



Gusset Plate Triage Analysis For Steel Truss Bridges in Washington

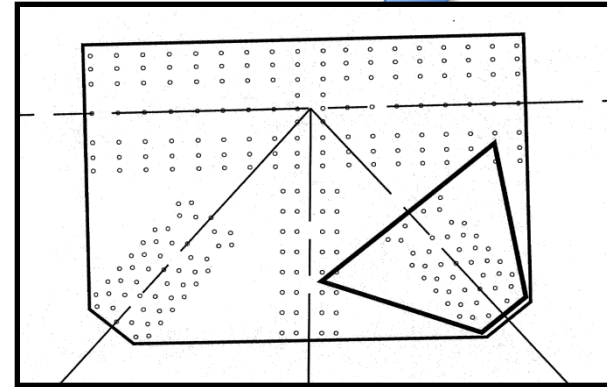
Patrick Gallagher, PE
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Olympia, Washington

2013 Western Bridge Engineer's Seminar
Bellevue, Washington

OUTLINE



- Why?
- Bridge Inventory
- Triage Method
- Triage Example
- Application
- What's Next



THE MOTIVATION

- Load Rating is a bit of a reaction based program.
 - An engineer is always allowed to check areas of concern. However, tradition and lack of concern has left gusset plates off of the usual list of items to check.
- Minneapolis, 2009 demonstrated a need to analyze quickly a lot of trusses quickly.



WSDOT'S TRUSS INVENTORY

- 130+ steel trusses owned by WSDOT
 - A total of 27.6 miles of truss on WSDOT's system, and local agencies have more.
 - Sizes range from the very small to the very large.
 - Types range from simple to very complex.
 - Simple span, continuous, drop spans, erection stresses built in.
 - Not every bridge has good plans.
- Modeling
 - Boundary Conditions
 - Global and Local
 - Lane Configuration
- This is a daunting task to evaluate!



THE TRIAGE PLAN

- Identify if a gusset will control a rating.
 - Other methods are available, FHWY, finite element, compare to the current AASHTO Design Code.
- Almost every bridge is deemed okay with the triage method and the rating is not governed by the gussets. We need to identify which ones are not okay, and fast!



SIEVE ANALOGY

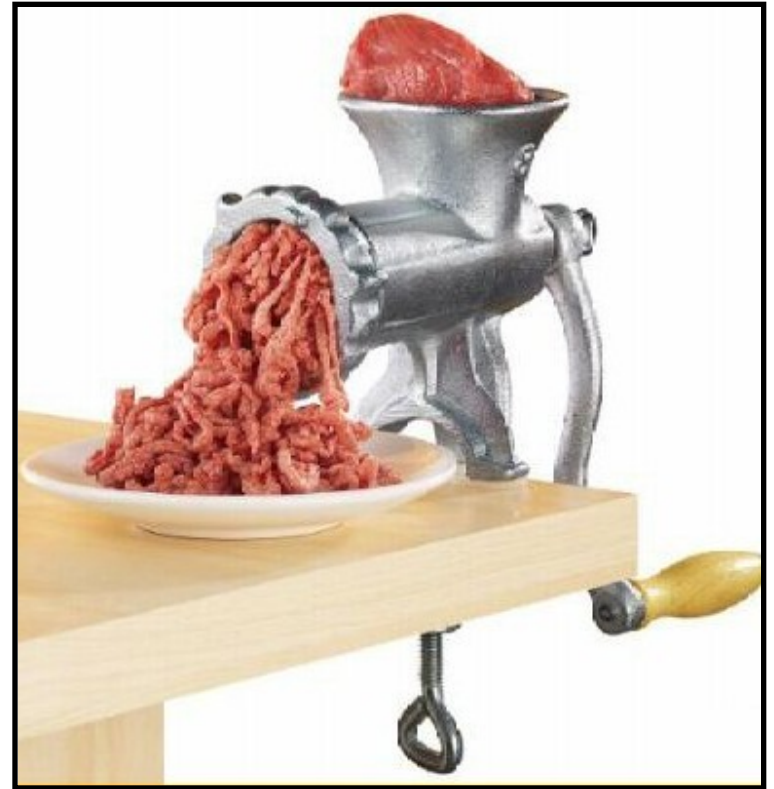
- SIEVE 1:
 - With the Triage Method, if the Rating Factors are higher than those currently listed, then the analysis is done.
- SIEVE 2:
 - If the gusset ratings are lower than those currently listed, then the FHWA Method is used.
- SIEVE 3:
 - If RFs are still very low, more detailed analysis tools could be utilized.
- SIEVE 4:
 - If more detailed analysis yields low RFs, then the low RFs are used for rating the bridge.

Most bridges are deemed okay within “Sieve 1.” This takes minimal analysis effort.



DEVELOPMENT OF TRIAGE METHOD

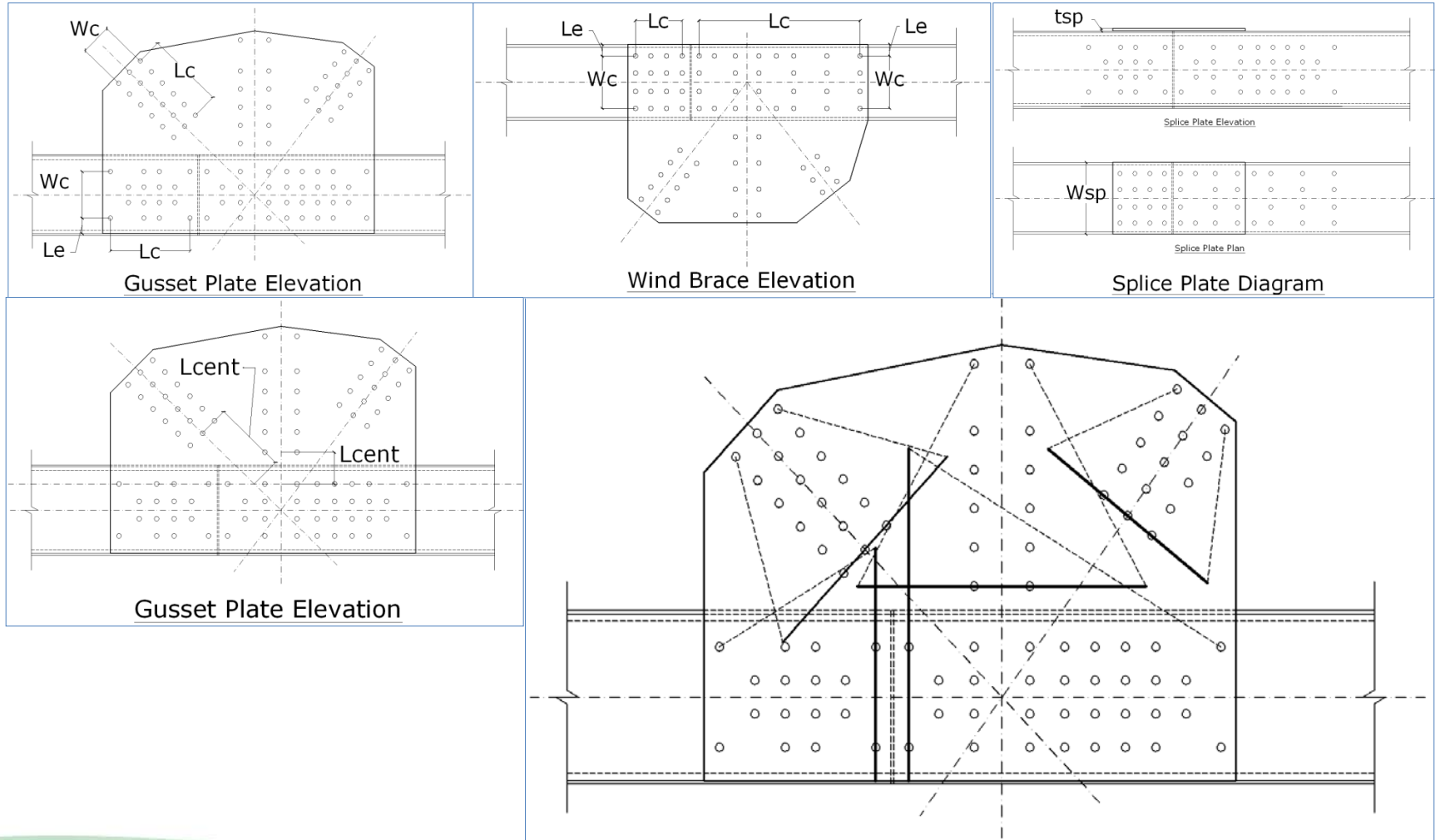
- UW Research
- BPO Involvement
- Standardizing calcs is critical. With so many engineers to do the work, and so few to review, and so few to maintain the load ratings, uniformity is key.



THE TRIAGE METHOD

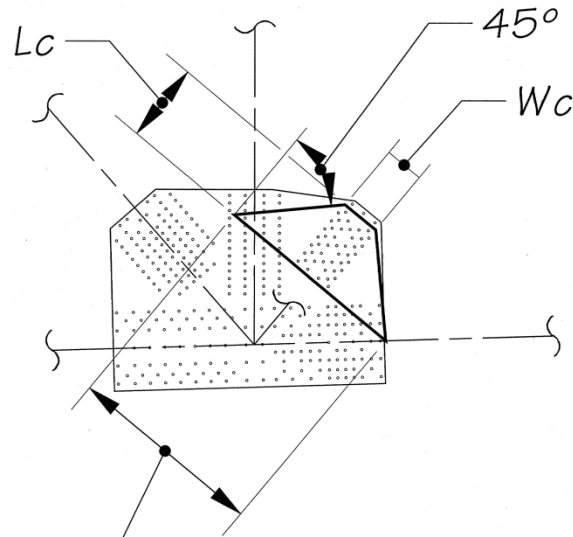
- Three failure modes considered:
 - Gusset Yielding
 - Gusset Buckling ~ Compression Members Only
 - Rivet Shear
- If the connection is milled to bear, compression on both sides, no evaluation necessary. Tension against Milled to bear requires an evaluation.
- All plates crossing a joint are considered
 - Gussets, Wind Plates, Splice Plates
- Stress reversals require a separate evaluation for each direction.
 - Stress reversal = $2.17 \text{ LL} > 1.3 \text{ DL}$

THE TRIAGE METHOD

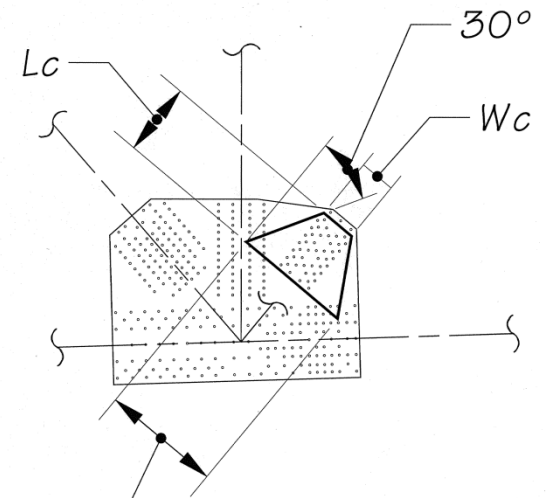


LENGTHS USED FOR AREA CALCS

THE TRIAGE METHOD



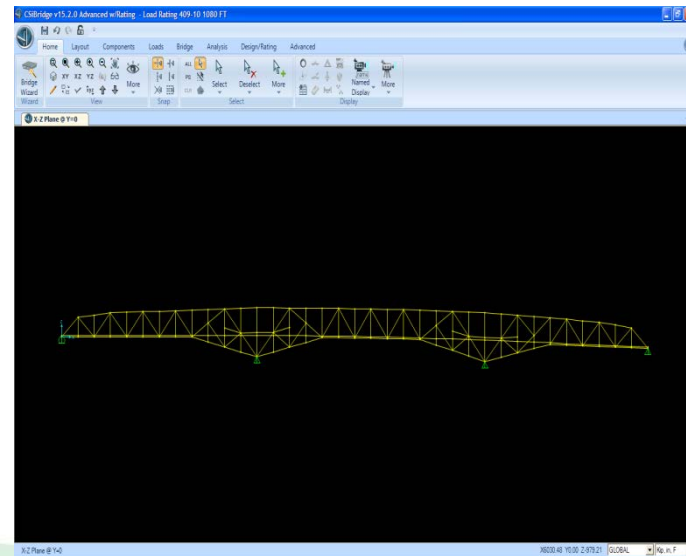
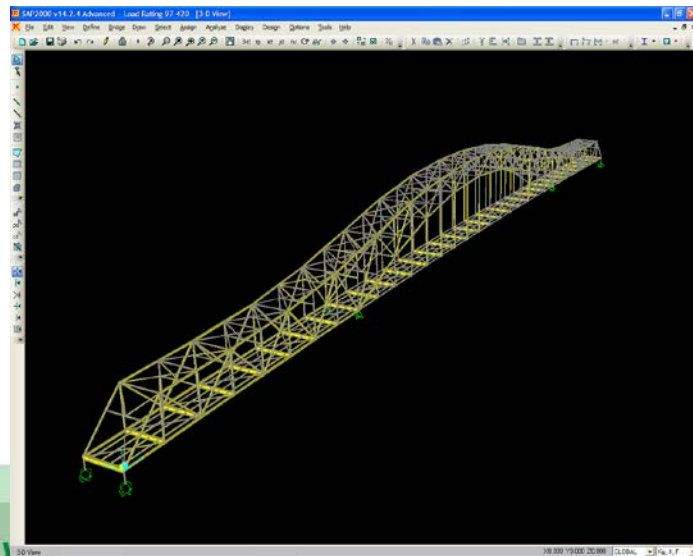
LENGTH USED TO
DETERMINE PLATE
AREA BUCKLING



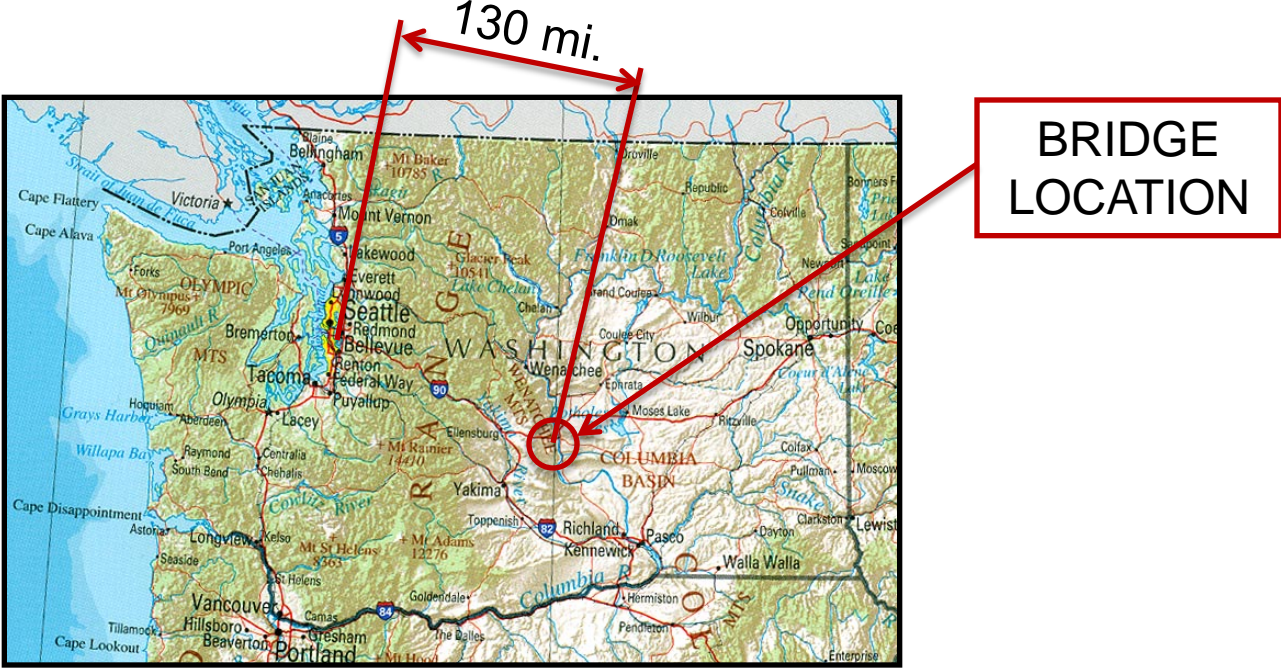
LENGTH USED TO
DETERMINE PLATE
AREA FOR YEILDING

MODELING ~ METHODS

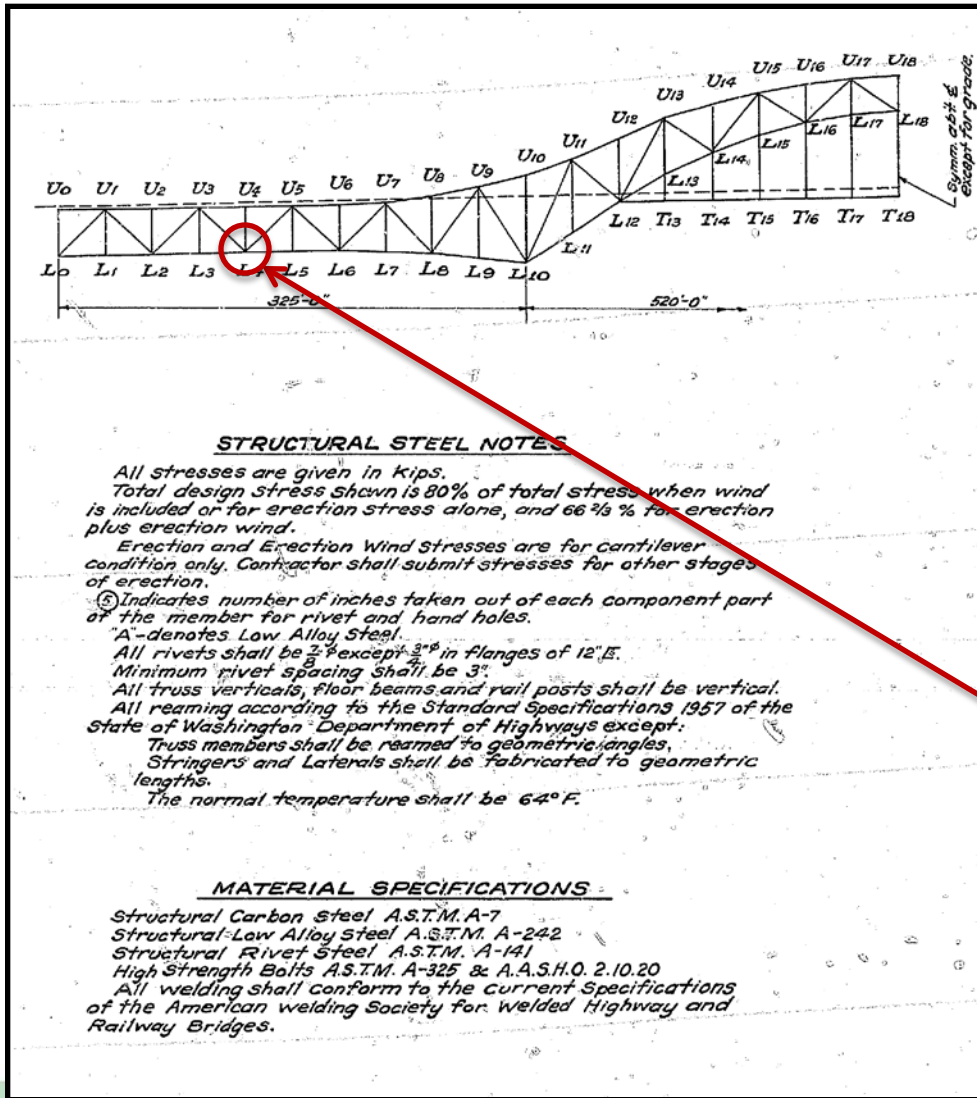
- CSI used for analysis
 - Original analysis condition considered.
 - Verified model against original dead loads.
 - Modeled idealized boundary conditions.
- 2D or 3D models used.
 - 2D quicker, 3D more useful later, but rarely.



EXAMPLE ~ VANTAGE BRIDGE



TRIAGE EXAMPLE ~ MATERIALS

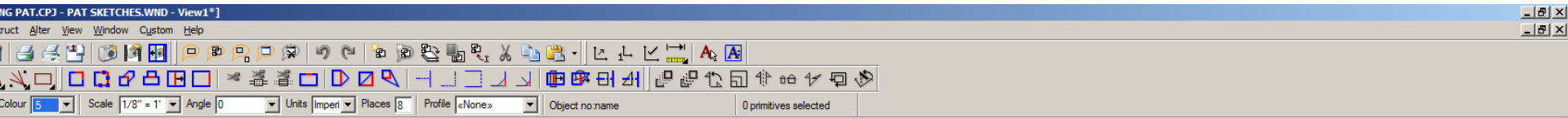







ASTM A-7 ~ $f_y = 33\text{ksi}$
ASTM A-242 ~ $f_y = 50\text{ksi}$
ASTM A-141 ~ $f_y = 24\text{-}32\text{ ksi}$

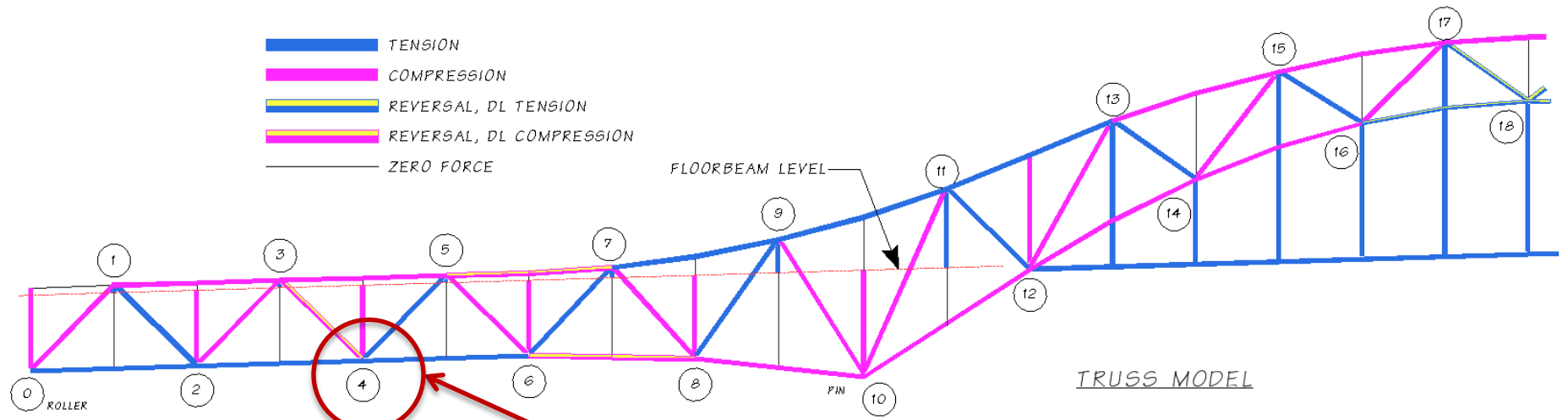
For rivets, f_y varies depending upon connection length per the 2011 Interim to the 2010 MBE Article 6A.6.12.5.

EXAMPLE
NODE ~ L4

TRIAGE EXAMPLE ~ FORCES

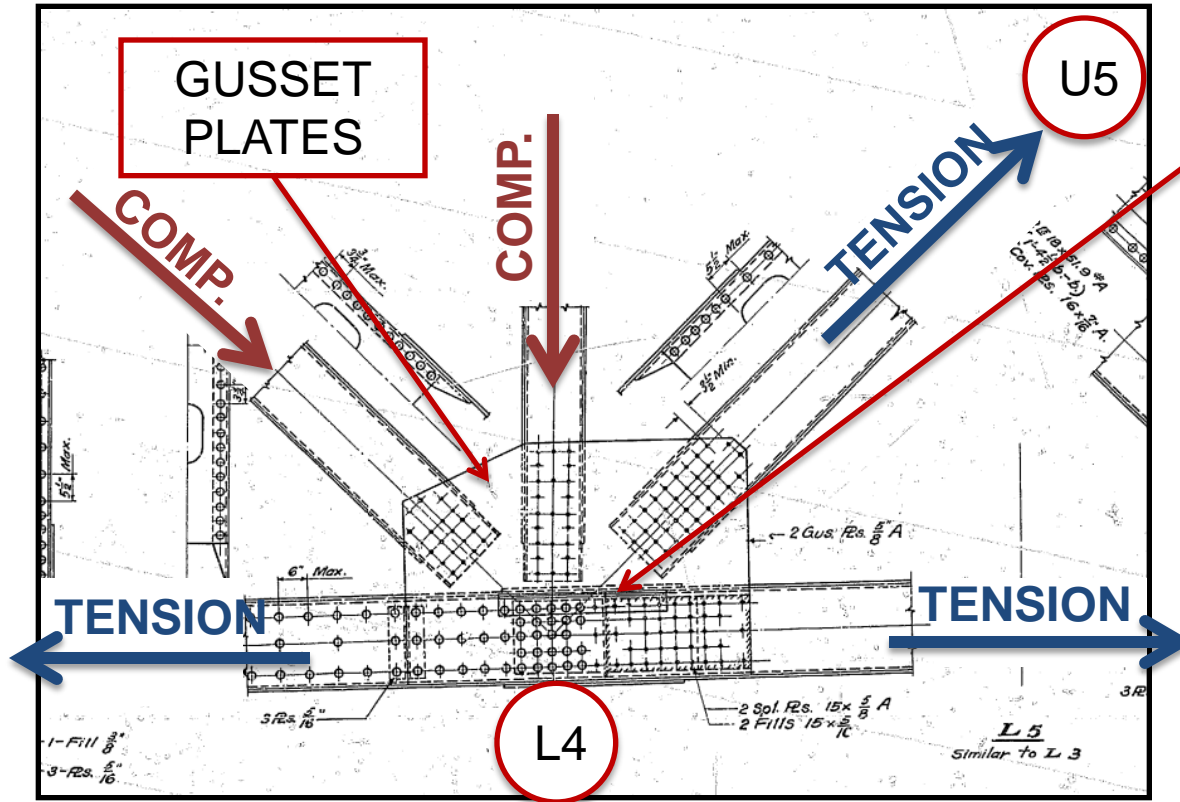


-  TENSION
-  COMPRESSION
-  REVERSAL, DL TENSION
-  REVERSAL, DL COMPRESSION
-  ZERO FORCE



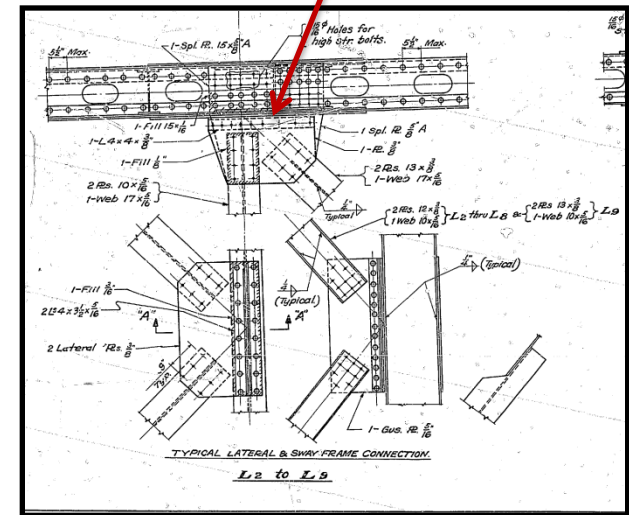
**EXAMPLE
NODE ~ L4**

TRIAGE EXAMPLE ~ AS-BUILTS



AS-BUILT ~ NODE L4

CONSIDER L4-U5 FOR OUR EXAMPLE

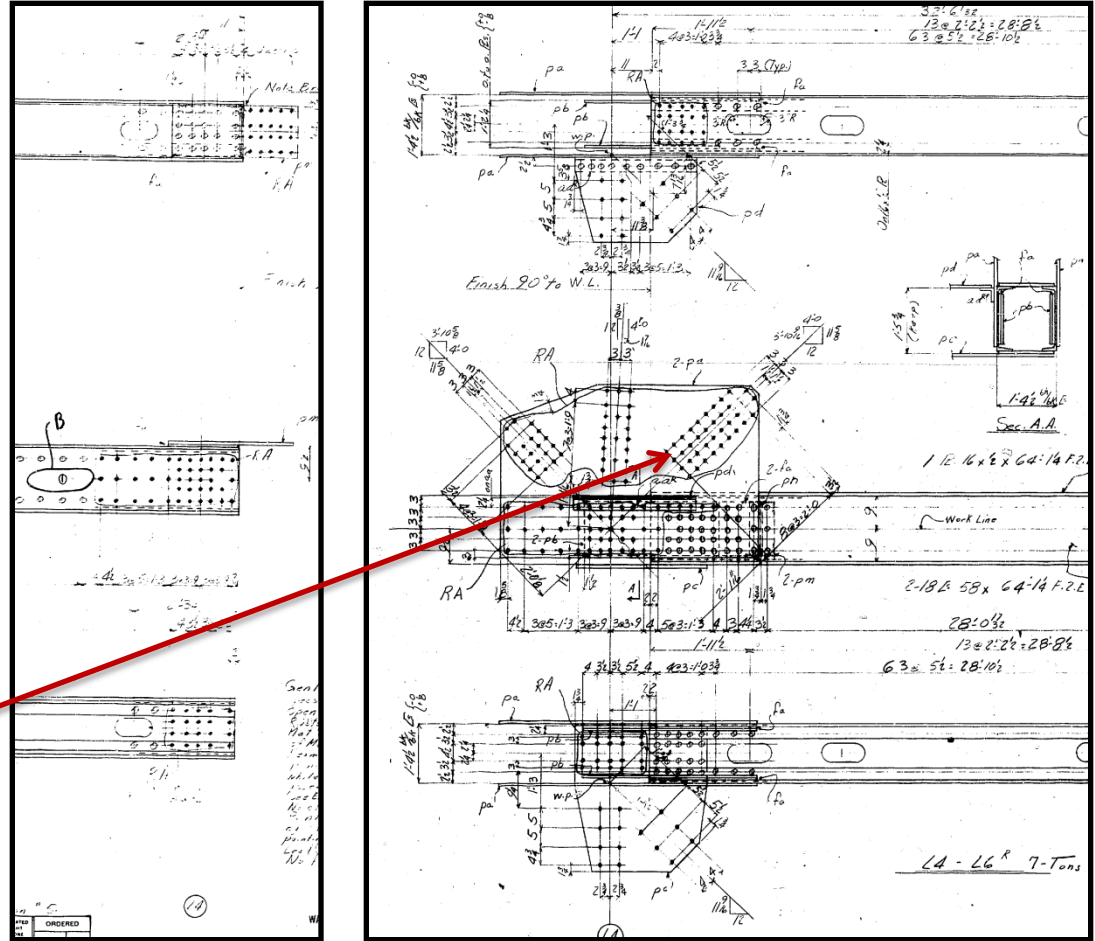


AS-BUILT ~ NODE L4

TRIAGE EXAMPLE ~ SHOP DRAWINGS

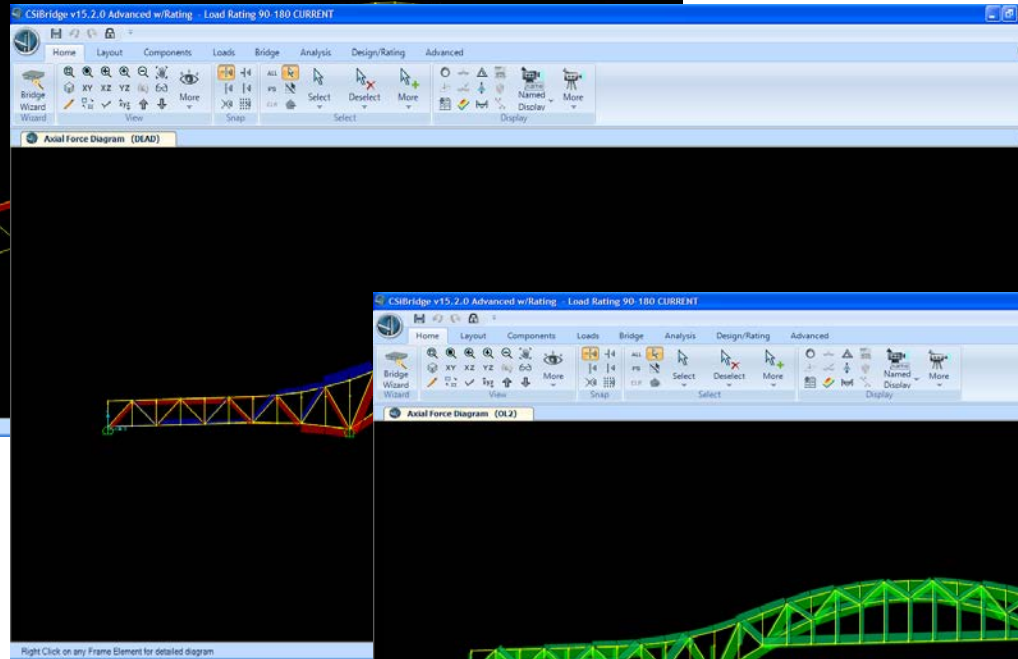
Often times the As-Builts are not correct. For determining exact plate sizes and connection geometry, the shop drawings are the only reliable tool.

CONNECTION
CONSIDRED
~ L0-U5



SHOP DRAWINGS ~ NODE L4

MODELING ~ VANTAGE



MODELING RESULTS

- Member 1028 = L4-U5

MEMBER END FORCES:

LANE DISTRIBUTION FACTORS:				
	LANE 2	LANE 3	LANE 4	TOTAL
1080 FT SPAN	0.4064	0.6713	0.8583	1.9360
Multiple Presense Factor				
	2 LANES	3 LANES	4 LANES	
	1.00	0.90	0.75	

TABLE: Element Forces - Frames ~ THREE LANES CONTROL

Frame	OutputCase	DEAD	UNIT LANE		LANES 2, 3, 4		TRIAGE INPUTS		LEGAL IN LEFT		IF 2.17* opposing LL >> 1.3*DL, THEN BOTH DIRECTIONS OF LOAD ARE CONSIDERED.
			Tension (kips)	Comp. (kips)	Tension (kips)	Comp. (kips)	Tension (kips)	Comp. (kips)	T. (kips)	C. (kips)	
1028	DEAD	314.7									
	HS-20 TK		50.0	-34.6	87.1	-60.2	Chord?	N			1.3DL = 409.1 kips 2.17 opposing LL = -193.0 kips
	HS-20 18K		75.9	-36.6	132.3	-63.8	CONTROLLING HS-20				CHECK: No reversal check required.
	HS-20 26K		81.9	-40.8	142.6	-71.0	142.64	-71.05	54.7	-35.7	
	TYPE 3		35.2	-24.4	61.4	-42.6	61.39	-42.57			
	TYPE 3S2		46.4	-31.6	80.8	-55.1	80.78	-55.06			
	TYPE 3-3		49.1	-33.4	85.6	-58.2	85.62	-58.16			
	NRL		53.9	-36.8	94.0	-64.2	93.97	-64.20			
	LEGAL LANE		56.4	-33.5	98.2	-58.4	98.25	-58.43			
	OL1		65.2	-44.9	113.7	-78.2	50.39	-30.14	NOTE:		
	OL2		118.5	-79.3	206.4	-138.1	91.52	-53.20	OL for triage input		

ANALYSIS

Gusset Plate Inputs & Summary

Sheet Information										Comments																																																																																																																																										
Rated By	Company	Date	Bridge ID	Gusset ID	Number of Connections	Include Rivets?	Condition Factor, ϕ_c	Redundancy Factor, ϕ_s																																																																																																																																												
Patrick Gallagher	WSDOT Bridge	12/19/2012	90/180	L4	5	Y	1	1		Live load distribution considered in the reactions input below.																																																																																																																																										
<p>LL Distribution Factors</p> <p>Forces entered into spreadsheet shall be based on a single lane distribution.</p> <p>AASHTO & Legal Trucks: 1.000</p> <p>OL Trucks: 1.000</p> <p>Legal Truck w/OL: 1.000</p> <p>LL Distribution factor for Design & Legal truck shall be based on the number of lanes multiplied by the appropriate reduction factor.</p> <p>LL Distribution factor for one OL placed in lane closest to truss multiplied by the appropriate reduction factor.</p> <p>LL Distribution factor for Legal Truck w/OL assumes legal loads are placed in lanes adjacent to OL truck multiplied by the appropriate reduction factor.</p>									ϕ_s equals 1 for LFR																																																																																																																																											
<p>LL Input and RF Summary</p> <table border="1"> <thead> <tr> <th rowspan="2">Load Case ID</th> <th colspan="5">Live Loads</th> <th rowspan="2">Minimum RF</th> <th rowspan="2">Controlling Connection ID</th> <th rowspan="2">Controlling Resistance Type</th> <th colspan="2">Operating RF for LFR only</th> </tr> <tr> <th>Truck Type</th> <th>Overload?</th> <th>γ_{LL}</th> <th>Impact Factor (I)</th> <th>Rating Method</th> <th>γ_{LL}</th> <th>Minimum RF</th> </tr> </thead> <tbody> <tr> <td>HS-20</td> <td>HS-20</td> <td>N</td> <td>2.17</td> <td>0.0943</td> <td>LFR</td> <td>1.66</td> <td>L4-L3</td> <td>Rivets</td> <td>1.3</td> <td>2.77</td> </tr> <tr> <td>TYPE 3</td> <td>TYPE 3</td> <td>N</td> <td>2.17</td> <td>0.0943</td> <td>LFR</td> <td>2.65</td> <td>L4-U4</td> <td>Rivets</td> <td>1.3</td> <td>4.43</td> </tr> <tr> <td>TYPE 3S2</td> <td>TYPE 3S2</td> <td>N</td> <td>2.17</td> <td>0.0943</td> <td>LFR</td> <td>2.52</td> <td>L4-U4</td> <td>Rivets</td> <td>1.3</td> <td>4.21</td> </tr> <tr> <td>TYPE 3-3</td> <td>TYPE 3-3</td> <td>N</td> <td>2.17</td> <td>0.0943</td> <td>LFR</td> <td>2.63</td> <td>L4-L3</td> <td>Rivets</td> <td>1.3</td> <td>4.40</td> </tr> <tr> <td>NRL</td> <td>NRL</td> <td>N</td> <td>2.17</td> <td>0.0943</td> <td>LFR</td> <td>1.69</td> <td>L4-U4</td> <td>Rivets</td> <td>1.3</td> <td>2.81</td> </tr> <tr> <td>LEGAL LANE</td> <td>LEGAL LANE</td> <td>N</td> <td>2.17</td> <td>0.0943</td> <td>LFR</td> <td>2.26</td> <td>L4-L3</td> <td>Rivets</td> <td>1.3</td> <td>3.77</td> </tr> <tr> <td>OL1</td> <td>OL1</td> <td>Y</td> <td>1.3</td> <td>0.2</td> <td>LFR</td> <td>4.68</td> <td>L4-U4</td> <td>Rivets</td> <td>1.3</td> <td>4.68</td> </tr> <tr> <td>OL2</td> <td>OL2</td> <td>Y</td> <td>1.3</td> <td>0.2</td> <td>LFR</td> <td>3.01</td> <td>L4-L3</td> <td>Rivets</td> <td>1.3</td> <td>3.01</td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> </tbody> </table>											Load Case ID	Live Loads					Minimum RF	Controlling Connection ID	Controlling Resistance Type	Operating RF for LFR only		Truck Type	Overload?	γ_{LL}	Impact Factor (I)	Rating Method	γ_{LL}	Minimum RF	HS-20	HS-20	N	2.17	0.0943	LFR	1.66	L4-L3	Rivets	1.3	2.77	TYPE 3	TYPE 3	N	2.17	0.0943	LFR	2.65	L4-U4	Rivets	1.3	4.43	TYPE 3S2	TYPE 3S2	N	2.17	0.0943	LFR	2.52	L4-U4	Rivets	1.3	4.21	TYPE 3-3	TYPE 3-3	N	2.17	0.0943	LFR	2.63	L4-L3	Rivets	1.3	4.40	NRL	NRL	N	2.17	0.0943	LFR	1.69	L4-U4	Rivets	1.3	2.81	LEGAL LANE	LEGAL LANE	N	2.17	0.0943	LFR	2.26	L4-L3	Rivets	1.3	3.77	OL1	OL1	Y	1.3	0.2	LFR	4.68	L4-U4	Rivets	1.3	4.68	OL2	OL2	Y	1.3	0.2	LFR	3.01	L4-L3	Rivets	1.3	3.01																																
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Plate Material & Dimension Inputs

Gusset Plate Properties		Wind Gusset Plate Properties		Splice Plate Properties		Rivet Properties	
Fy_gp (ksi)	50	Fy_wp (ksi)	33	Fy_sp (ksi)	50	Fu_r (ksi)	24
Thickness, tgp (in)	0.625						
Num Plates, np	2						

ANALYSIS

Triage Procedure Connection Inputs						Rated By	Patrick Gallagher	
Connection Information						Company	WSDOT Bridge	
Connection ID	Chord or Web?	Splice PL's?	Wind Bracing GP?	Comp. or Tension?	Notes to Input / RF	Date	#####	
L4-L5	Web	N	N	Tension		Bridge ID	90180	

Gusset Plate Connection			
Wc (in)	9	2*Lc tan 30 + Wc	36.71
Lc (in)	24	Is Plate Width < 2*Lc tan 30 + Wc?	N
Wc (in)			
Wc (in)			

Individual Splice Plate Dimensions			Wind Bracing GP Dimensions				
Splice ID	Wc (in)	Lc (in)	Splice ID	Wc (in)	Lc (in)	Ls (in)	Lp (in)

Summary of Yielding Resistance Calculations				
Agg_wb (in ²)	45.89		Rn (k)	1324.8
Awa (in ²)	0.00	»		
1Agg (in ²)	0.00			

Buckling Resistance Inputs							Summary of Buckling Resistance Calculations				
Controlled Length, Lcnd (in)	Lcnd (in)	Lcnd (in)	Lcnd (in)	»	»	»	Rb (k)				
77.36	2.210	2.210	17.07								
Uncontrolled Length, Lcnd (in)	Lcnd (in)	Lcnd (in)	Lcnd (in)	»	»	»	Rb (k)				
0.00	0.000	0.000	0.000								
Code Ref: Lcnd (in) < Lcnd (in) at width of the joint											

Rivet Input				Rivet Resistance
Rivet Diameter, D_r (in)	# of Single Shear Rivets, ns	# of Double Shear Rivets, nds	»	Rn (k)
0.875	72	0		1039.1

Rating Factors	
Controlling Resistance (k)	Resistance Type
1039.1	Rivets

Dead Load Rating Method				Controlling Legal Load for DL rating	
Rating Method	LFR	»	Factored DL (k)	Maximum Legal Load	54.68950305
yDL	1.3		409.11	Maximum force due to legal load based on one lane distribution	
Dead Load (k)	314.7				

LRFR				Controlling RF	
Rating Method	LRFR	»	Factored DL (k)	Controlling RF	
yDL_C			0		
DL_C (k)					
yDL_W					
DL_W (k)					

LL Input and Connection RF Summary						Resistance Type				
Load Case ID	Truck Type	yLL	Impact Factor (I)	Rating Method	Member LL (k)	Yielding		Buckling		Rivets
						RF	RF	RF	RF	
H5-20	H5-20	2.17	0.0943	LFR	142.641576	2.70	N/A	N/A	1.86	
TYPE 3	TYPE 3	2.17	0.0943	LFR	61.3899792	6.28	N/A	N/A	4.32	
TYPE 3S2	TYPE 3S2	2.17	0.0943	LFR	80.7759216	4.77	N/A	N/A	3.28	
TYPE 3-3	TYPE 3-3	2.17	0.0943	LFR	85.621536	4.50	N/A	N/A	3.10	
NRL	NRL	2.17	0.0943	LFR	93.9728592	4.10	N/A	N/A	2.82	
LEGAL LANE	LEGAL LANE	2.17	0.0943	LFR	98.245224	3.92	N/A	N/A	2.70	
DL1	DL1	1.3	0.2	LFR	50.39439796	10.56	N/A	N/A	6.93	
DL2	DL2	1.3	0.2	LFR	91.51805184	5.82	N/A	N/A	3.82	

SUMMARY OF NODES

TRUCK	RATING FACTORS																								MIN. RATING FACTORS		MIN. RATING FACTORS					
	L0		L2		L4		L6		L8		L10		L12		L13		L14		L15		L16		L17		L18		Inventor	Operatin	Inventor	Operatin		
	y	g	y	g	y	g	y	g	y	g	y	g	y	g	y	g	y	g	y	g	y	g	y	g								
AASHTO 1	2.52	4.20	2.83	4.73	2.65	4.43	2.43	4.06	2.15	3.59	4.08	6.81	3.25	5.43	2.50	4.17	2.50	4.17	2.47	4.12	2.50	4.16	1.28	2.14	2.49	4.15	1.28	2.14	1.28	2.14	ALL SPANS Inventor Operatin y g 1.28 2.14 1.22 2.03 1.22 2.03 1.30 2.17 1.30 2.17 0.81 1.36 1.30 2.17 1.30 2.17 NA 1.39 NA 1.11 NA 2.88 NA 1.11 NA 1.39 0.95 1.36 1.58 2.27	1.51
AASHTO 2	1.85	3.09	2.07	3.45	2.52	4.21	1.88	3.14	1.57	2.63	2.89	4.83	2.48	4.15	2.37	3.96	2.37	3.96	2.30	3.84	2.32	3.87	1.22	2.03	2.36	3.95	1.22	2.03	1.22	2.03		
AASHTO 3	1.71	2.85	1.93	3.22	2.59	4.33	1.74	2.91	1.45	2.43	2.63	4.38	2.34	3.91	2.53	4.23	2.34	3.91	2.43	4.05	2.18	3.63	1.30	2.17	2.49	4.16	1.30	2.17	1.30	2.17		
NRL	1.62	2.70	1.77	2.95	1.69	2.81	1.55	2.58	1.38	2.30	2.59	4.33	2.11	3.52	1.59	2.65	1.59	2.65	1.57	2.62	1.59	2.65	0.81	1.36	1.58	2.64	0.81	1.36	1.30	2.17		
Legal Lane	1.50	2.50	1.59	2.65	2.22	3.71	1.55	2.59	1.30	2.17	1.89	3.15	2.10	3.50	2.77	4.63	2.09	3.49	2.54	4.24	1.81	3.02	1.39	2.31	2.07	3.46	1.30	2.17	0.81	1.36		
OL1	NA	3.98	NA	3.74	NA	4.68	NA	3.57	NA	3.23	NA	6.84	NA	5.70	NA	3.78	NA	3.78	NA	3.71	NA	3.78	NA	1.39	NA	3.76	NA	1.39	1.30	2.17		
OL2	NA	2.04	NA	1.88	NA	2.94	NA	1.84	NA	1.65	NA	3.24	NA	3.11	NA	3.02	NA	3.02	NA	2.85	NA	2.82	NA	1.11	NA	2.88	NA	1.11	NA	1.39		
Inventory (HS20)	1.06				1.63		1.12		0.95		1.15		1.49		1.85		1.47		1.82		1.18		0.95		1.36		0.95		NA	1.11		
Operating (HS20)	1.77		1.91		2.73		1.87		1.58		1.92		2.49		3.08		2.46		3.04		1.97		1.58		2.27		1.58		0.90	1.11		

TRUCK	RATING FACTORS																								MIN. RATING FACTORS							
	U1		U3		U5		U7		U8		U9		U10		U11		U13		U15		U17		L4, L6, L16 REV.		U6 REV.		Inventor	Operatin				
	y	g	y	g	y	g	y	g	y	g	y	g	y	g	y	g	y	g	y	g	y	g	y	g								
AASHTO 1	2.90	4.84	2.25	3.75	3.51	5.86	2.93	4.90	5.62	9.39	2.41	4.03	7.58	12.65	4.40	7.34	2.84	4.74	2.47	4.12	2.13	3.55	4.94	8.25	5.95	9.93	2.13	3.55	MIN. RATING FACTORS	1.51		
AASHTO 2	2.13	3.55	1.68	2.81	2.61	4.36	2.15	3.58	3.95	6.59	2.30	3.83	5.30	8.85	4.20	7.00	2.47	4.13	2.30	3.84	1.99	3.32	3.76	6.28	4.17	6.97	1.68	2.81				
AASHTO 3	1.98	3.30	1.57	2.62	2.43	4.06	1.98	3.31	3.58	5.98	2.27	3.79	4.81	8.03	4.05	6.76	2.33	3.89	2.24	3.74	2.10	3.51	3.53	5.90	3.79	6.32	1.57	2.62				
NRL	1.84	3.07	1.46	2.43	2.27	3.79	1.88	3.14	3.53	5.89	1.53	2.56	4.75	7.93	2.80	4.67	1.80	3.01	1.57	2.62	1.35	2.26	3.24	5.40	3.73	6.23	1.35	2.26				
Legal Lane	1.71	2.86	1.47	2.46	2.11	3.52	1.78	2.96	2.56	4.27	1.80	3.00	2.69	4.48	3.02	5.03	2.09	3.49	2.00	3.34	1.81	3.02	3.42	5.70	2.81	4.69	1.47	2.46				
OL1	NA	4.70	NA	3.55	NA	6.10	NA	4.69	NA	8.64	NA	3.62	NA	11.72	NA	7.53	NA	4.44	NA	3.71	NA	3.05	NA	8.13	NA	9.28	NA	3.05				
OL2	NA	2.44	NA	1.89	NA	3.22	NA	2.41	NA	4.10	NA	2.55	NA	5.55	NA	4.83	NA	3.10	NA	2.85	NA	2.36	NA	4.45	NA	4.40	NA	1.89				
Inventory (HS20)	1.28		1.12		1.45		1.29		1.55		1.40		1.35		1.58		1.48		1.41		1.18		2.71		1.76		0.90				NA	1.89
Operating (HS20)	2.13		1.88		2.43		2.16		2.58		1.51		2.26		2.64		2.48		2.35		1.97		4.73		2.94		0.90				1.51	1.11

TRUCK	RATING FACTORS										MIN. RATING FACTORS	
	U3, U5, U17 REV.		L8 REV.		L17 REV.		L18 REV.		Tie Splice		Inventor	Operatin
	y	g	y	g	y	g	y	g	y	g		
AASHTO 1	4.94	8.25	10.96	18.29	7.97	13.31	6.11	10.20	3.92	6.54	MIN. RATING FACTORS	1.64
AASHTO 2	3.76	6.28	8.27	13.80	5.77	9.64	4.55	7.60	2.73	4.55		
AASHTO 3	3.53	5.90	7.80	13.01	5.33	8.90	4.24	7.07	2.46	4.11		
NRL	3.24	5.40	6.90	11.52	5.01	8.36	3.97	6.63	2.45	4.09		
Legal Lane	3.42	5.70	6.82	11.38	4.58	7.64	3.63	6.06	1.68	2.81		
OL1	NA	8.13	NA	19.06	NA	15.22	NA	11.56	NA	5.49		
OL2	NA	4.45	NA	10.15	NA	7.59	NA	6.11	NA	2.56		
Inventory (HS20)	2.39		5.08		3.38		2.48		0.98			
Operating (HS20)	3.99		8.48		5.64		4.13		1.64			

CONTROLLING RF W/O GUSSETS:

AASHTO 1 = 1.10
 AASHTO 2 = 1.05
 AASHTO 3 = 1.12
 NRL = NA ~ Pre 2011
 Legal Lane = 1.00
 OL1 = 1.08
 OL2 = 0.92
 HS20 Inventory = 0.31
 HS20 Operating = 0.52

OTHER PORTIONS HAVE
 LOWER RFS, GUSSETS DO NOT
 CONTROL. RATING COMPLETE

APPLICATION ~ SO WHAT?

- SIEVE 1:
 - If the Rating Factors are higher than those currently listed, then the analysis is done.
- SIEVE 2:
 - If the gusset ratings are lower than those currently listed, then the FHWA Method is used.
- SIEVE 3:
 - If RFs are still very low, more detailed analysis tools could be utilized.
- SIEVE 4:
 - If more detailed analysis yields low RFs, then the low gusset RFs are used for rating the entire bridge.

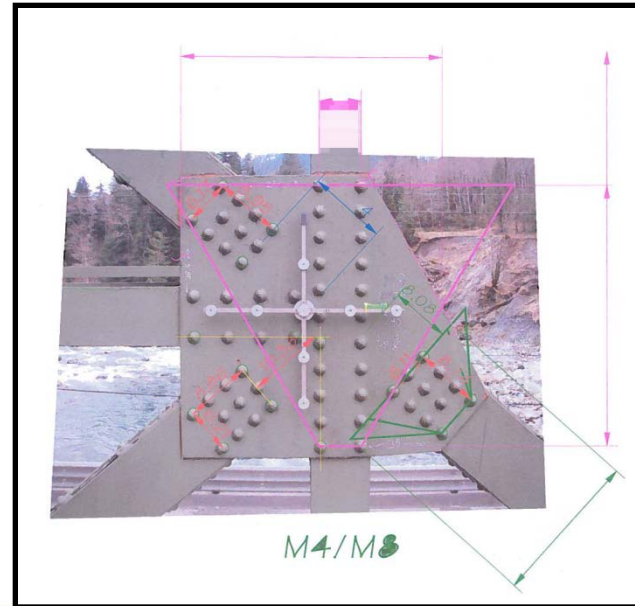
OTHER FACTORS

- Know the spreadsheet and how it works.
 - Not everything fits into the mold of that spreadsheet.
 - Stacked gussets, varying material strengths, varying rivet diameters, triple shear rivets.
- Know what you're trying to achieve.
 - Lift span bridges are closed under live load.
 - Understand erection stresses and how they were managed.
- Know how truss bridges function.
 - Truss engineering is a dying art. Learn how they work.
 - If it should be a zero force member, make it one.
 - Hanger members should all have the same loads.
 - Understand drop spans and cantilever spans.

NO AS-BUILTS?



U3/U9



M4/M8

WHAT'S NEXT?

- Once the ratings are updated for gussets, maintaining those records will be ongoing.
- Inspection practices have been adjusted to account for gussets.
- More effort and discussion will be given to bridge maintenance.
- The timeliness is excellent. With a huge design and construction package being completed, maintenance is a natural place to turn efforts towards.

FUTURE OF INSPECTION

- Gusset plates are now their own BMS Element.
- Bridge inspections have been including field verification of gusset thicknesses.
- Truss ratings include gusset ratings.



QUESTIONS:



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