



DESIGN OPTIMIZATION FOR SOUND TRANSIT'S LIGHT RAIL LYNNWOOD EXTENSION

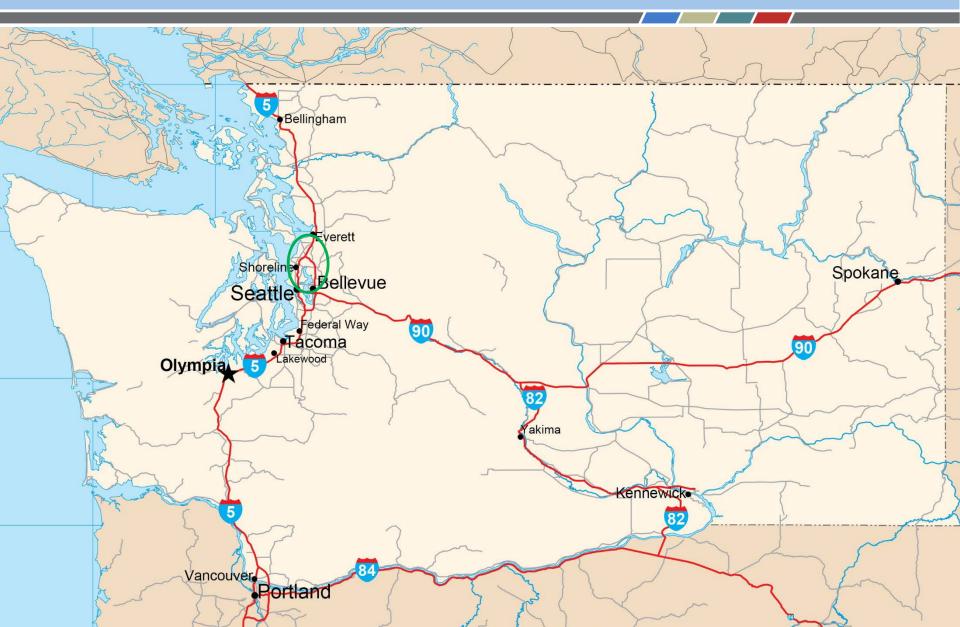
Preliminary Structural Design

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WESTERN BRIDGE ENGINEERS' SEMINAR | SEPT 2015

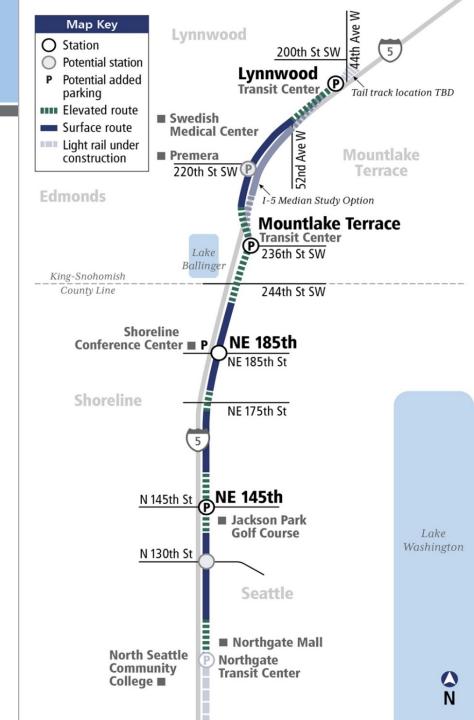


PROJECT LOCATION



SOUND TRANSIT LIGHT RAIL LYNNWOOD LINK EXTENSION

- 8.5 miles Northgate Mall to Lynnwood
- 4.1 miles Elevated guideway structure
- 4.4 miles Retaining walls
- Noise walls
- 4 Light rail stations (+2 future)
- 1 New pedestrian bridge over I-5
- 1 Bridge widening over I-5
- 1 New road bridge over LRT





NORTH CORRIDOR TRANSIT PARTNERS (NCTP)

• A Joint Venture Consultant Team:

Parametrix Parsons Brinckerhoff

• Sub-consultant firms:

Grijalva Engineering

GHL Consultants

Hewitt Architects

Paula Ito CADD Services

GeoEngineers

Bolima Drafting and Design

And more subconsultants

DESIGN OBJECTIVES

- A. Meet Sound Transit's design requirements for safety and performance
- B. Design optimization for cost-effectiveness and performance
- c. Identify and minimize potential risks
- D. Provide cost estimates that support budget and funding planning
- E. Support the final EIS studies

EVALUATION CRITERIA FOR OPTIMIZATION

Performance and ConstraintsMaintenanceDurabilityCostSpeed of ConstructionConstructabilityAestheticsConstruction ImpactsSound Transit PracticesContract Packaging

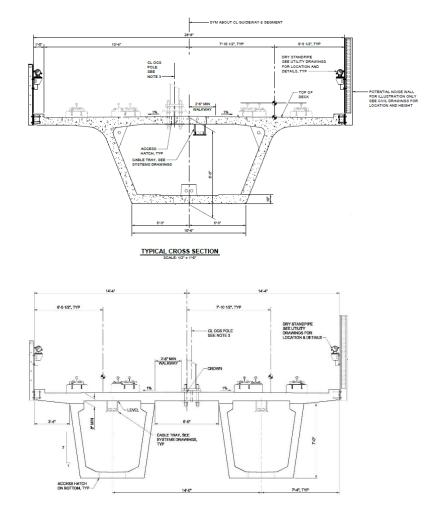
LIGHT RAIL AERIAL GUIDEWAY

- Types of superstructure/girders
- Typical girder sections
- Span lengths and layouts
- Pier shapes and sizes
- Foundations



TYPES OF SUPERSTRUCTURE / GIRDER (4.1 MILES +/-)

Segmental Box Girders



TYPICAL GUIDEWAY SECTION SCALE: 1/2" = 110"

PT Precast Tub Girders



TYPICAL SEGMENTAL BOX GIRDER SECTIONS

- Girder depth
- Deck width
- Web slant ratio
- Interface with piers
- PT layout and diaphragms
- Super-elevation



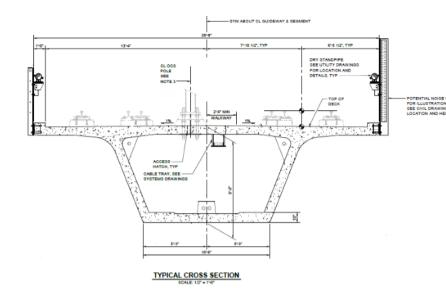
BOX GIRDER SECTION

Typical depth = 8 feet

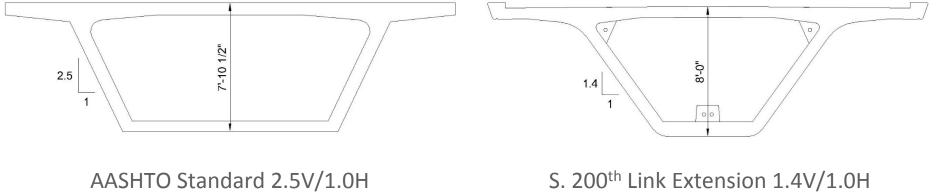
- Convenient height for maintenance works
- Suitable for desired span length
- Proportional to the deck width (twin tracks)

Deck width (Twin Tracks) = 28'- 8"

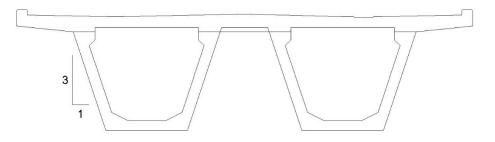
Soffit width = 10' - 6"



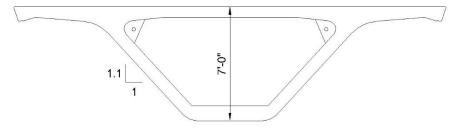
WEB SLANT RATIO (V/H)







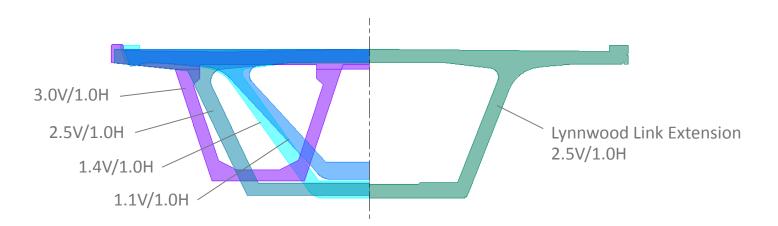
Northgate Link Extension 3.0V/1.0H



Central Link Light Rail 1.1V/1.0H

Increase V/H Ratio (more vertical):

- Increase PT force vertical components (efficient)
- Increase box torsional capacity and section modulus
- More box interior space
- Less aerodynamic transversely



WEB SLANT RATIO (V/H): VISUAL EFFECTS

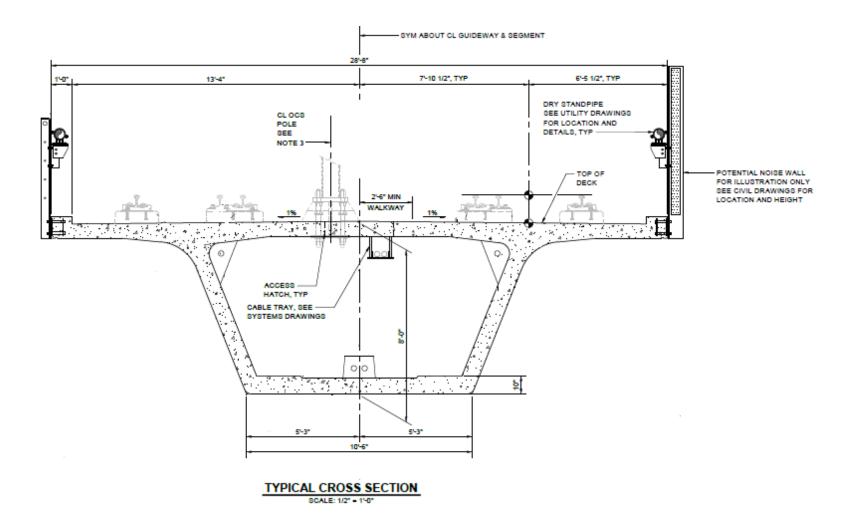


Integral with rectangular columns

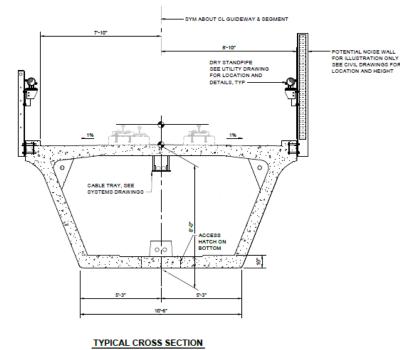


Streamline and match tub girder

TYPICAL SECTION – TWIN TRACK

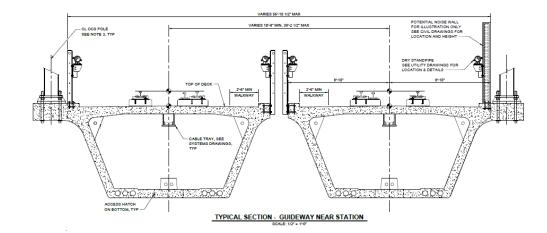


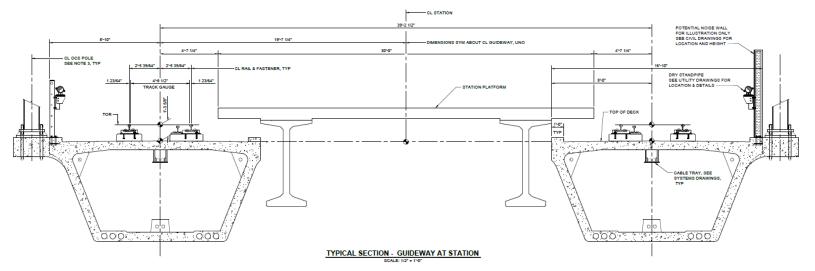
- Box section same as the twin track box
- Same section geometry
- Without deck overhangs
- Same interface with the piers



SCALE: 1/2" = 1'0"

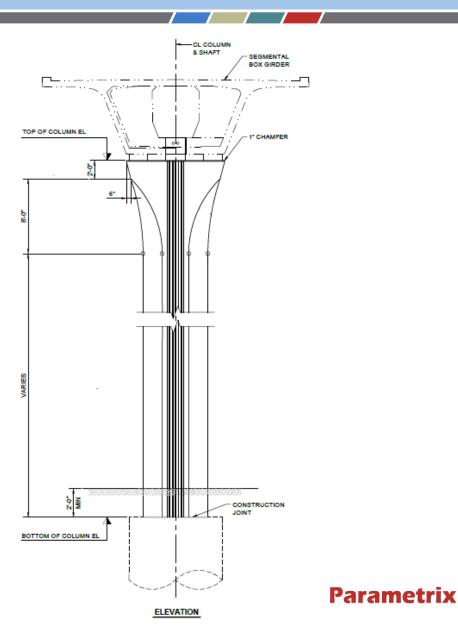
TYPICAL SECTION – SINGLE TRACK



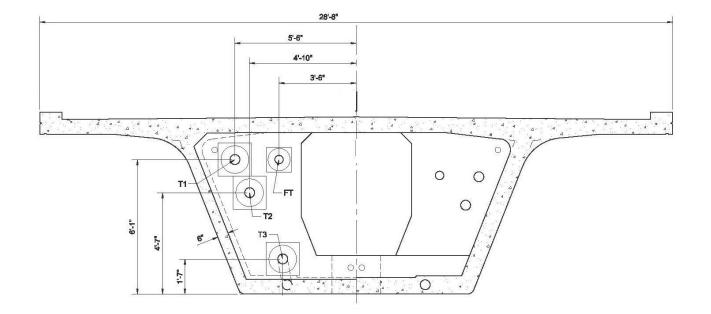


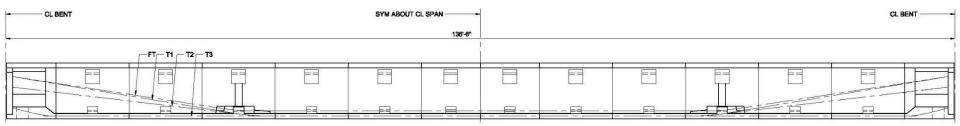
PIER INTERFACE

- No external diaphragm
- Integral
- Pin
- Movable



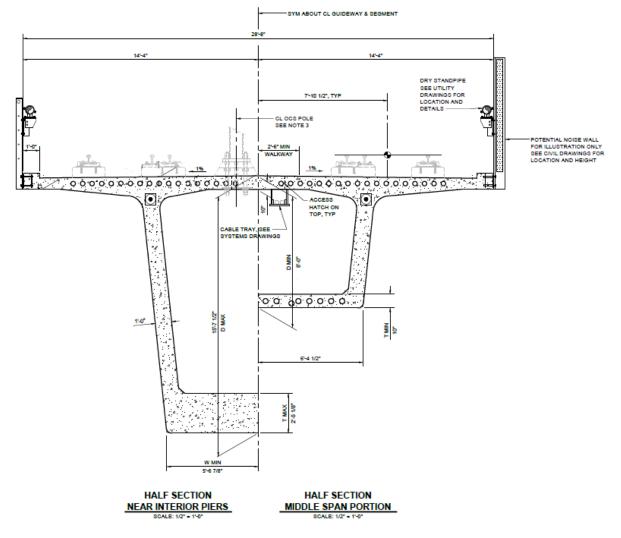
PT LAYOUT AND DIAPHRAGMS





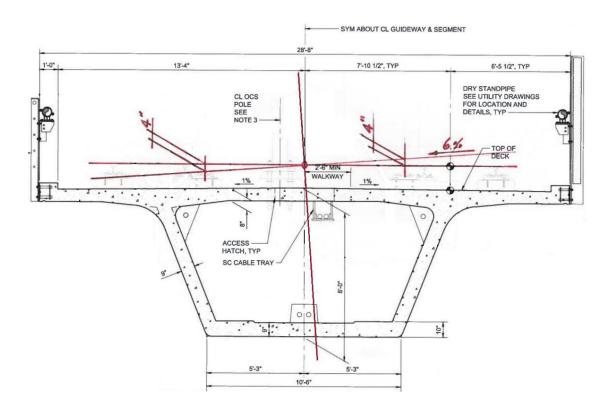
VERTICAL SECTION AT CL GUIDEWAY

VARIABLE DEPTH SECTION – LONG SPANS



SUPER-ELEVATION: ADJUST PLINTH HEIGHTS

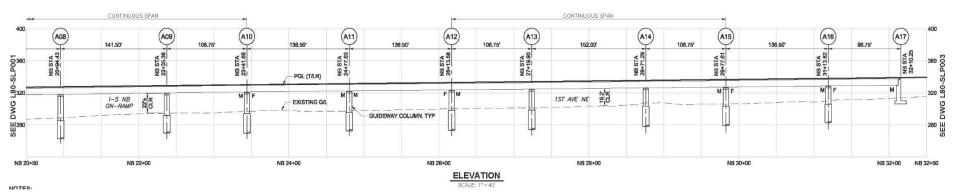
- Adjusting plinth heights instead of rotating the boxes
 - Reduce vertical ups and downs of the tracks
 - Reduce the length of vertical curves of the tracks





Approximately 4.1 miles of elevated guideway structures, Construction efficiency is important.

- Maximize the use of simply supported girders
- Double cantilever construction for long spans



MAXIMUM SPAN LENGTH

- Strength (load support capacity)
- Deflections/displacements
- Accelerations/vibrations
- Allowable rail gap length
- Construction methods



VIBRATION AND DEFLECTION

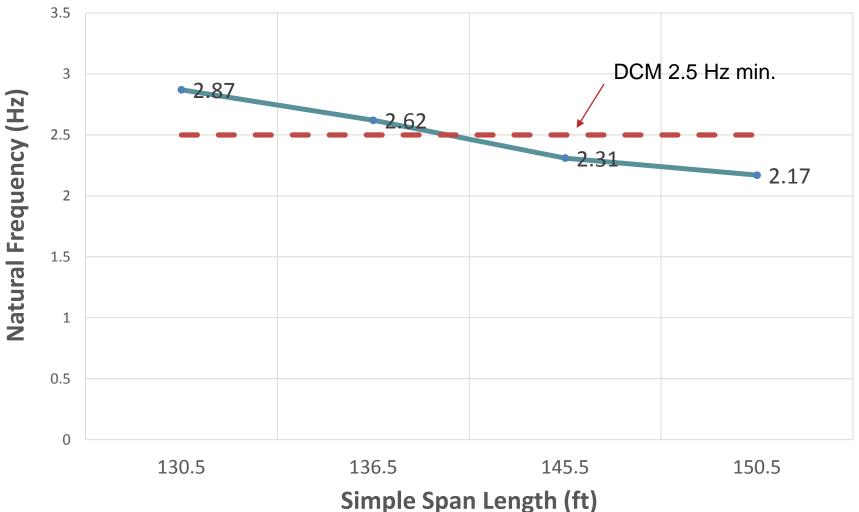
Vibration

- First mode of natural frequency
 - Simply Supported Span >= 2.5 Hz
 - Continuous Spans >= 3.0 Hz
- If frequency lower than above criteria, rail car and track interaction shall be evaluated

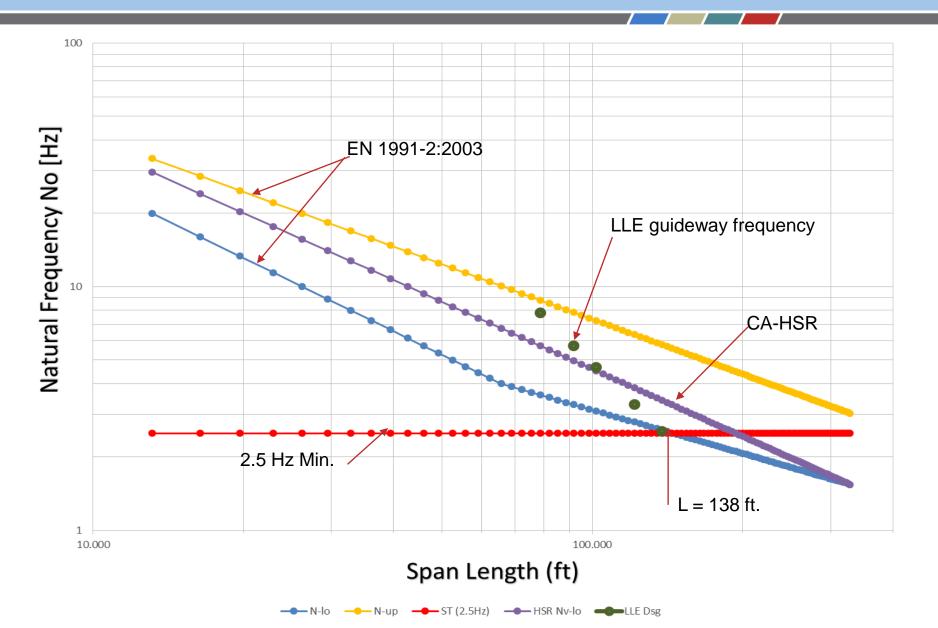
Deflection

• Deflections due to LL + Dynamic <= L/1,000

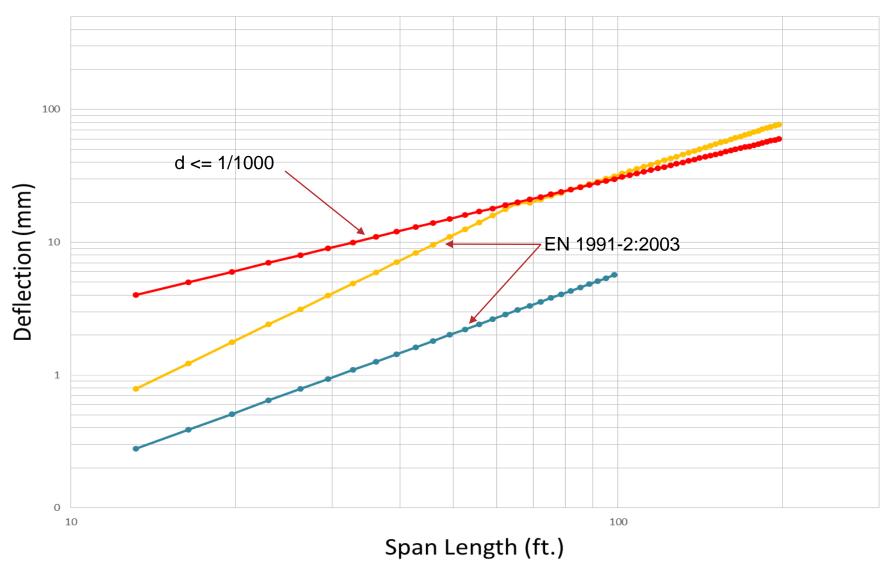
SIMPLE SPAN LENGTH (FT) VS. NATURAL FREQUENCY (Hz)



NATURAL FREQUENCY LIMITS VS. SPAN LENGTH

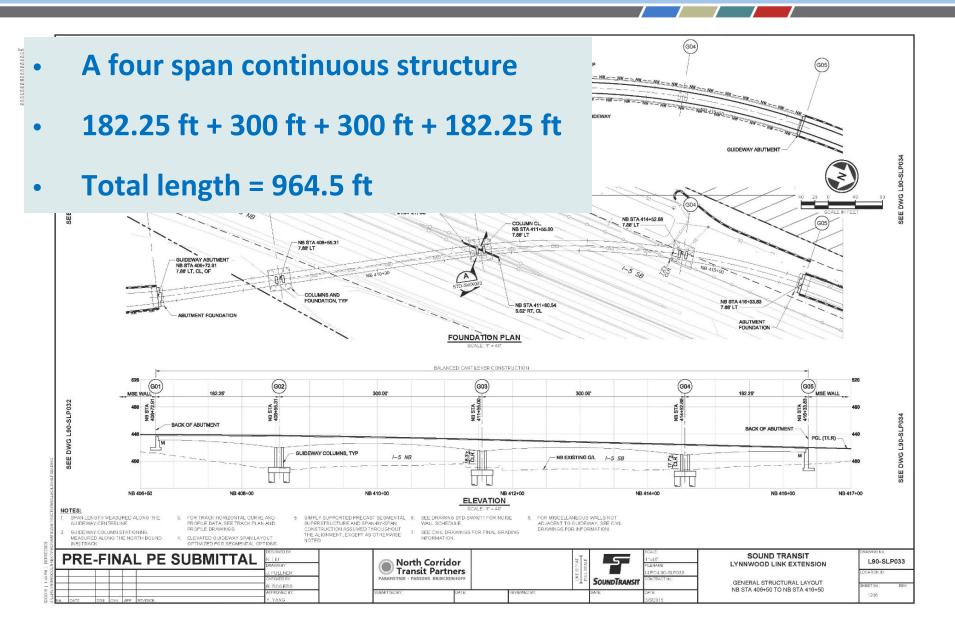


DEFLECTION LIMITS VS. SPAN LENGTH



→ d-up → d-lo → ST (L/1000)

RAIL GAP (Δ) CHALLENGE





- Sound Transit DCM: Broken rail gap <= 2 inches
- Sound Transit may approve slightly wider gaps under special conditions

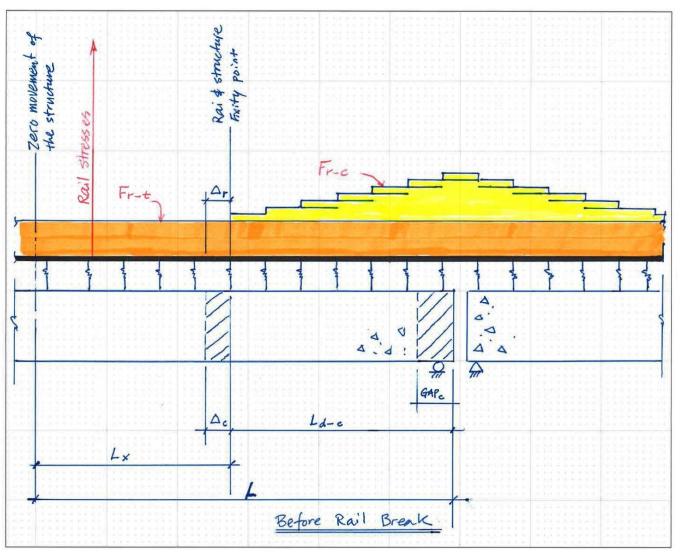


MAJOR FACTORS THAT INFLUENCE RAIL GAP

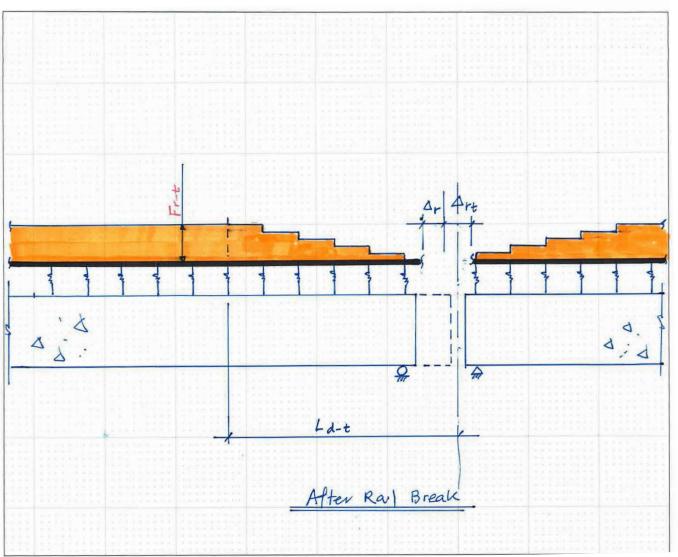
- Concrete strength (f'c)
- Young's modulus of concrete (Ec) and rail (Es)
- Temperature range (TU)
- Rail fastener friction (Ff) & spacing (Sf)
- Rail vehicle acceleration/deceleration
- Supporting structure movement (Δ)



RAIL INTERNAL STRESSES AND GAP



RAIL INTERNAL STRESSES AND GAP







• If rail breaks, at either abutment (expansion joint)

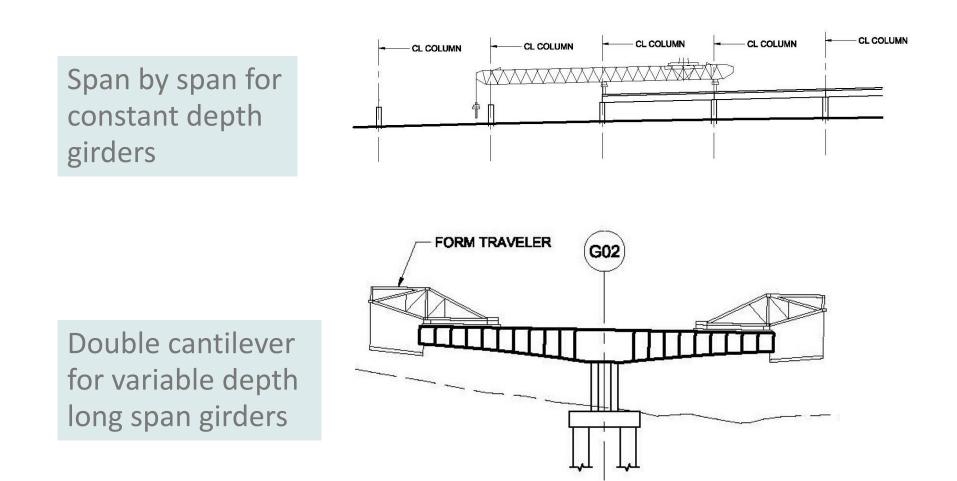
Total Δ (rail stresses, temperature, structural move, etc.)

= 2.3 inches

Accepted for this special condition (Long Span)



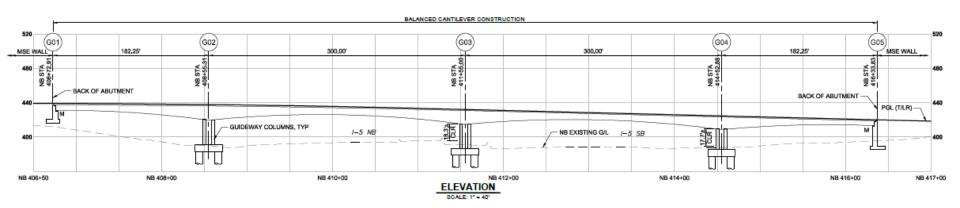
CONSTRUCTION METHODS (SUGGESTED)



MAXIMUM SPAN LENGTHS (SEGMENTAL)

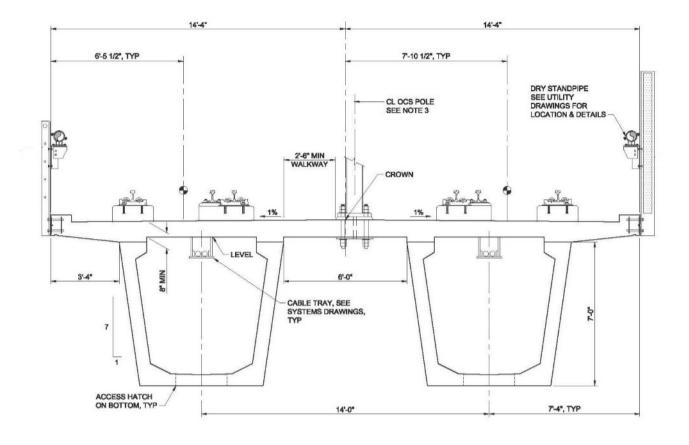
□ Constant depth girder 8 feet typical:

- Simply Supported Span, L max = 137 feet +/-
- Continuous Interior Span, L max = 150 feet +/-
- □ Long spans with viable depth girders:
 - L max = 300 feet



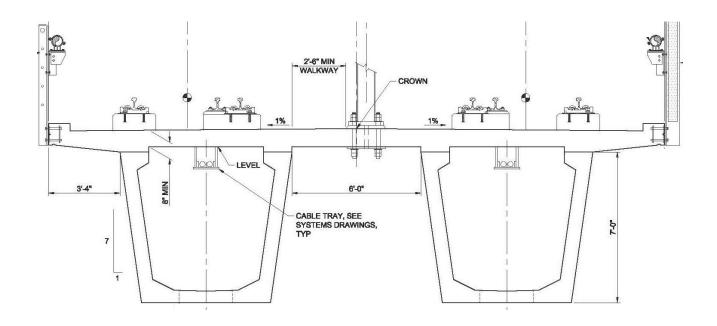


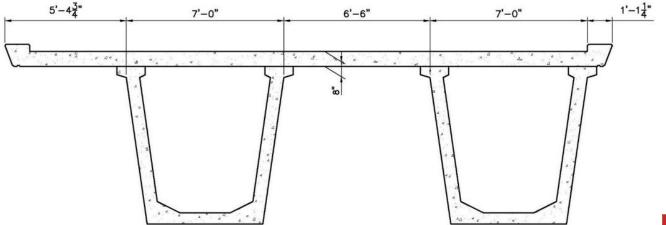
PT TUB GIRDERS – STRUCTURAL ALTERNATIVE



SCALE: 1/2" = 1'-0"

PT TUB GIRDERS – CURVE AFFECTS SPAN LENGTH





Deck Eccentricity on Curved Alignment

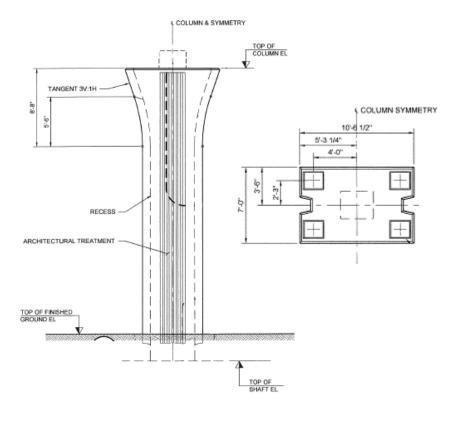
Span	Radius (ft.)										
(ft.)	500	600	700	800	900	1000	1085	1200	1500	1950	2500
		e (in.) - Eccentricity due to Curve									
60	10.80	9.00	7.71	6.75	6.00	5.40	4.98	4.50	3.60	2.77	2.16
70	14.69	12.25	10.50	9.19	8.17	7.35	6.77	6.12	4.90	3.77	2.94
80	19.19	15.99	13.71	12.00	10.66	9.60	8.85	8.00	6.40	4.92	3.84
90	24.28	20.24	17.35	15.18	13.50	12.15	11.20	10.12	8.10	6.23	4.86
100	29.98	24.99	21.42	18.74	16.66	15.00	13.82	12.50	10.00	7.69	6.00
110	36.26	30.23	25.92	22.68	20.16	18.15	16.72	15.12	12.10	9.31	7.26
120	43.15	35.97	30.84	26.99	23.99	21.59	19.90	18.00	14.40	11.08	8.64
130	50.63	42.21	36.19	31.67	28.15	25.34	23.36	21.12	16.90	13.00	10.14
136.5	55.81	46.53	39.89	34.91	31.04	27.94	25.75	23.28	18.63	14.33	11.18
140	58.70	48.94	41.97	36.73	32.65	29.39	27.09	24.49	19.60	15.08	11.76
145	62.96	52.50	45.01	39.39	35.02	31.52	29.06	26.27	21.02	16.17	12.61
150	67.37	56.18	48.17	42.16	37.48	33.73	31.09	28.12	22.50	17.31	13.50

LIGHT RAIL AERIAL GUIDEWAY

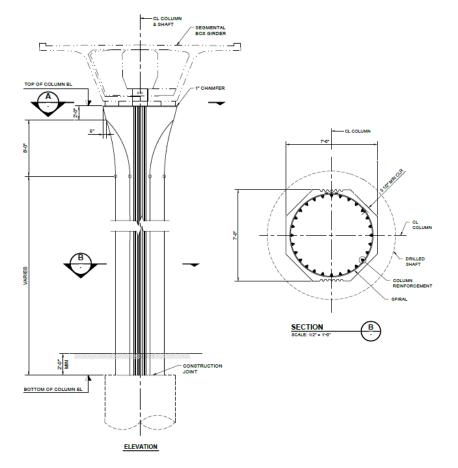
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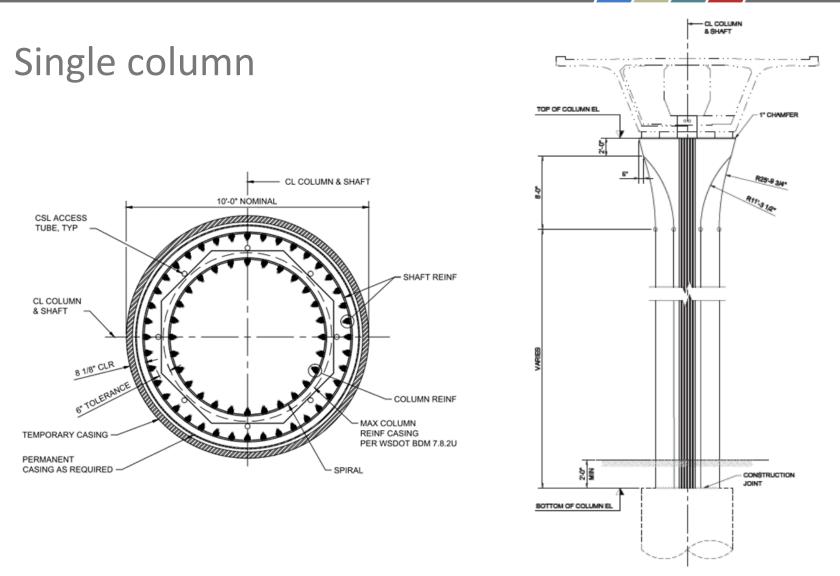


Rectangular columns vs. Circular columns



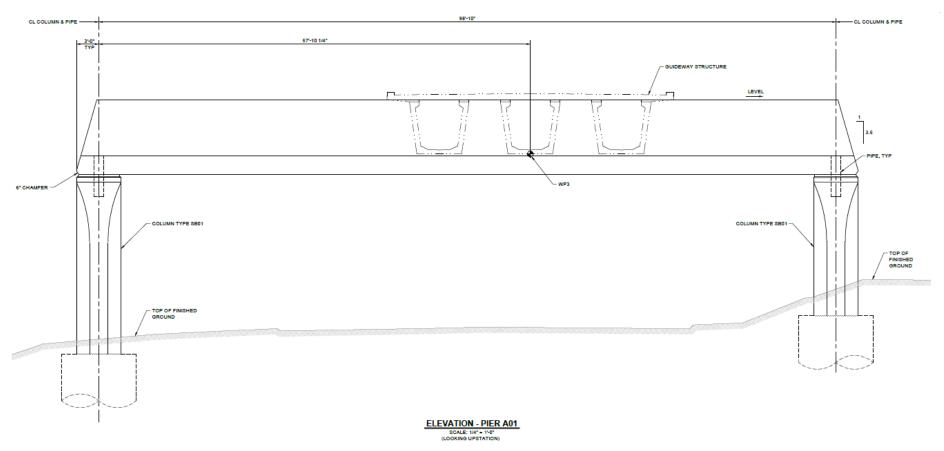
SCALE: 1/4" = 1'-0"





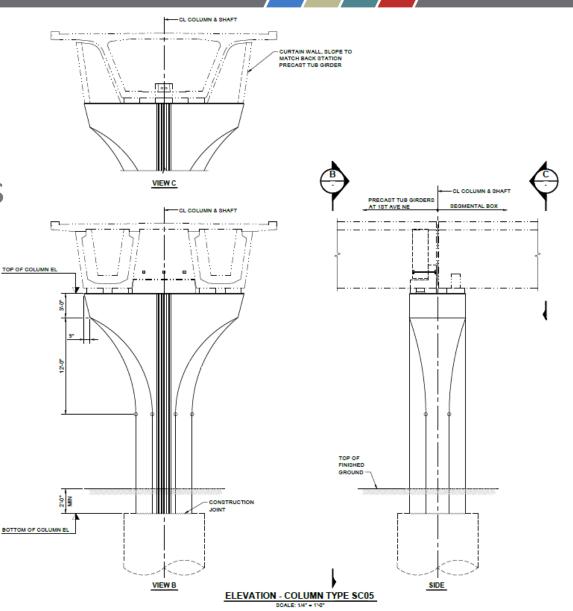
ELEVATION

Straddle bents



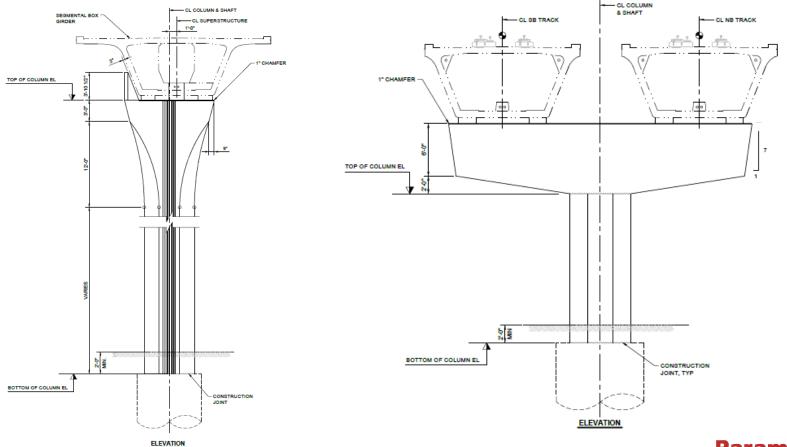
Support:

- CIP box girders
- Twin tub girders



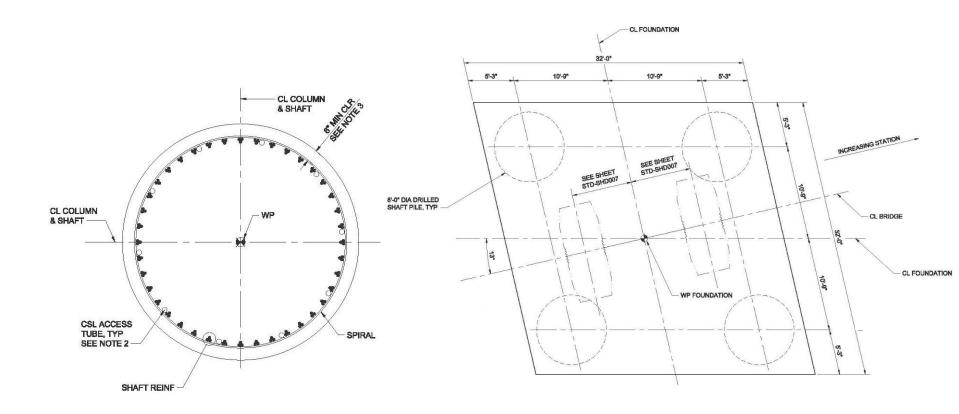
Offset

Hammerhead

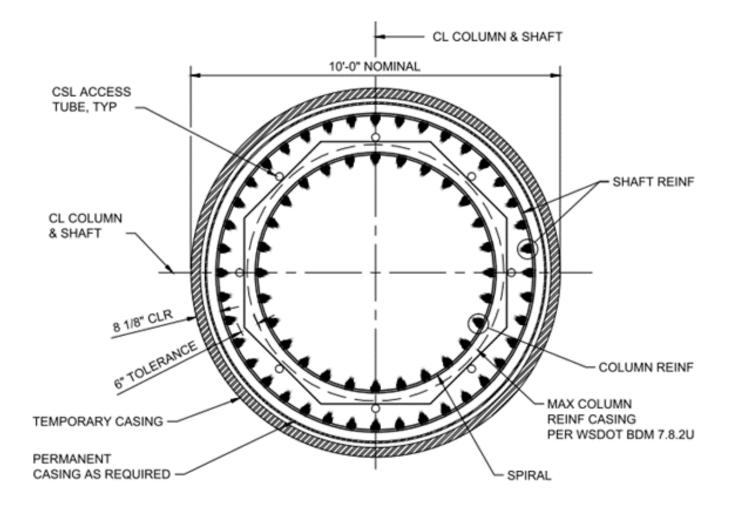


FOUNDATIONS

Single shaft Pile/shaft group



SHAFT VS. COLUMN SIZES



SHAFT VS. COLUMN SIZES

- WSDOT BDM Section 7.8.2
- WSDOT Standard Specifications, Section 6-19

	Colu	umn		Shaft					
Nominal Dia	Max. Dia.	Cover	Max. Cage Dia	Nominal Shaft Dia	Metric Casing Dia	Max (Outside) Reinf Dia		Rebar	
ft.	ft.	in.	in.	ft.	ft.	in.	in.	in.	
4.00	4.05	2.0	44.58	6.0	6.560	64.02	6.0	3.72	
4.00	4.05	2.0	44.58	6.5	6.560	64.02	6.0	3.72	Note (1)
4.50	4.70	2.0	52.45	7.0	7.220	71.89	6.0	3.72	
5.50	5.59	2.0	63.10	8.0	8.200	83.70	6.0	4.30	
6.50	6.58	2.0	74.91	9.0	9.190	95.51	6.0	4.30	
7.00	7.10	2.0	81.208	10.0	9.840	101.81	6.0	4.30	Note (2)
8.00	8.51	2.0	98.11	11.0	11.250	118.71	6.0	4.30	
9.00	9.49	2.0	109.92	12.0	12.240	130.52	6.0	4.30	
Note (1)	Assume up to three #11 mian reinforcing bar each bundle								
Note (2)	Assume up to three #14 mian reinforcing bar each bundle Parametr								

SEISMIC DESIGN – TWO-LEVEL EARTHQUAKE HAZARD DESIGN

Design Life = 100 years

Operating Design Earthquake (ODE):

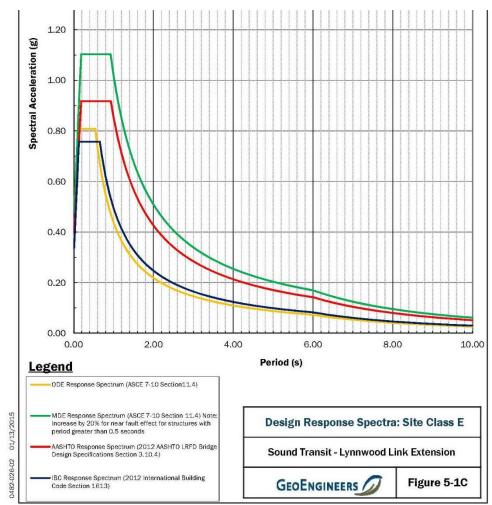
- Return period 150 years
- 50% probability of exceedance

Maximum Design Earthquake (MDE):

- Return period 2,500 years
- 4% probability of exceedance

Compare to **AASHTO** single level design:

- Return period 1,000 years
- 9.5% probability of exceedance



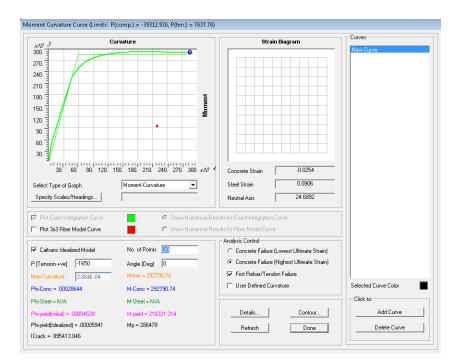
SEISMIC DESIGN – PERFORMANCE AND RISK ACCEPTANCE

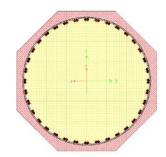
Operating Design Earthquake (ODE):

- Without significant structural damage
- Can be repaired during normal operating hours

Maximum Design Earthquake (MDE):

- To avoid major failure and prevent collapse
- To maintain life safety







OPERATING DESIGN EARTHQUAKE

- Earthquake event with a 150 year return period
- Force based design per AASHTO LRFD Bridge Design Specifications
- Response modification factor = 1.0 per Sound Transit DCM

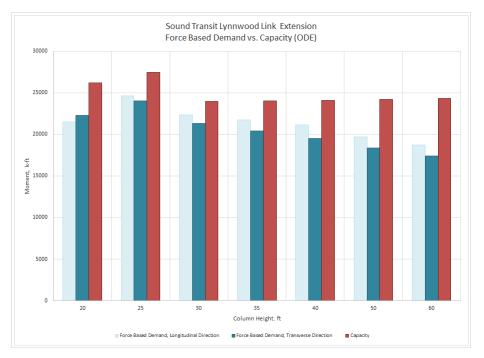


Table 8A-3 Response Modification Factors

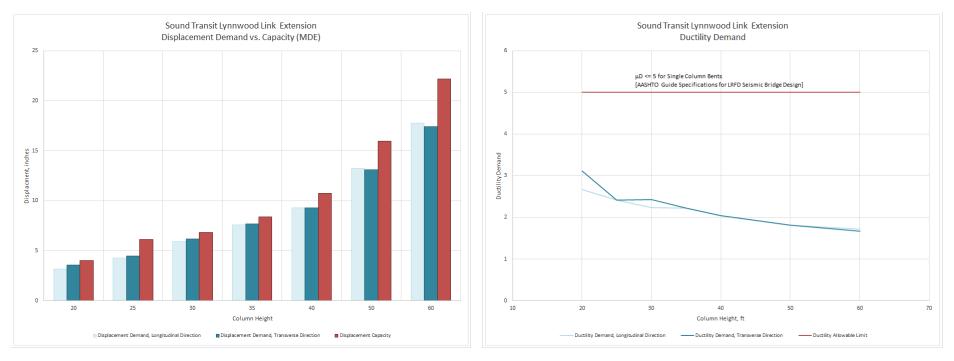
Substructure	ODE ³ (150 year)
Wall-type pier ¹	1.0
Reinforced concrete pile bents	
a. Vertical piles only	1.0
b. One or more batter piles	1.0
Single Columns (reinforced concrete)	1.0
Steel or composite steel and concrete pile bents	
a. Vertical piles only	1.0
b. One or more batter piles	1.0
Multiple column bent (reinforced concrete)	1.0

Connections ²	ODE (150 year)
Superstructure to Abutments ² Expansion joints within a span of the superstructure	1.0 1.0
Columns, piers or pile bents to cap-beam or Superstructure Columns or piers to foundations ³	1.0 1.0

[Sound Transit DCM]

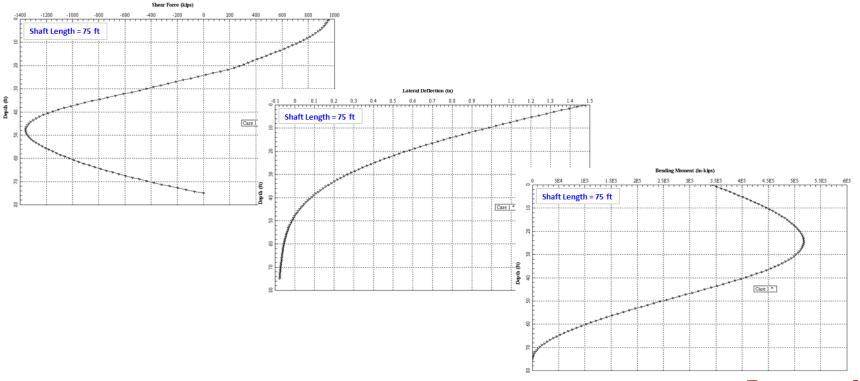
MAXIMUM DESIGN EARTHQUAKE

- Earthquake event with a 2,500 year return period
- Displacement based design per AASHTO Guide Specifications for LRFD Seismic Bridge Design
- P- Δ checked separately per Article 4.11.5 of the Guide Specifications



LATERAL DESIGN OF SHAFTS

- Typical shaft diameter = 10 feet
- Shaft length = 60-75 feet (avg.) / 100 feet (max.)
- Designed for over-strength plastic moment and shear at base of column

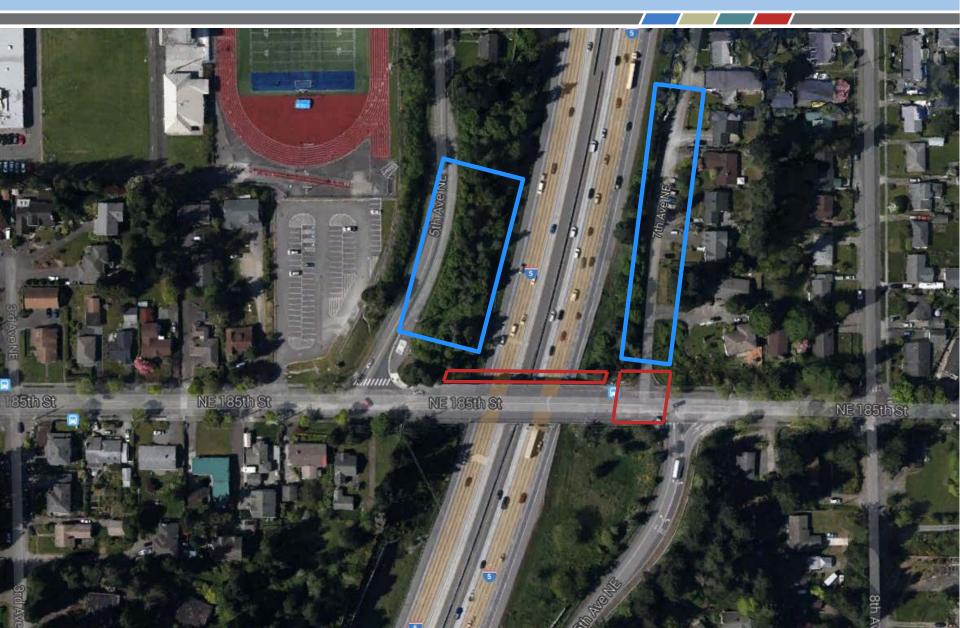


ROADWAY BRIDGES

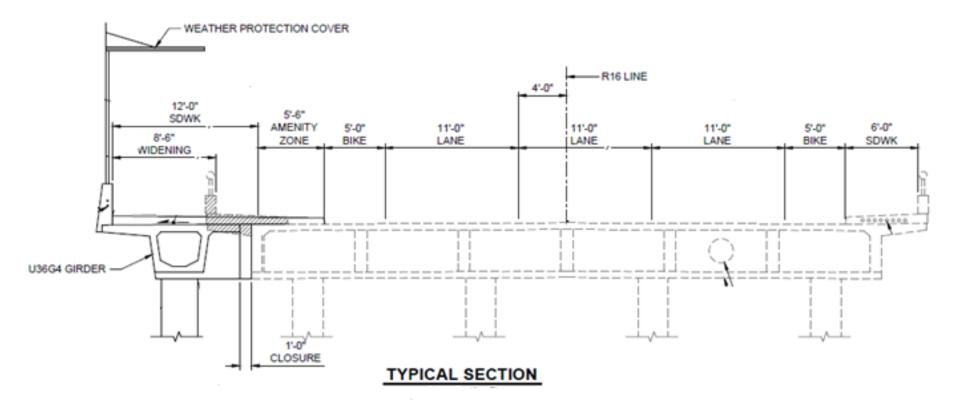
- Widening NE 185th Street Bridge over I-5
- New NE 185th Street Bridge over light rail lines
- Replacing NE 195th Street Pedestrian Bridge over I-5



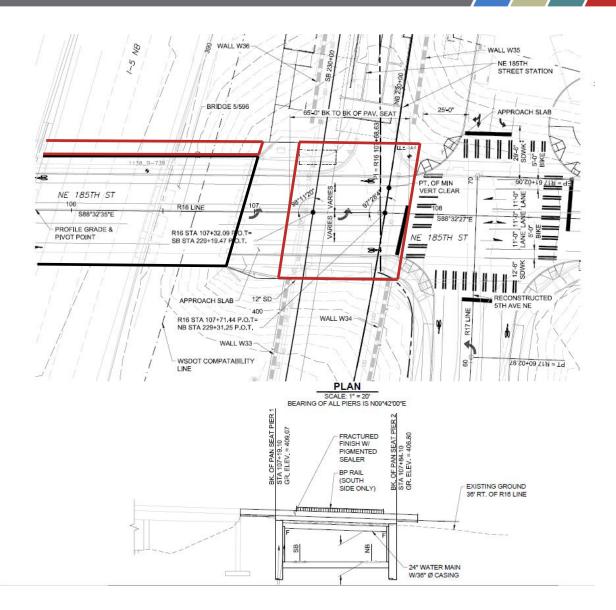
NE 185TH STREET BRIDGES



NE 185TH STREET WIDENING – CROSS SECTION

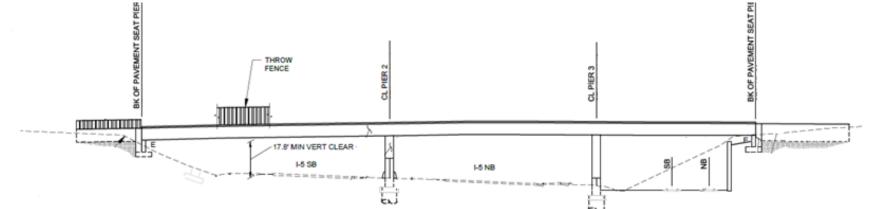


NE 185TH STREET LRT UNDERCROSSING



NE 195TH PEDESTRIAN BRIDGE – ELEVATION









Thank you for your time **QUESTIONS?**

Contact Information:

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WESTERN BRIDGE ENGINEERS' SEMINAR | SEPT 2015

