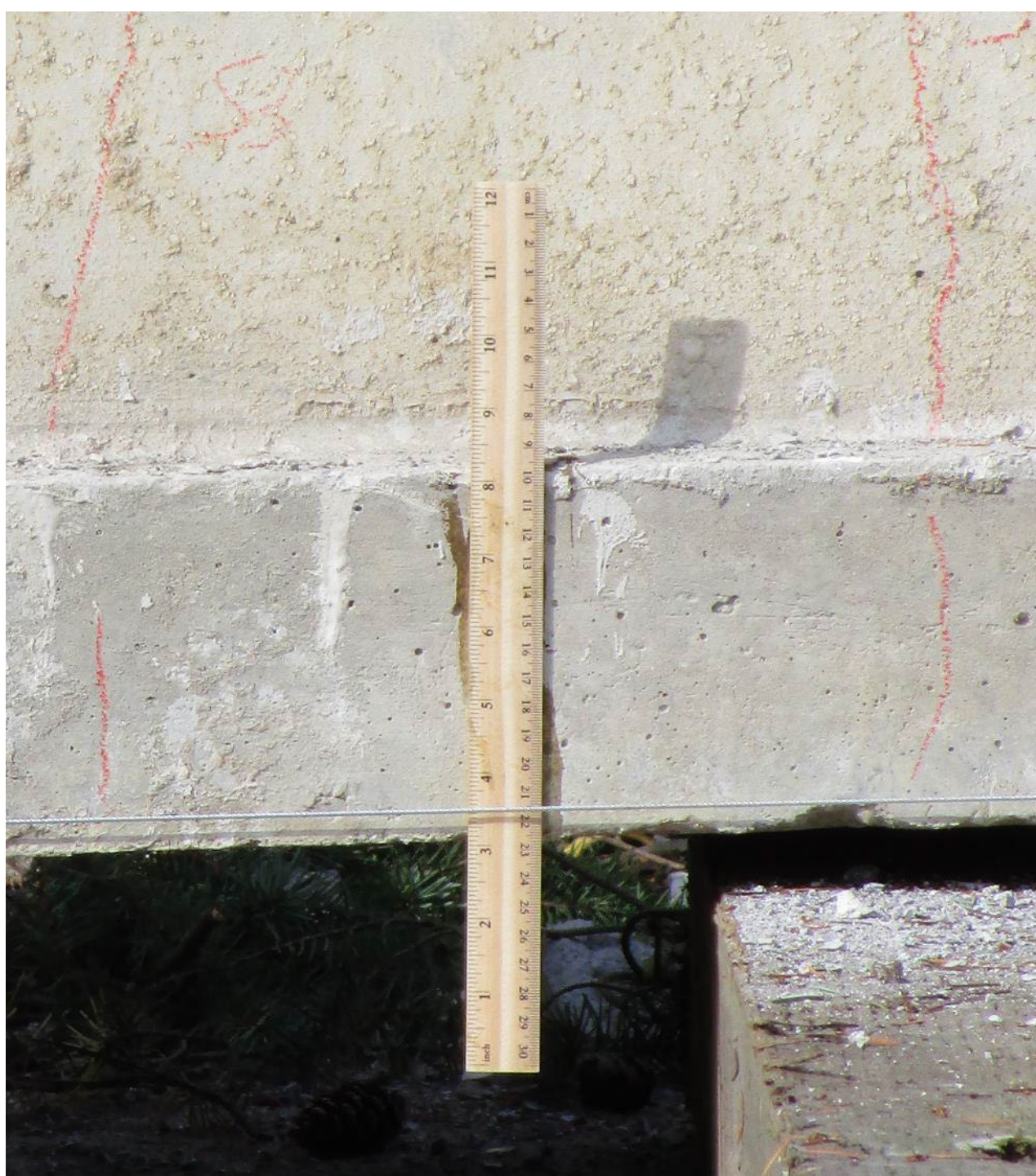
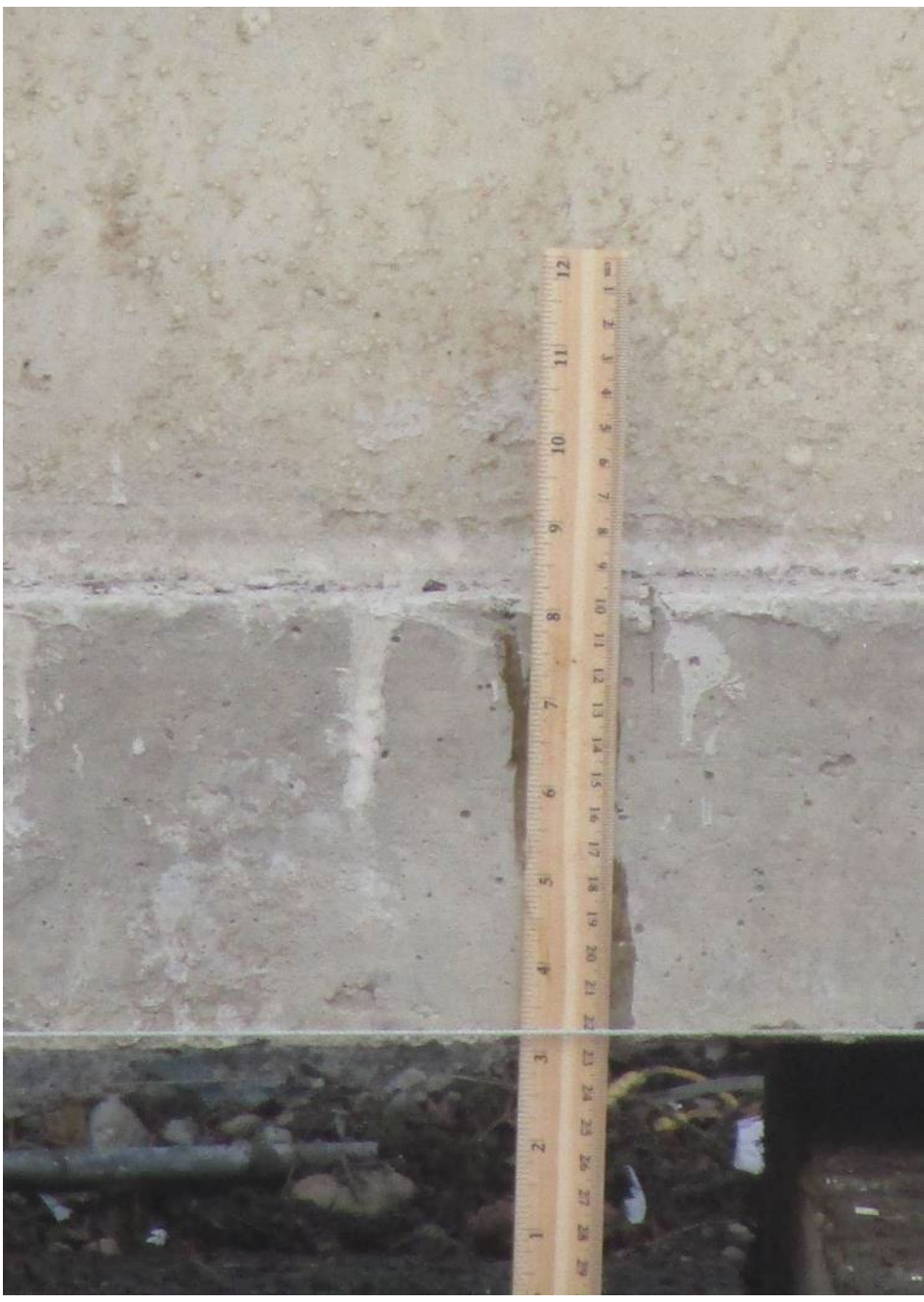


# Unloaded Specimen

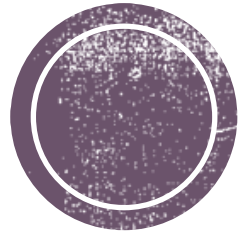
- Notes:
  - Small vertical cracks near midspan during high loads
  - Small diagonal cracks near end of applied loads
- All crack closed upon unloading.
- Minor residual deformation (within measurement precision)











# Proof Load Testing

## Analyze Results

Select a Test Method

Determine a Proof Load

Develop a Protocol

Conduct Test

Analyze Results



# Results Summary

- All 4 tests exceeded the proof load four flexure and shear
- No test resulted in a failed beam
- No test was terminated due to distress in the beam.
- The resulting load factors for the tested beams area above 1.0

Table 6 Maximum Applied Proof Loads

Test number	Girder Length	Target Proof Load	Max Applied Flexure	Max Applied Shear
#20B	20'-0"	2,495 k-in, 42 kip	3,610 k-in	52.17 k
#20D	20'-0"	2,495 k-in, 42 kip	3,528 k-in	46.25 k
#16A	15'-9"	1,694 k-in, 33 kip	2,730 k-in	43.8 k
#16B	15'-9"	1,694 k-in, 33 kip	2,765 k-in	43.2 k

Capacity and Rating

$$OP = \frac{k_o L_p}{X_{pA}} = \frac{(1.0)(52.17)}{1.61} = 32.40 \text{kip}$$

$$RF_0 = \frac{OP}{L_R(1 + IM)} = \frac{k_o L_p}{X_{pA}(1 + IM)} = \frac{32.40}{20 * (1.33)} = 1.22$$

Table 8.8.3.3.1-1—Adjustments to  $X_p$

Consideration	Adjustment
One-Lane Load Controls	+15%
Nonredundant Structure	+10%
Fracture-Critical Details Present	+10%
Bridges in Poor Condition	+10%
In-Depth Inspection Performed	-5%
Rateable, Existing $RF \geq 1.0$	-5%
$ADTT \leq 1,000$	-10%
$ADTT \leq 100$	-15%



# Short Span Channel Bridges

- Application to wider bridge inventory?
  - Channel bridges were all built within a 20 month window
  - Performance of these bridges over their lifespan has been adequate and bridges remain in fair to satisfactory condition.
- Rating factors for in-service bridges were adjusted from proof load tests based on the following factors.
  - 0.9 – proof load uncertainty factor
  - Variations in HMA overlay depth (field measured vs design)
  - Superstructure condition

Br No.	Bridge Name	Age	ADT	Percent Trucks	Span	Cond. Code
240A	Cottage Lake Creek Bridge	72	14,759	4%	20'	5
3097	Dorre Don Way Bridge	74	95	1%	20'	5
3099	Maxwell Road Bridge	72	520	0%	20'	6
228F	312 <sup>th</sup> AVE SE Bridge	73	798	2%	20'	5
249C	C.W.Neal Bridge	72	99	2%	20'	6
578A	Evans Creek	73	170	5%	20'	5
916A	Pleasant Hill Rd	72	798	2%	20'	5
333A	Bear Creek Bridge	73	8,521	7%	20'	6
480A	Bear Creek Bridge	72	2,200	4%	20'	6
249B	C W Neal Road Bridge	72	99	3%	15.75'	5
909B	Clough Creek Bridge	72	1,328	3%	15.75'	5
3030	SE 380 St Bridge	73	760	2%	15.75'	6
3060	208th Ave SE Bridge	72	150	1%	15.75'	6
593C	May Creek Bridge	72	3717	5%	15.75'	5
1086B	Coal Creek Bridge	73	459	1%	15.75'	5

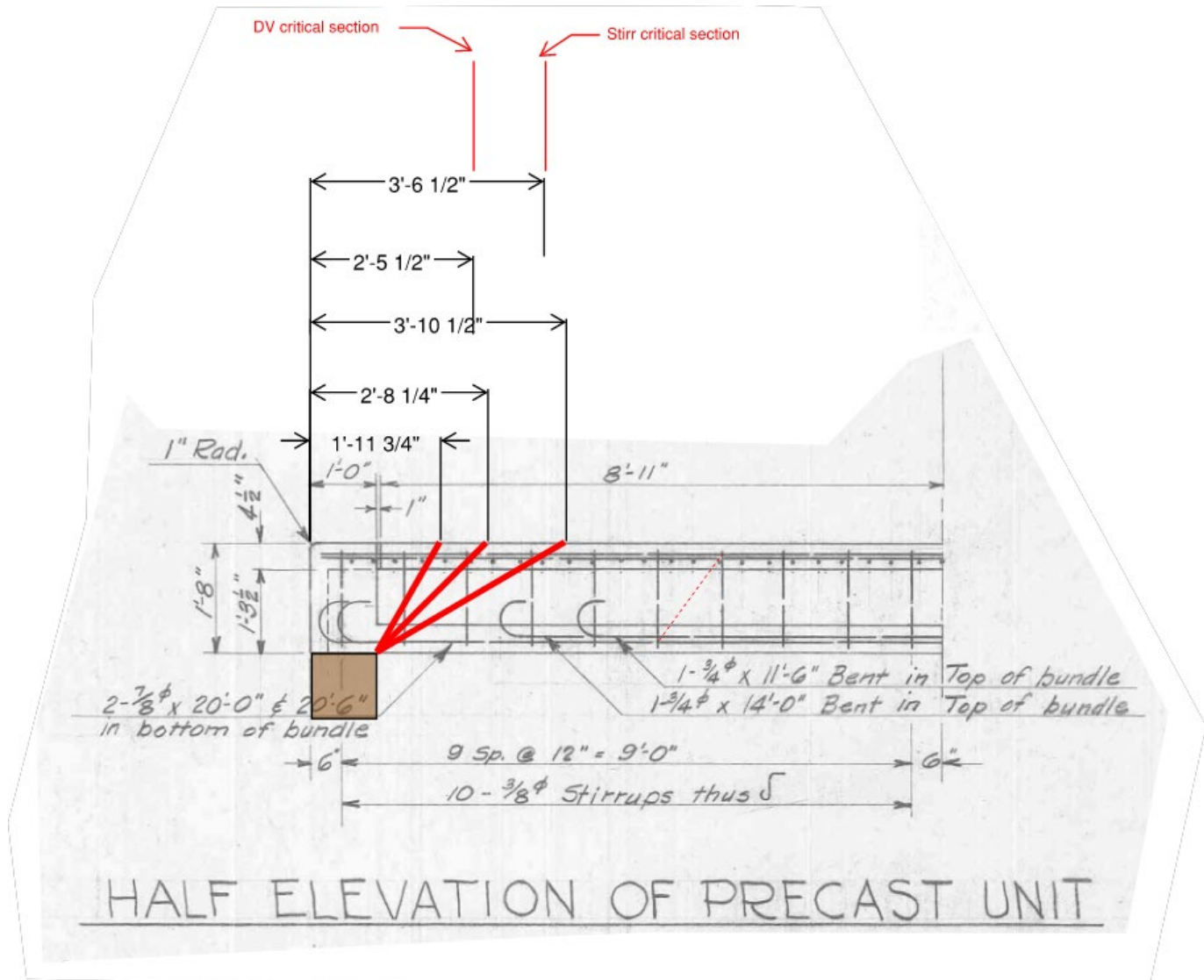


# Questions?

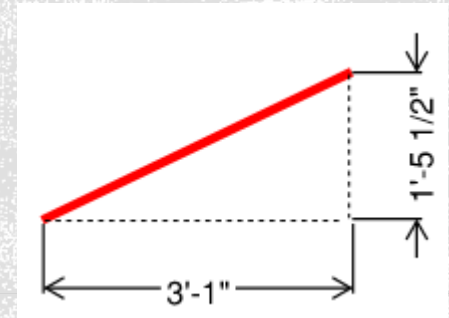
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# Why???



# Compression Strut vs Sectional Analysis

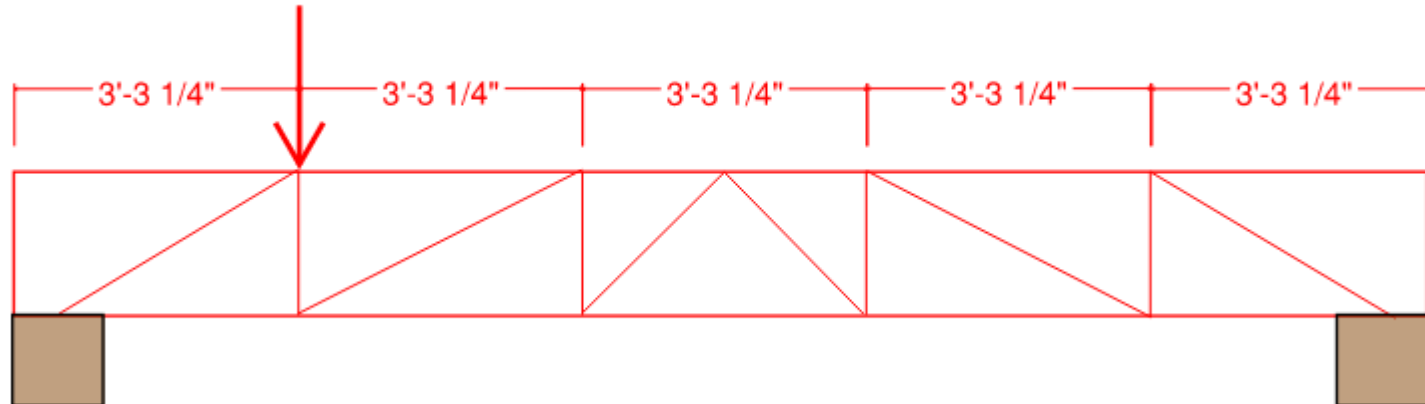


- 25 degree strut angle for STM



# Why???

## Compression Strut vs Sectional Analysis



- 25 degree strut angle for STM

