

Sound Transit *Sounder* Commuter Rail

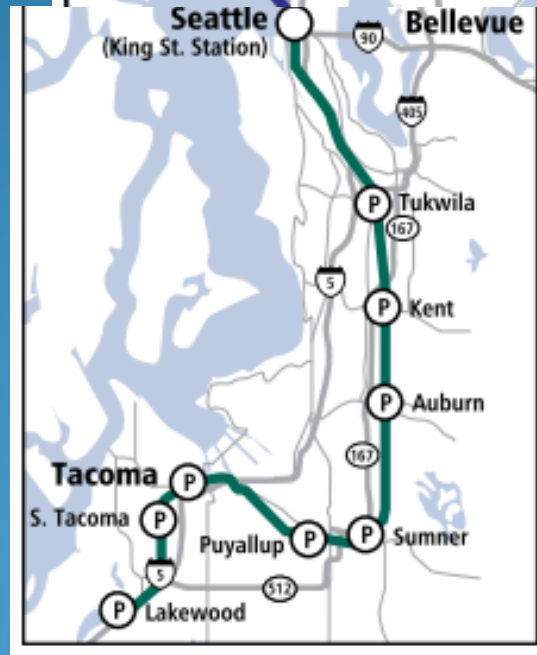
The D-to-M Streets Track and Signal Improvement Project: Pacific Avenue Bridge



Western Bridge Engineers' Seminar
September 4-6, 2013

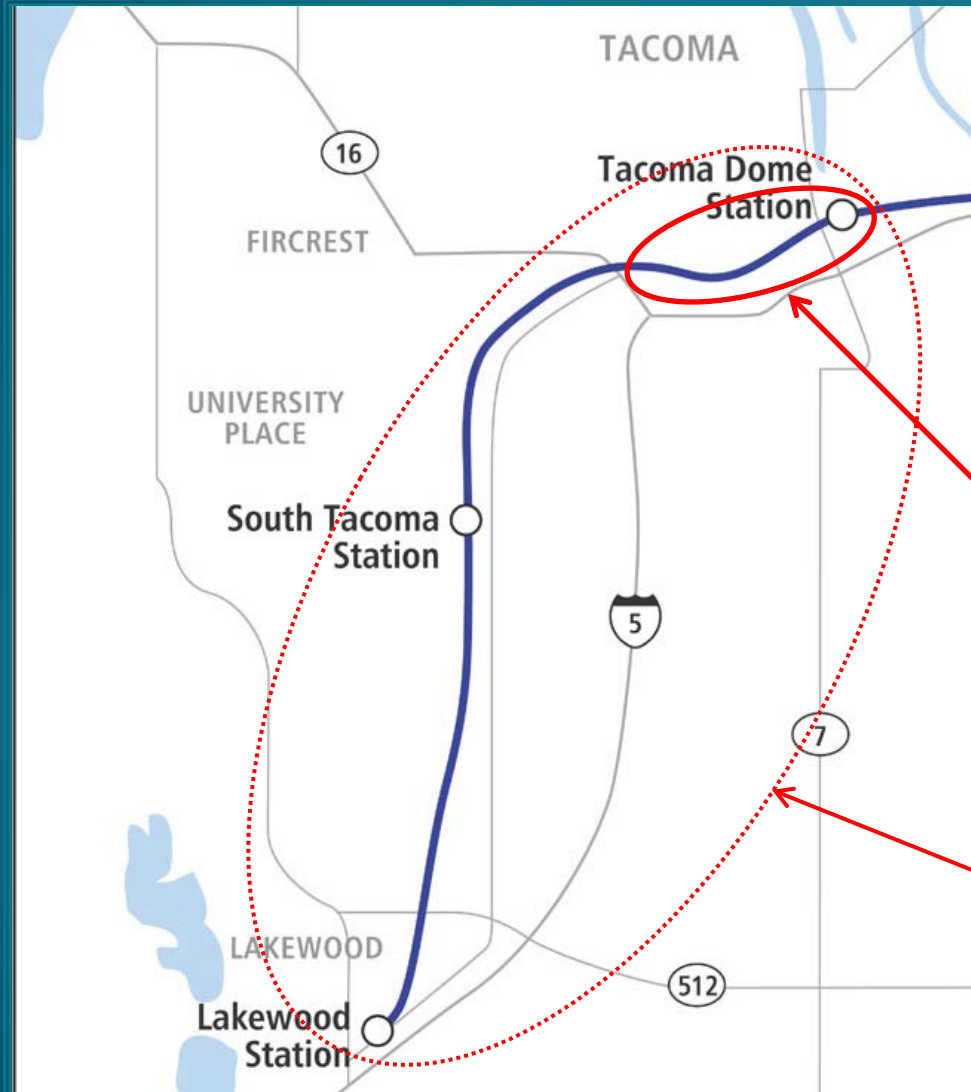
Sounder System Map

Everett – Seattle



Seattle - Lakewood

Tacoma to Lakewood Corridor



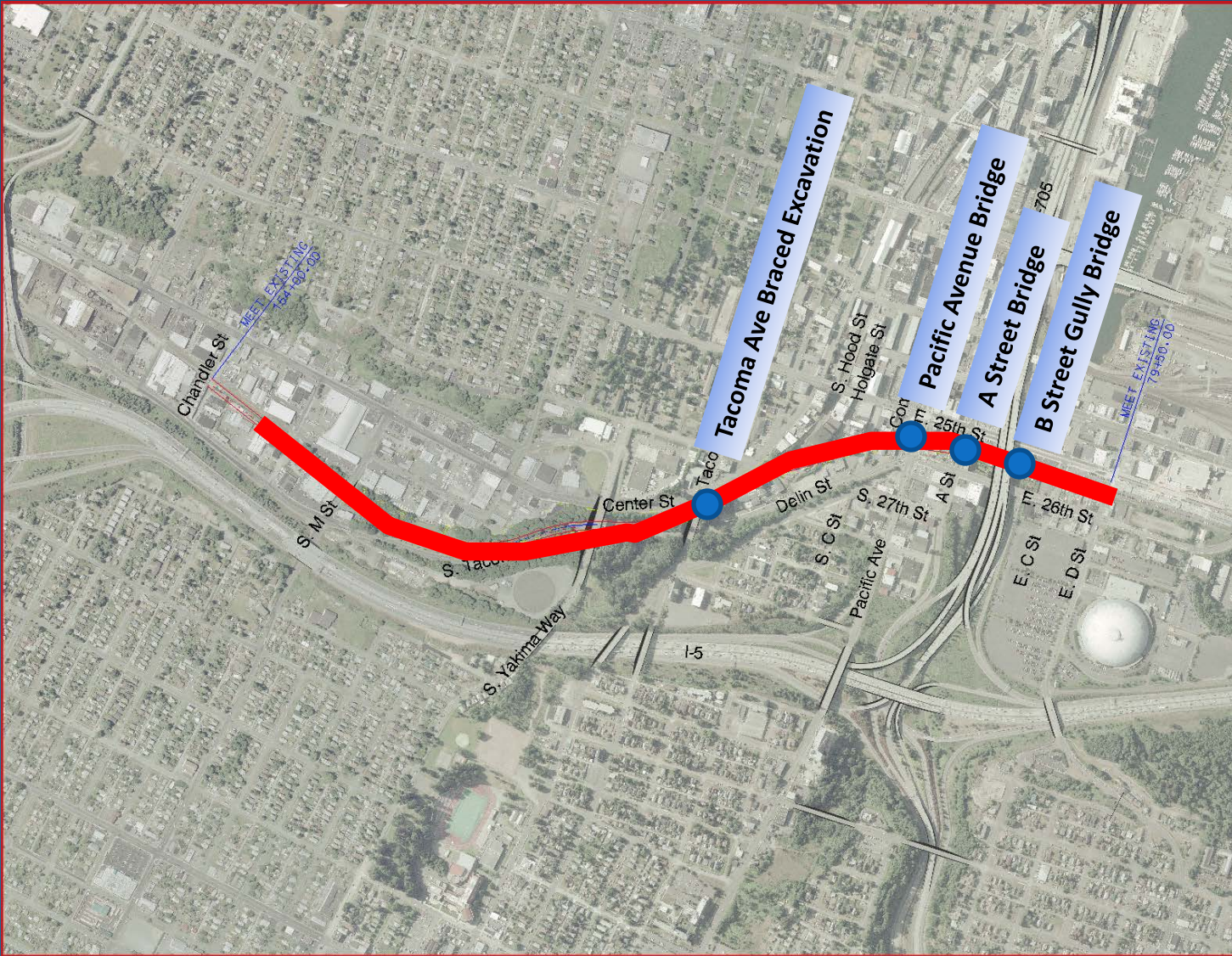
• 8.2 Miles

- 1.4 miles of new track
- 6.8 miles of track and signal upgrades

D to M Street

Tacoma to Lakewood

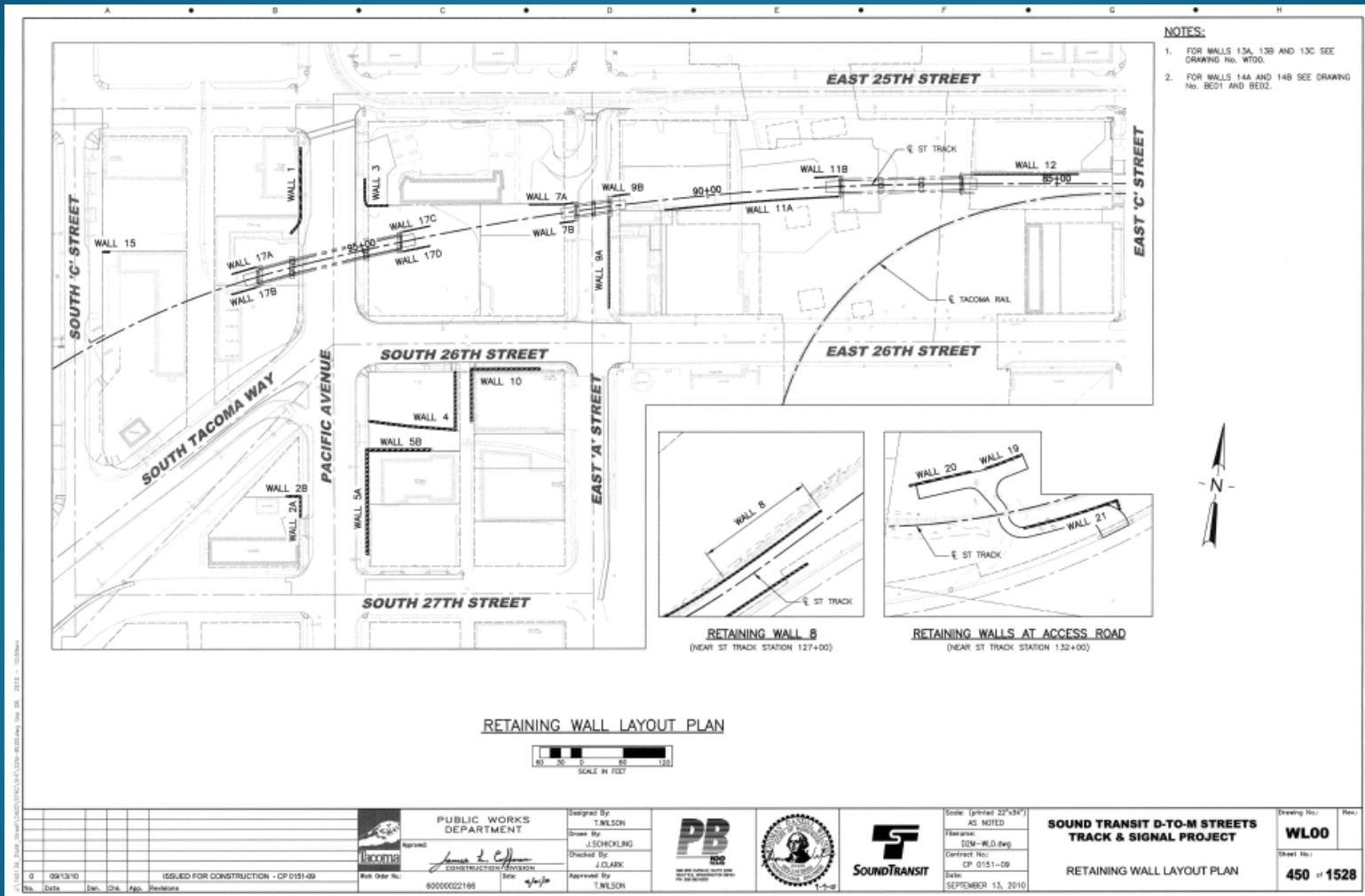
D to M Street Corridor



Project Elements

- At beginning of project (10 - 15% level of design)
 - 3 walls in downtown area
 - 1 bridge (3-span)
 - 3,500' of cut wall
 - 1 braced excavation
- At end of project (100% level of design)
 - 22 walls in downtown area & along cut
 - 3 bridges (2ea – 3 span, 1ea – 2 span)
 - 2,400' of soil nail wall
 - 1 braced excavation

- Wall Types: Soldier Pile, SP w/ Tiebacks, Concrete Cantilever, SEW, Soil Nails, Block walls



Tacoma Avenue Braced Excavation



B Street Gully Bridge - Rendering



B Street Gully Bridge



A Street Bridge - Rendering



A Street Bridge



Visualizations

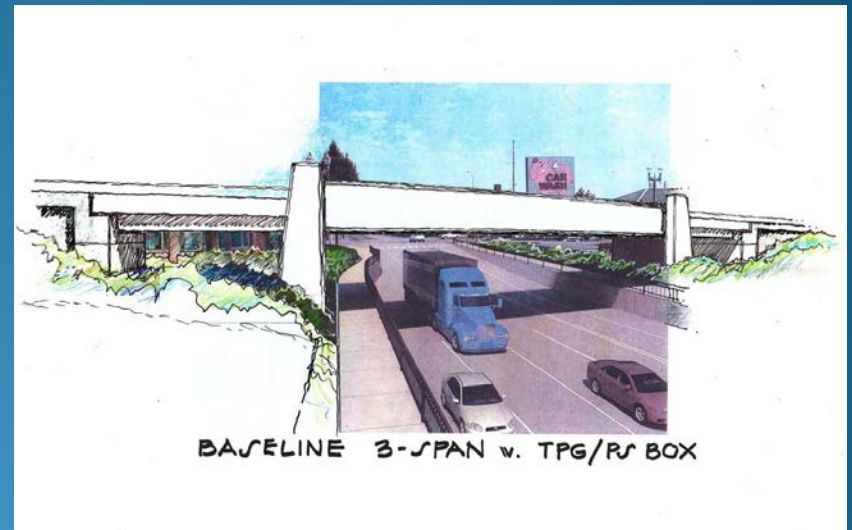
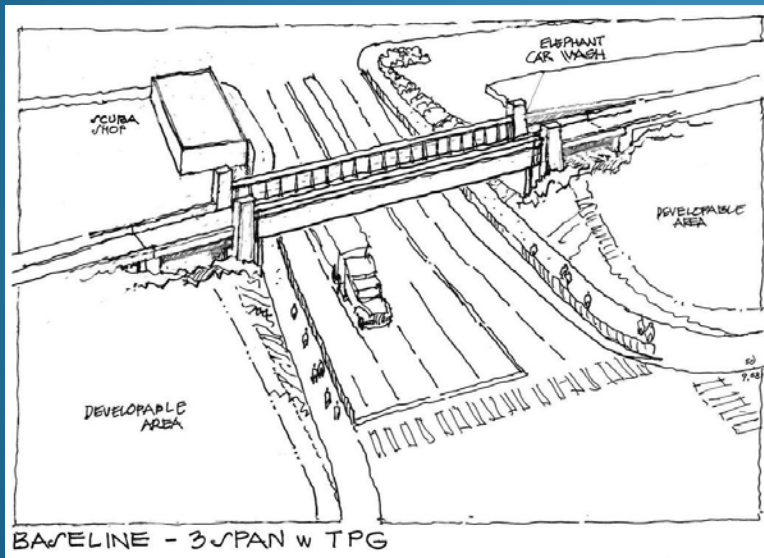
- Used for:
 - Project stakeholder meetings
 - Open houses
 - City Council approval of Pacific Avenue Bridge aesthetics
- Originally limited within project scope
- Became the **go-to deliverable** to show engineering elements to non-engineers

Financials

- Construction:
 - Engineers Estimate = \$66M
 - Low bid by Mid-Mountain Construction = \$40.8M
 - Bid + Change Orders \approx \$69M
 - Bulk of CO cost related to contaminated material discovery
- Design + DSDC: (PB + 6 Subconsultants)
 - Total Team Budget = \$14.5M
 - Design = \$10.5M
 - DSDC = \$4M

Pacific Ave Bridge Type Selection

- Bridge Type Study Undertaken in August 2008
 - General Criteria:
 - Feasible
 - Affordable
 - Attractive



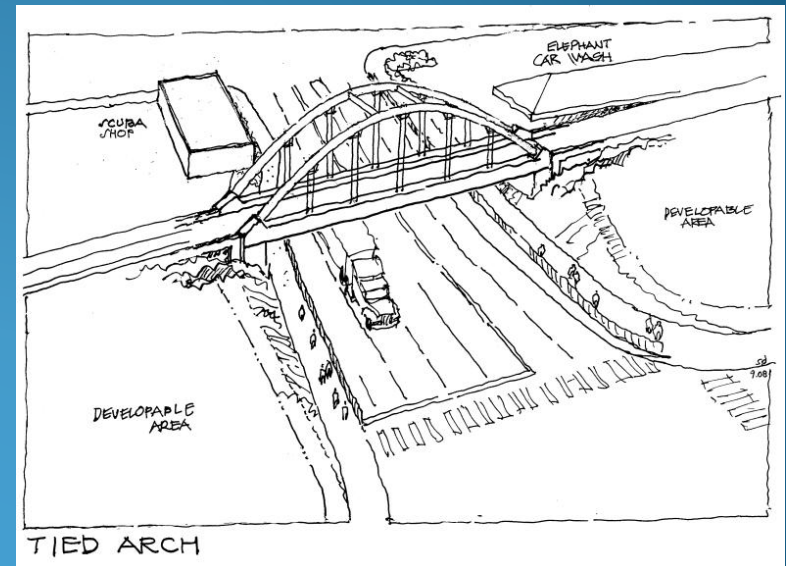
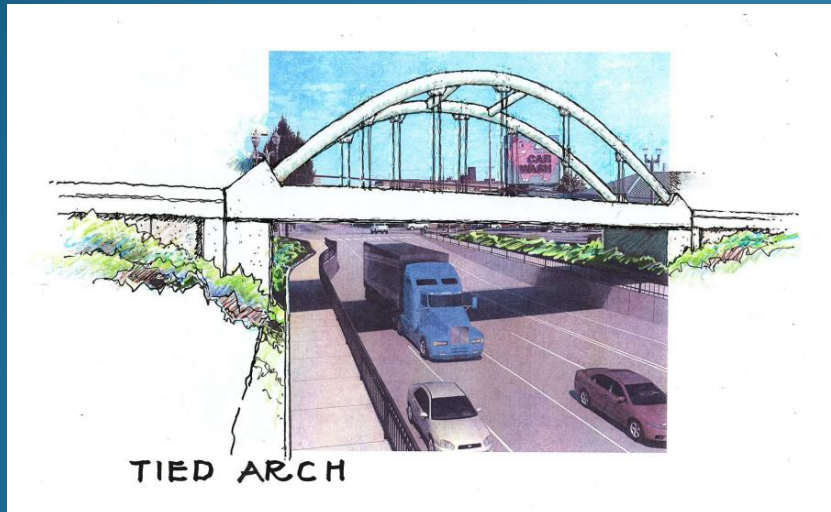
Baseline 3-span TPG with PS
Box side spans

Alternatives Considered

- Cast-in-Place Thru Girder
- Thru Plate Girder
- Tied Arch
- A-Frame
- Thru Truss (Pony Truss)
- Extradosed
- Thru Steel Box Girder
- Cable-Stayed

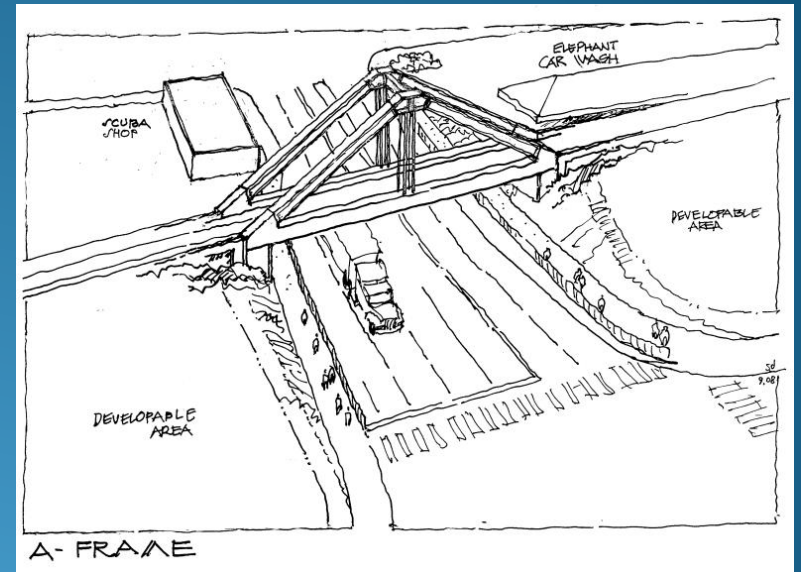
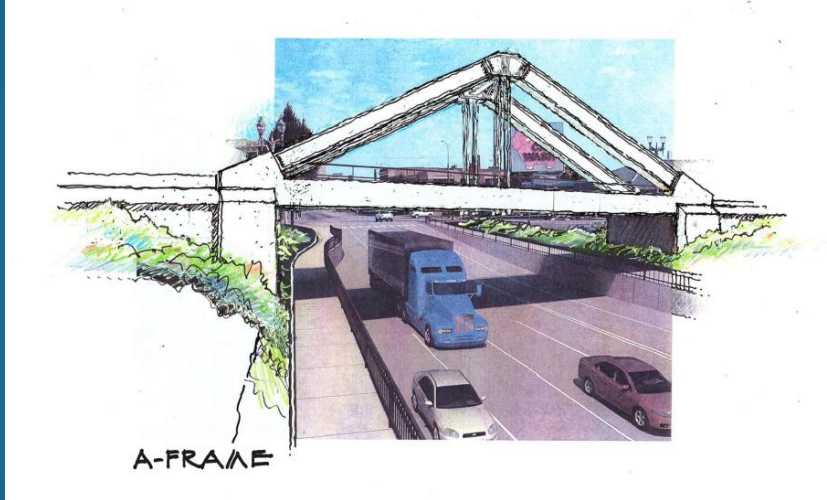
A few of the Alternatives Evaluated

- Single Span Tied Arch



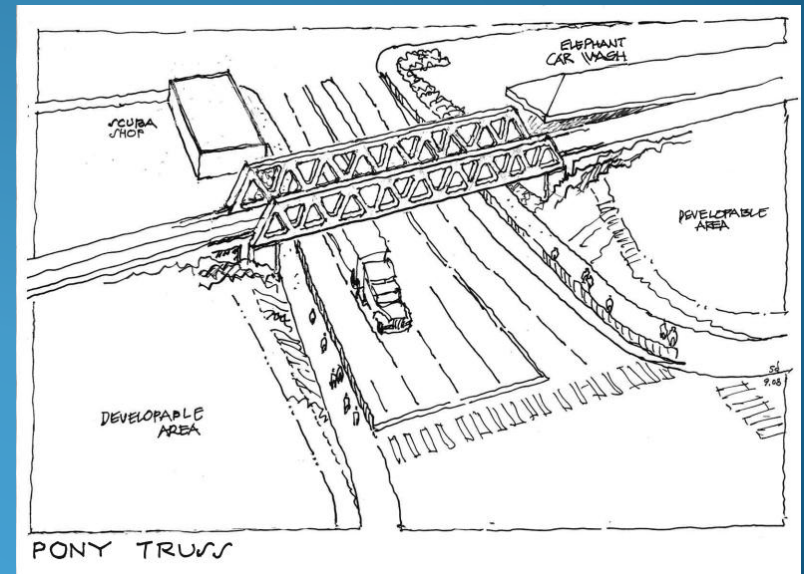
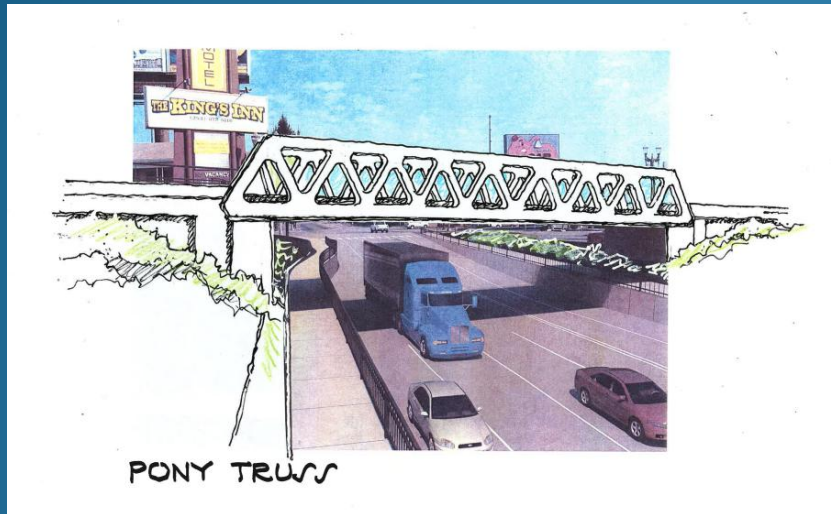
Alternatives Cont'd

- Single Span A-Frame



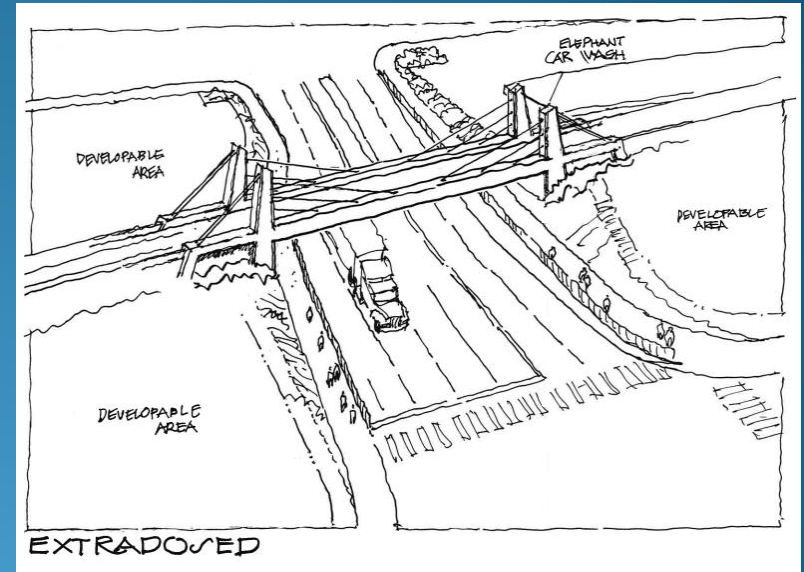
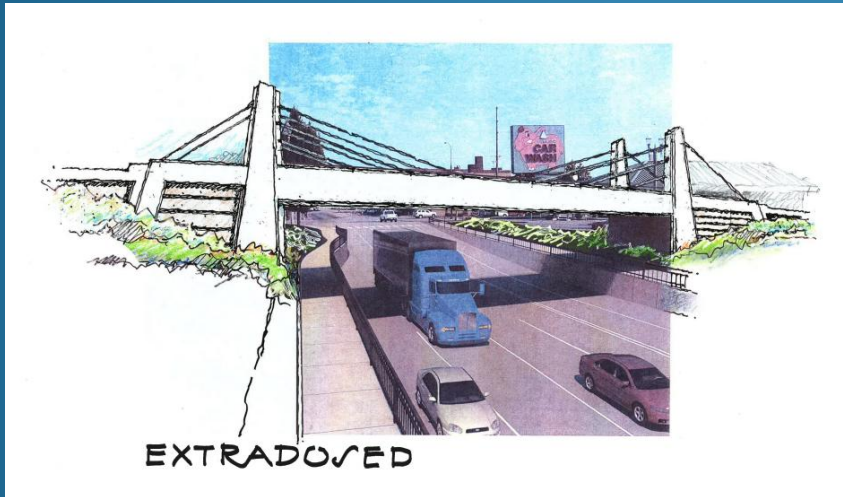
Alternatives Cont'd

- Single Span Pony Truss



Alternatives Cont'd

- Single Span Extradosed

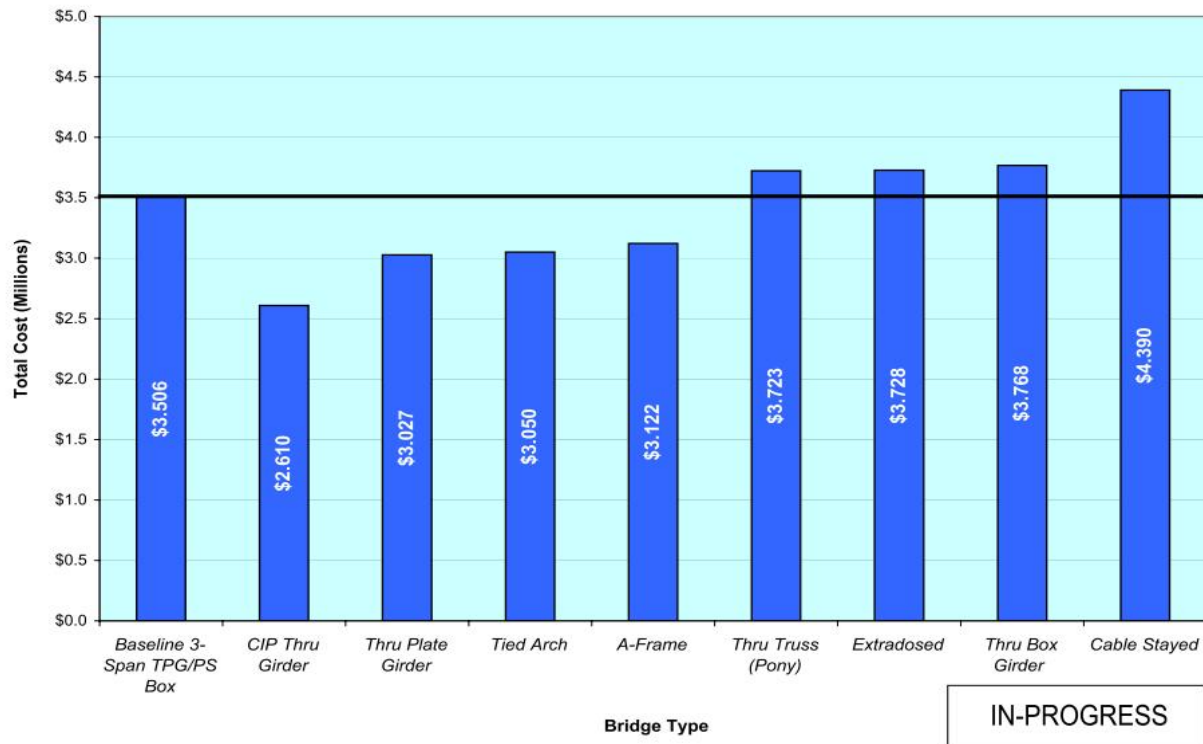


Bridge Type Cost Comparison

Sound Transit
D to M Street Track and Signal Project

Parsons Brinckerhoff, Inc.
September 2008

Bridge Type Cost Comparison



Structure Type Evaluation Matrix

A weighted criteria approach was taken using the following categories:

- a) *Aesthetics*
- b) *Impact to Roadway Profile*
- c) *Gateway Potential*
- d) *Cost*
- e) *Schedule*
- f) *Structural Behavior*
- g) *Constructability*
- h) *Durability*
- i) *Inspection and Maintenance*
- j) *Geotechnical / Foundations*

Weighting ranged from 1 – 5:

- 1 – Does not meet minimum criteria
- 2 – Meets minimum criteria
- 3 – Exceeds criteria
- 4 – Clearly exceeds criteria
- 5 – Significantly exceeds criteria

Structure Type Evaluation Matrix

D to M Street Track and Signal Project STRUCTURE TYPE EVALUATION MATRIX

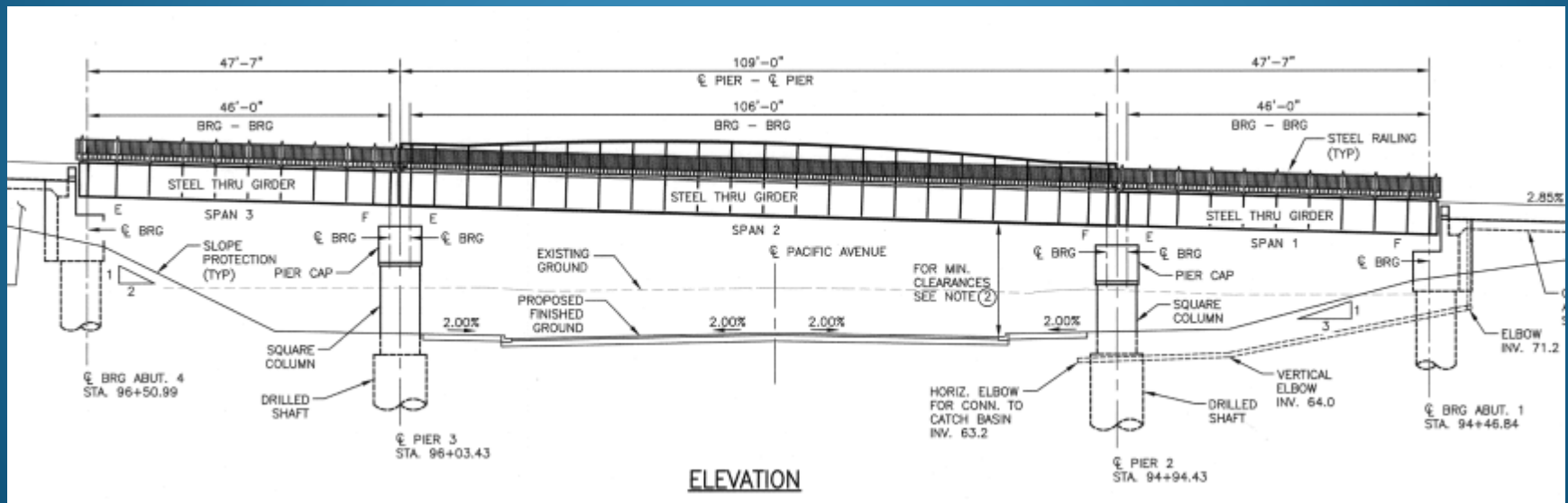
Criteria	Score Weight	STRUCTURE TYPE																	
		Baseline 3-span		A-Frame		Steel Through Girder		Concrete Through Girder		CIP Through Girder		Cable Stayed		Extradosed		Tied Arch		Through Truss	
Aesthetics	4																		
Impact to Roadway Profile	4																		
Gateway Potential	3																		
Cost	5																		
Schedule	3																		
Structural Behavior	2																		
Constructability	3																		
Durability	2																		
Inspection / Maintenance	3																		
Geotech / Foundation	2																		
Total Score			0		0		0		0		0		0		0		0		0
Ranking																			

- 1 - Does not meet minimum criteria
- 2 - Meets minimum criteria
- 3 - Exceeds Criteria
- 4 - Clearly Exceeds Criteria
- 5 - Significantly Exceeds Requirements

Highest score indicates most preferred structure type

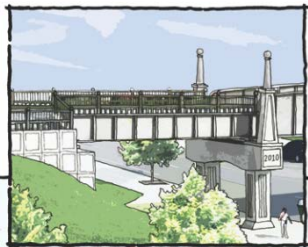
Final Alternative Selection

- The single span Thru Plate Girder was preferred based on:
 - Least cost
 - Most constructible
 - Least impact to roadway
- Ultimately due to urban design concerns in the downtown area a 3-span TPG structure was selected.



Public Workshops (July 2009)

REVISED "CLASSIC" BRIDGE ENHANCEMENT CONCEPT



"Classic" Concept is Preferred Concept for Final Design

- The concept incorporates elements that echo Brewery District historic character
- Column shape and pier cap reminiscent of historic architecture in the area
- Railing has simple, regular pattern
- Walls have repeating classical "coffer" pattern

Concept Refinements After Bridge Workshop #1

- The pilasters are taller and topped by globes to mark ends of center bridge span
- Column bases were reduced in size



OPTIONAL PILASTER CONCEPT



 **SOUNDTRANSIT**
RIDE THE WAVE

NIGHT LIGHTING CONCEPT

- Bridge spans are lit to provide downtown gateway and to accentuate the bridge architecture
- The sidewalks and bridge substructure are brightly lit for visibility and safety



 **SOUNDTRANSIT**
RIDE THE WAVE

Aesthetic Studies



Color, Railing Type, and
Surface Treatments



Aesthetic Lighting

Pacific Ave Bridge - Rendering



Pacific Ave Bridge - Photo



Pacific Ave Bridge Characteristics

- Steel through plate girder superstructure with reinforced concrete ballast pan
 - 106' Main Span with 11'-3" deep plate girders
 - 46'-0" Approach Spans with 5'-4" deep plate girders



Pacific Ave Bridge Characteristics

- Piers
 - Reinforced concrete cap on 5'-6" square columns
 - 8'-0" diameter drilled shafts



Pacific Ave Bridge Characteristics

- Abutments
 - Reinforced concrete cap on 6'-0" diameter drilled shafts

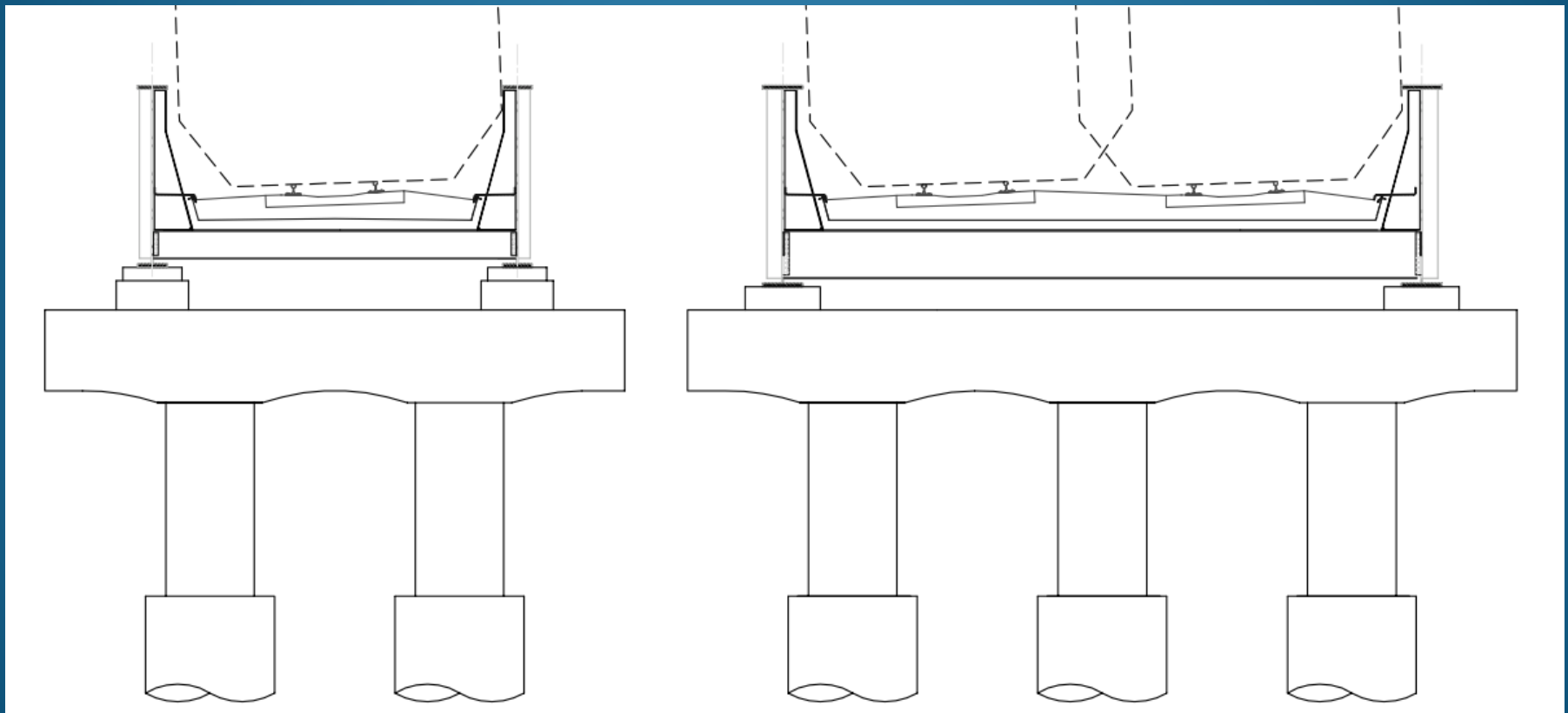


Design Challenges

- Substructure design must accommodate initial single track and future double track superstructures
 - Initial single track for Sound Transit's Sounder commuter train
 - Future additional track for Amtrak passenger train
- Liquefaction potential in 10' layer of soil overlain by 30' of fill
 - Downdrag on drilled shafts due to overlying material
 - Balance ductility with rail structure stiffness requirements

Designing for Future 2nd Track

- Two column/shaft substructure designed for eventual third symmetrical column/shaft



Initial - Single Track

Final - Two Tracks

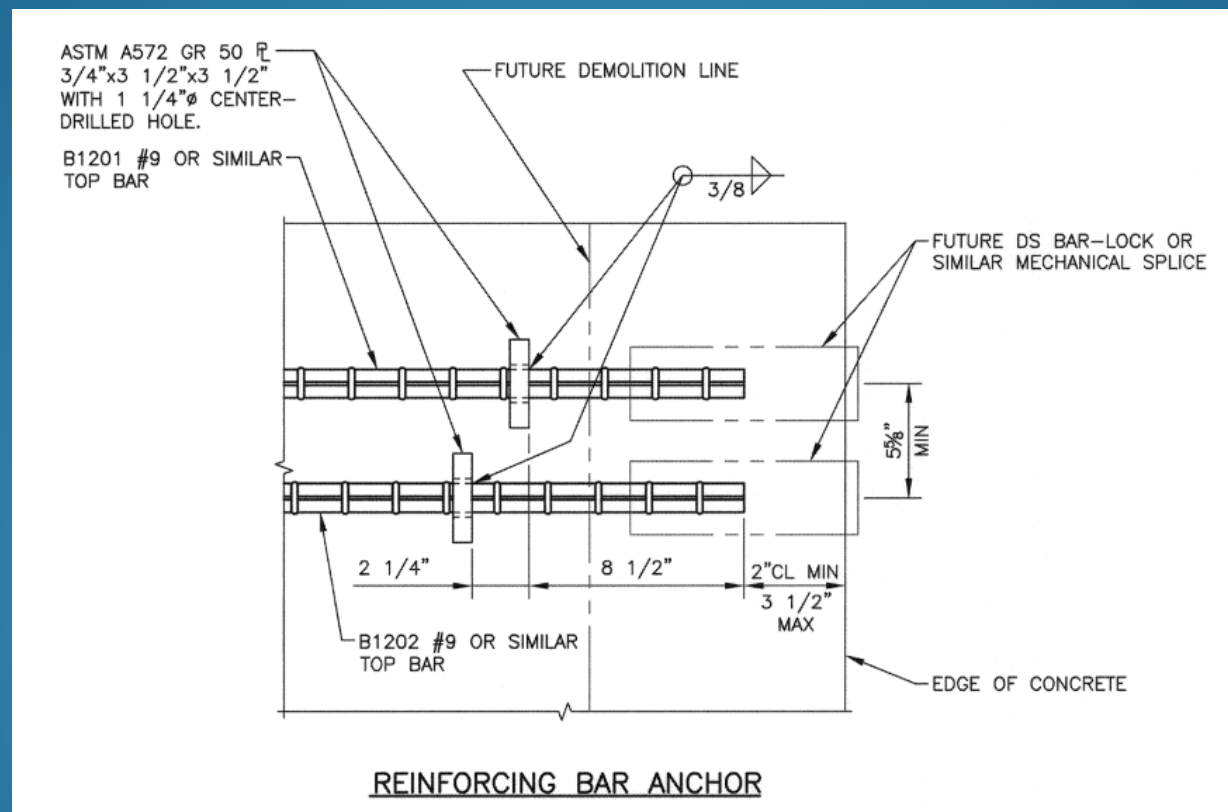
Designing for Future 2nd Track

- Top of bent elevations established for two-track superstructure
 - Floorbeams 70% greater in height for future structure
 - Bearings 70% greater in height for future structure
 - Temporary pedestals for initial structure elevation

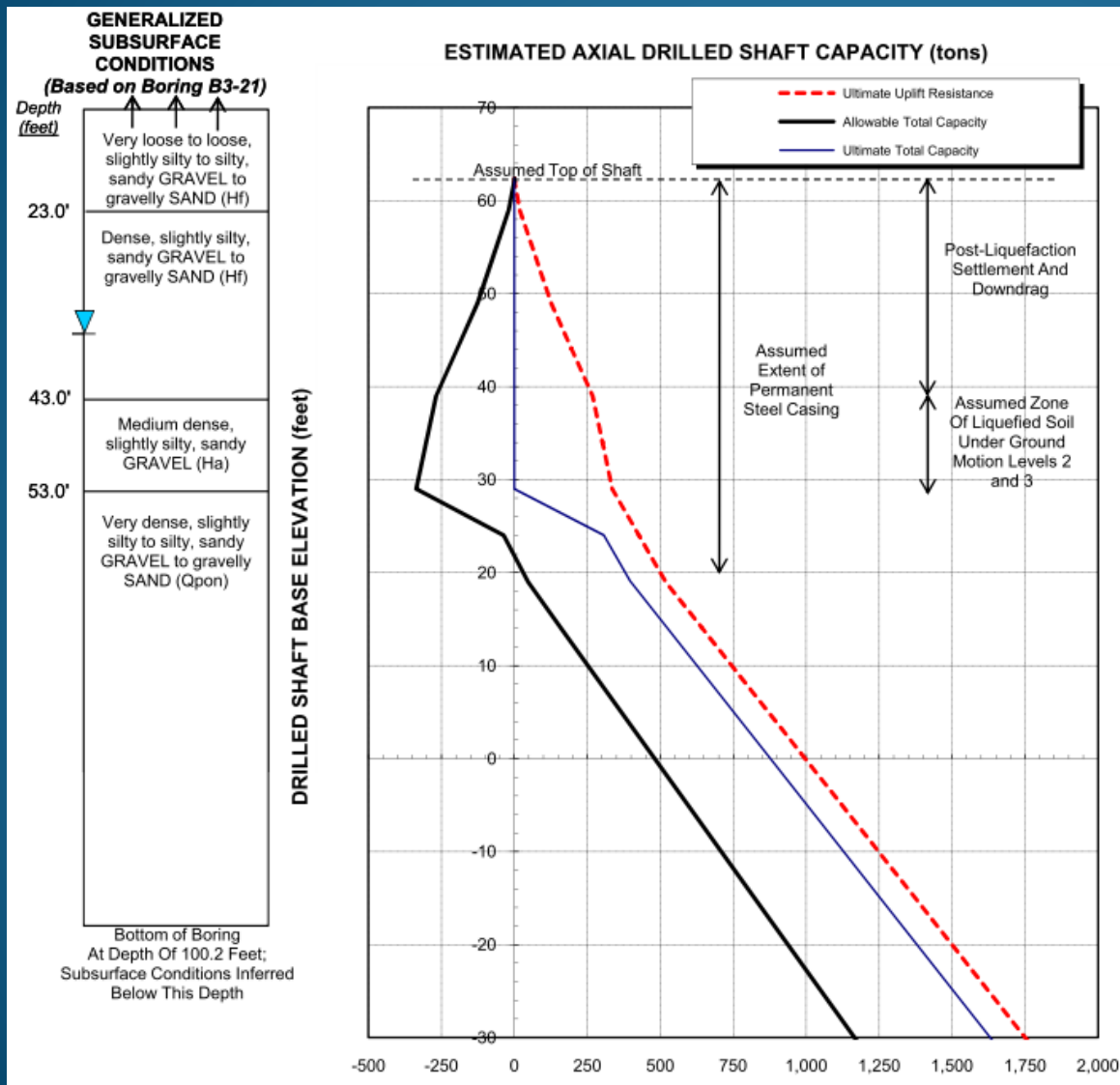




Designing for Future 2nd Track

- Cap reinforcement designed with internal headed anchorages to minimize service disruption during cap extension



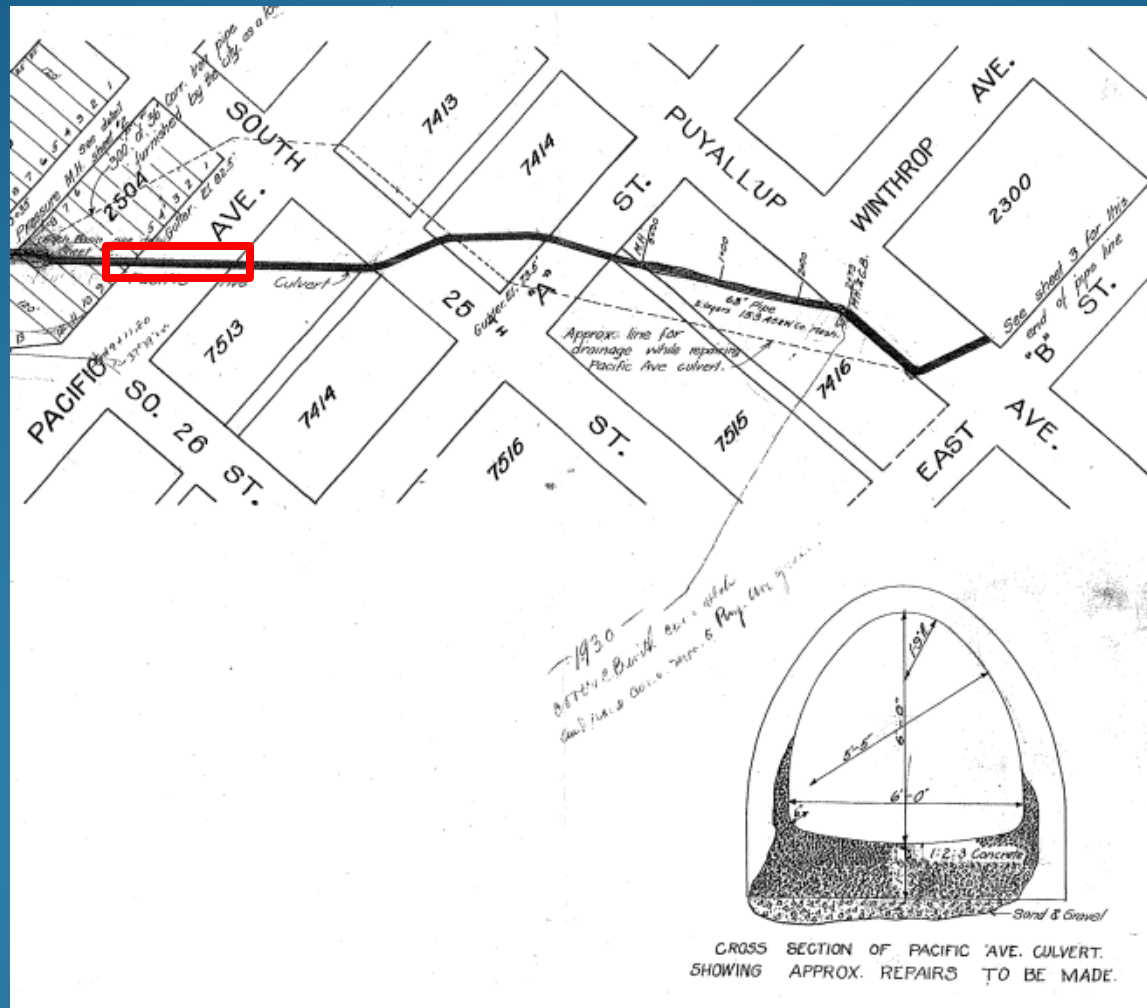
Liquefaction Hazard



- 
Post-Liquefaction Settlement and Downdrag
- 
Zone of Liquefied Soil
- Drilled shafts designed for additional 600 kip downdrag burden
- 45' permanent steel casing required for drilling

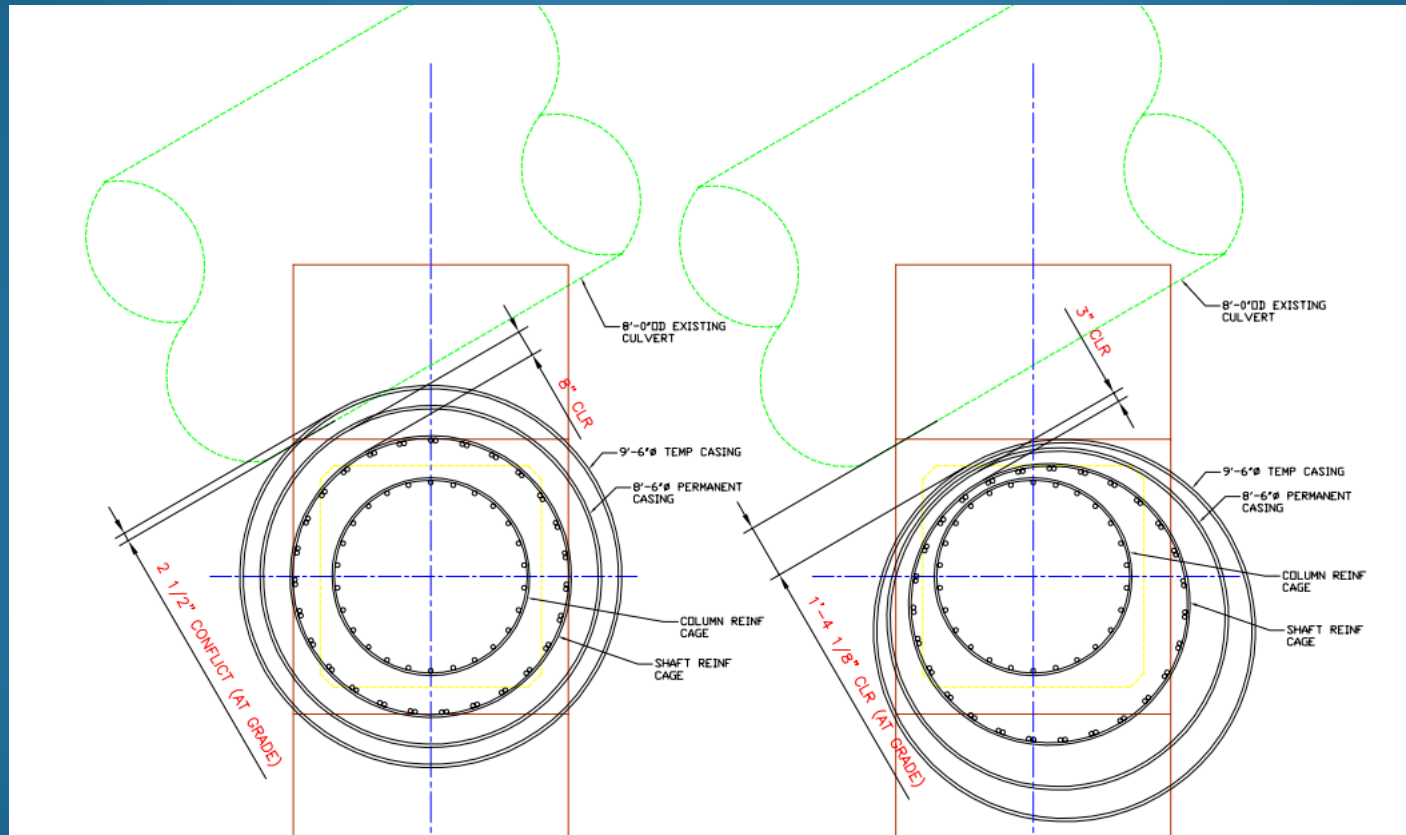
Pier 3 Drilled Shaft Conflict

- 72" diameter culvert 30' below grade at pier 3



Pier 3 Drilled Shaft Conflict

- Larger auger size vs. tolerance for plan location and plumbness for shaft resulted in potential conflict
- Explore shaft construction tolerance to avoid culvert



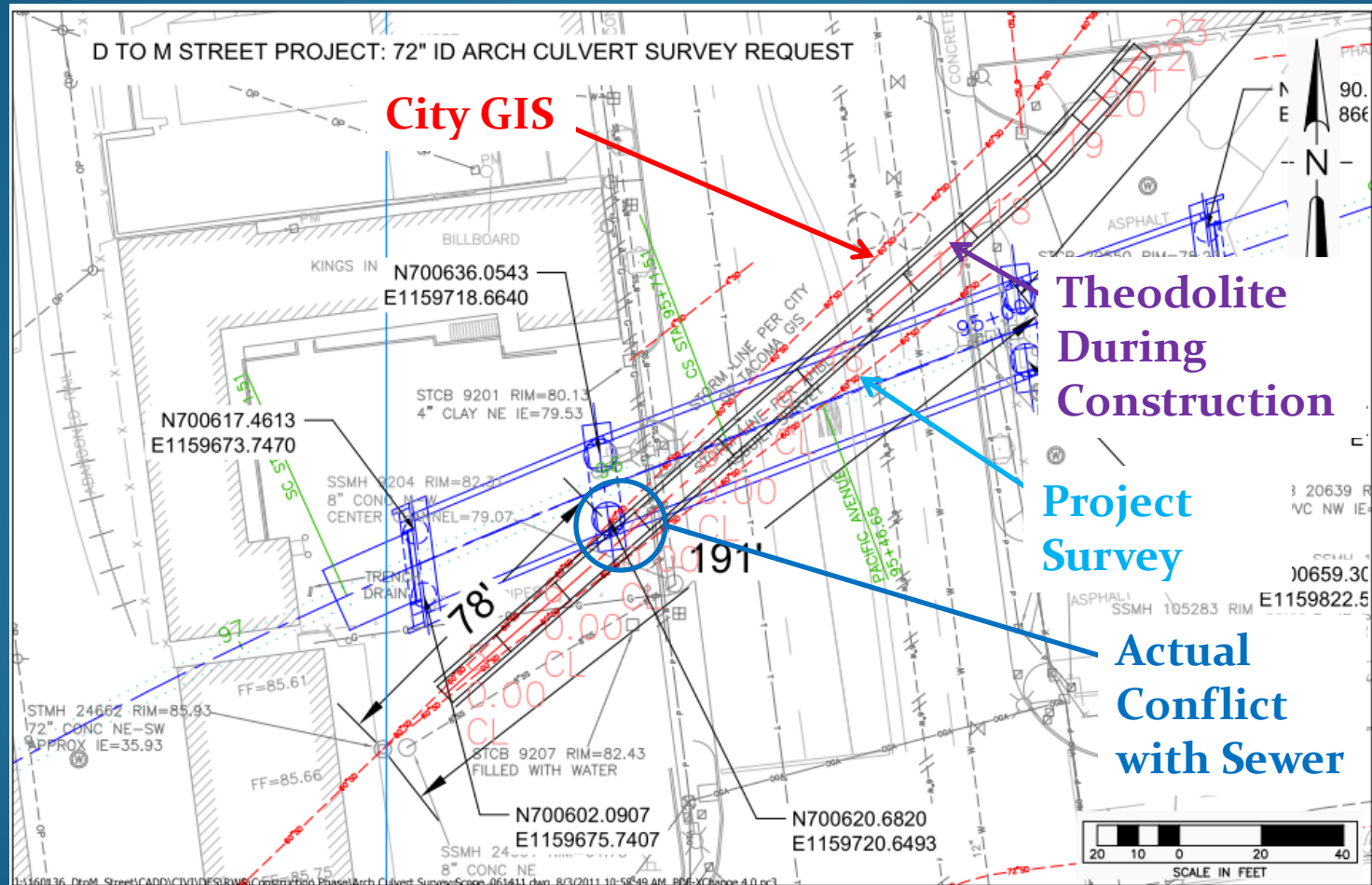
Pier 3 Drilled Shaft Conflict

- Culvert still too close for comfort. Eventual use of a gyroscopic theodolite below surface provided the desired confidence in location



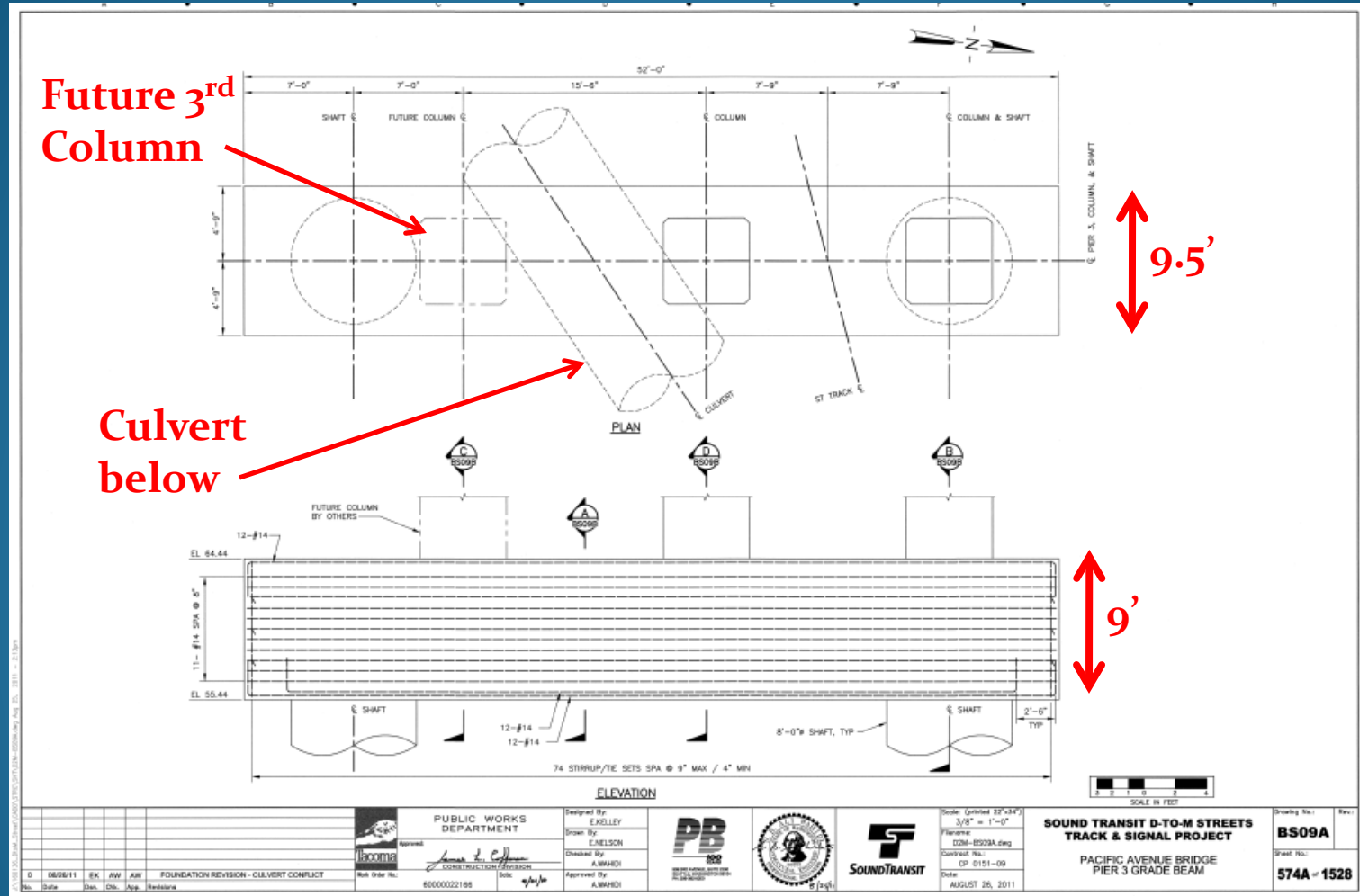
Pier 3 Drilled Shaft Conflict

- City GIS vs. surface survey vs. gyroscopic theodolite survey
- Theodolite investigation revealed actual conflict at Pier 3



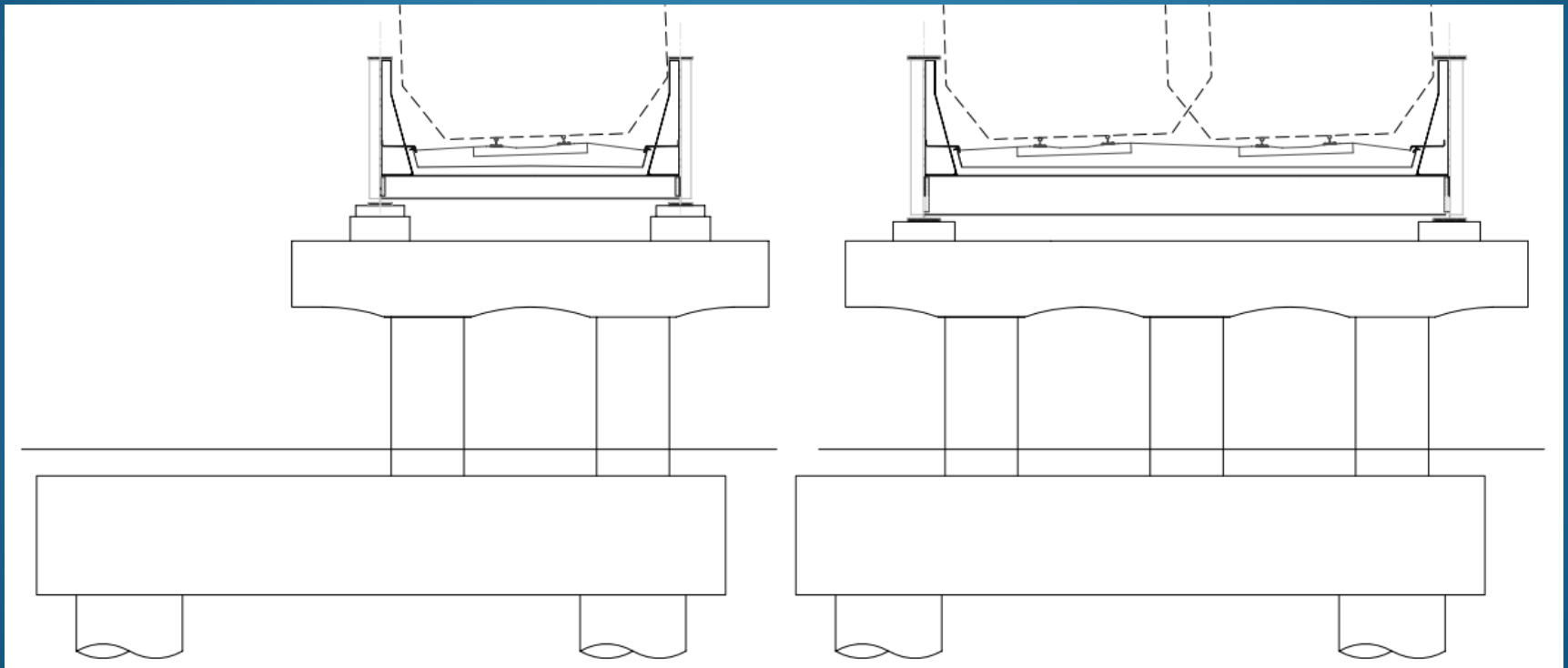
Pier 3 Drilled Shaft Conflict

- Redesign pier 3 using grade beam to avoid culvert



Pier 3 Drilled Shaft Conflict

- Design revision utilized existing 8' diameter drilled shaft reinforcing cages.
- Reinforcing cages were extended approximately 50' using mechanical couplers



Initial - Single Track

Final - Two Tracks

Pier 3 Drilled Shaft Conflict

- Excavation for grade beam installation



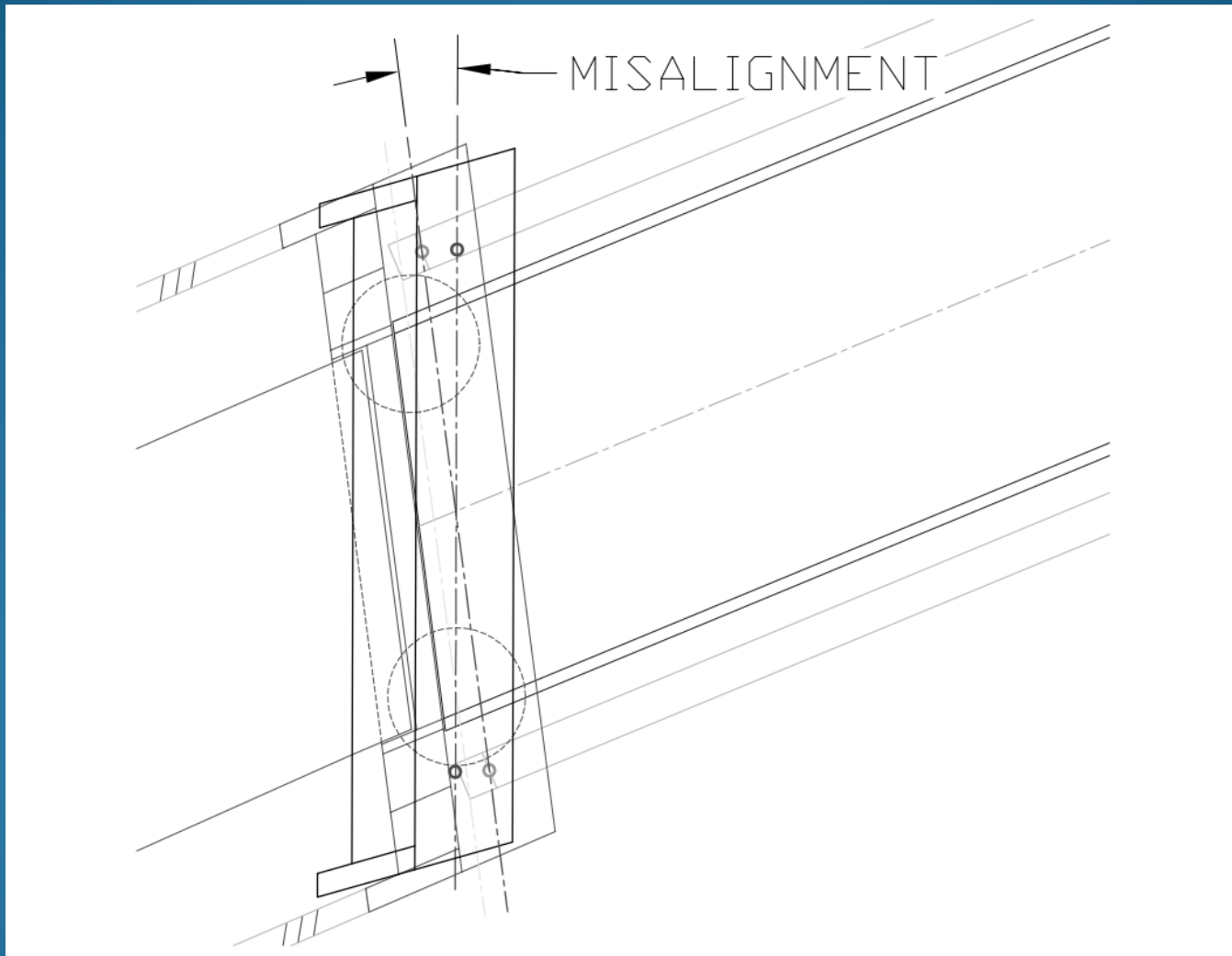
Pier 3 Drilled Shaft Conflict

- Shaft and grade beam reinforcing



Abutment Misalignment

- Bent 4 placed incorrectly

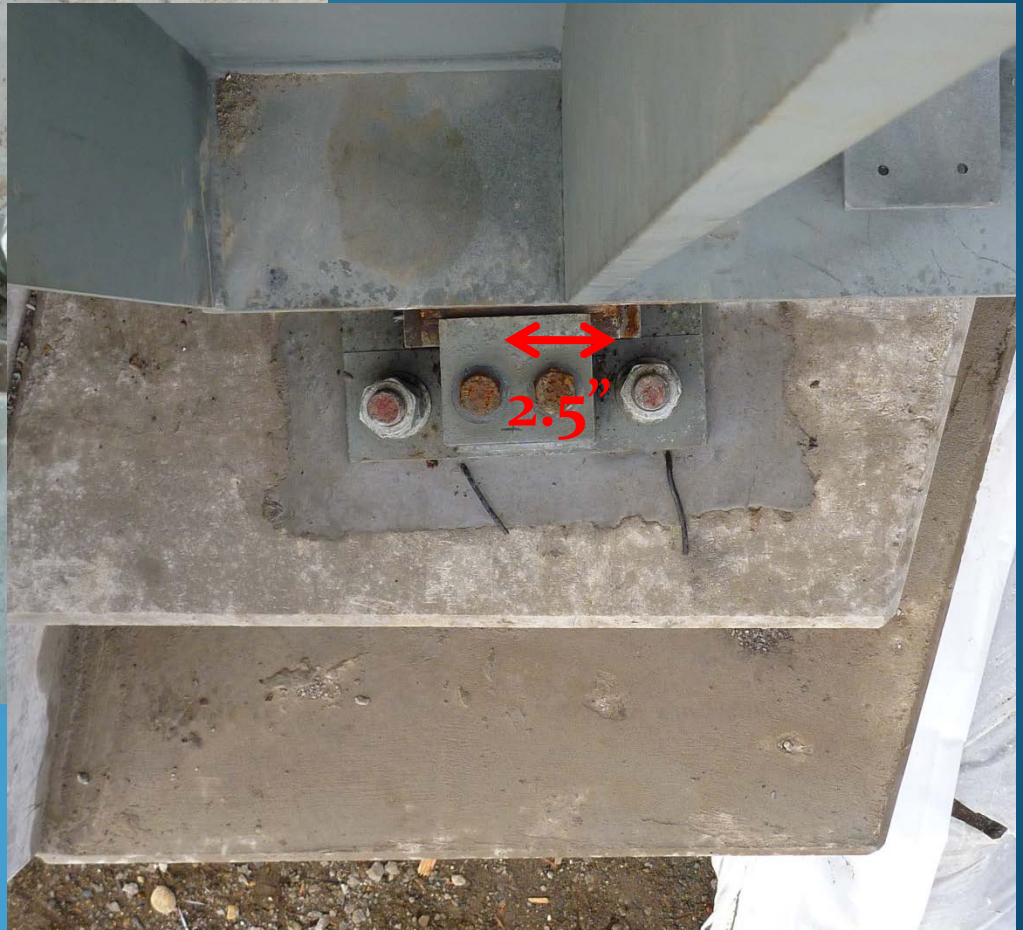


Abutment Misalignment

- Abutment 4 bearing stiffeners offset from bearing



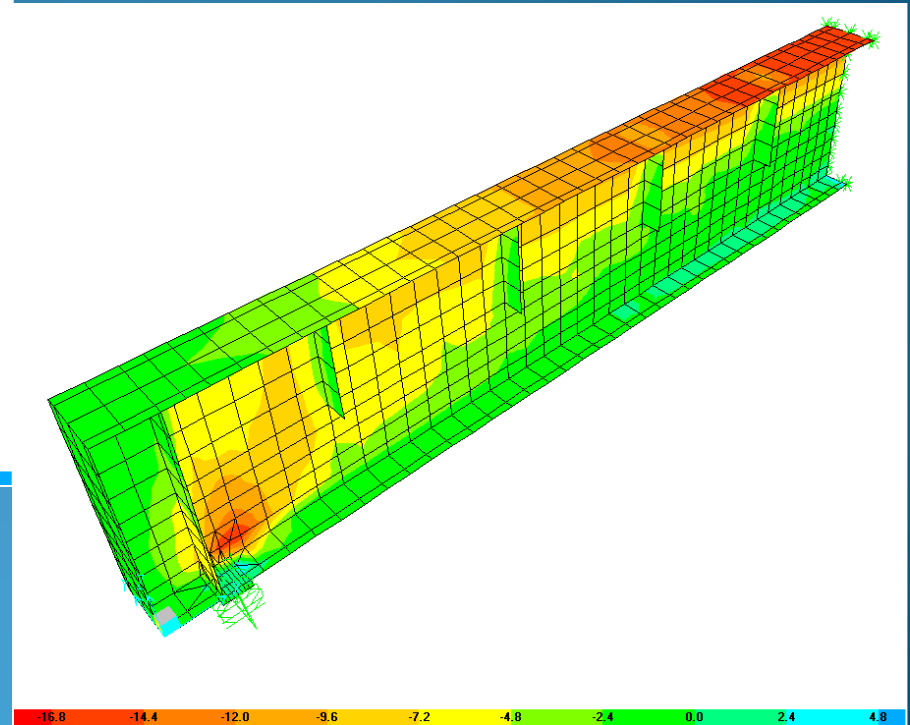
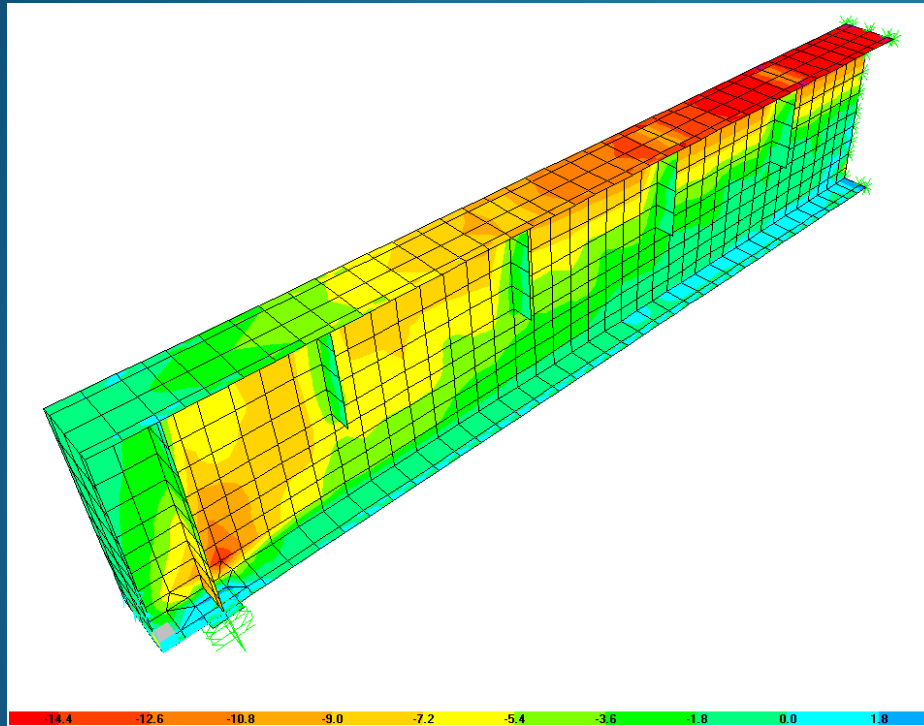
North Misalignment



South Misalignment

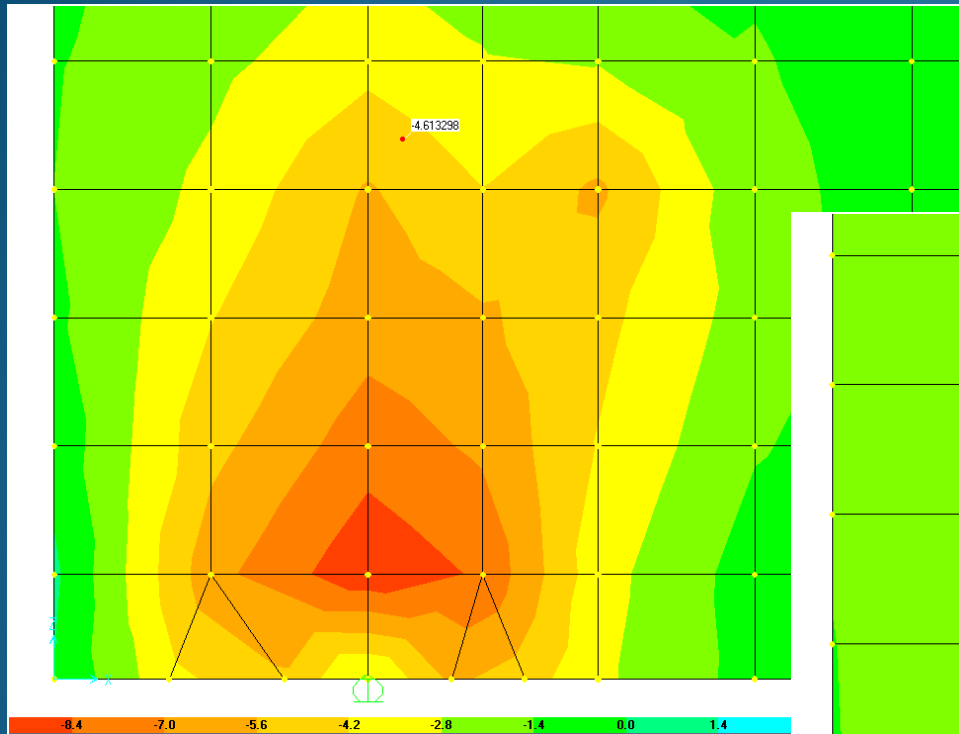
Abutment Misalignment

- Web stress comparison between design and as-constructed for north girder



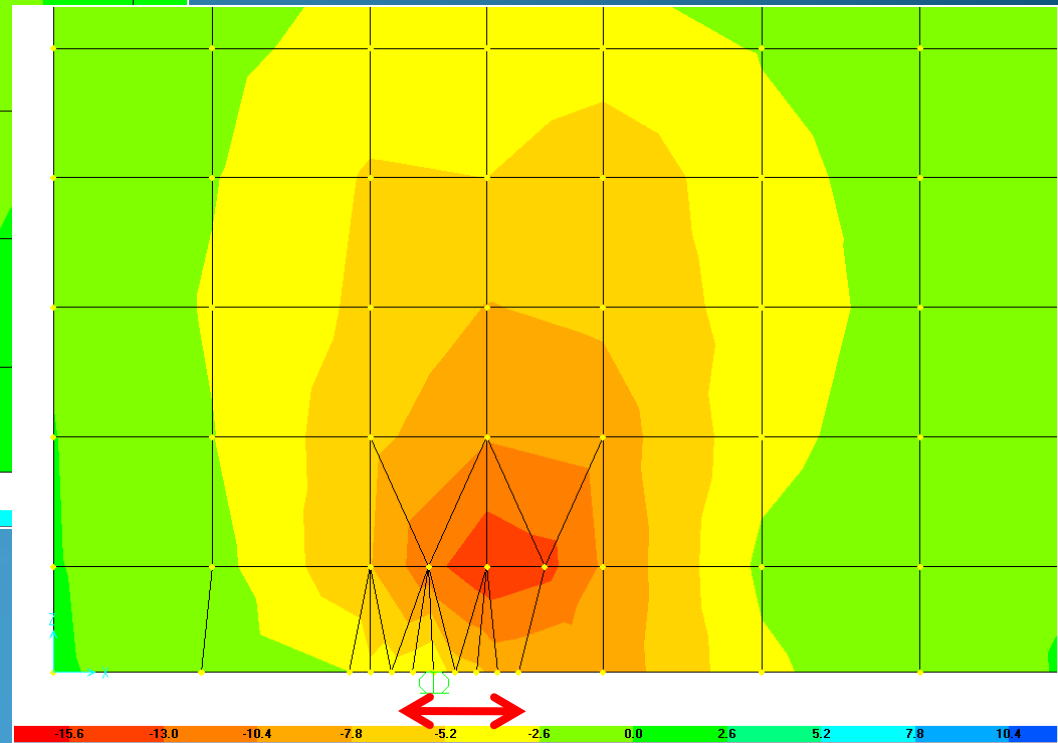
Abutment Misalignment

- Web Compressive Stress Detail



9.5 ksi Design Stress
(Aligned)

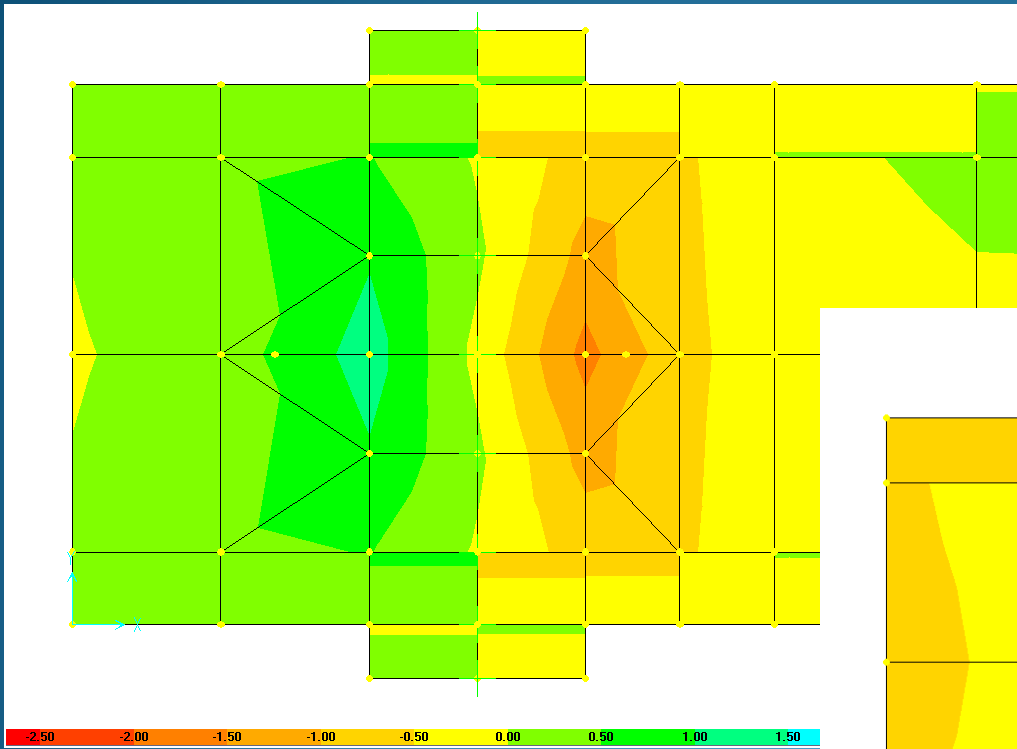
15.1 ksi As Constructed
(Misaligned 3")



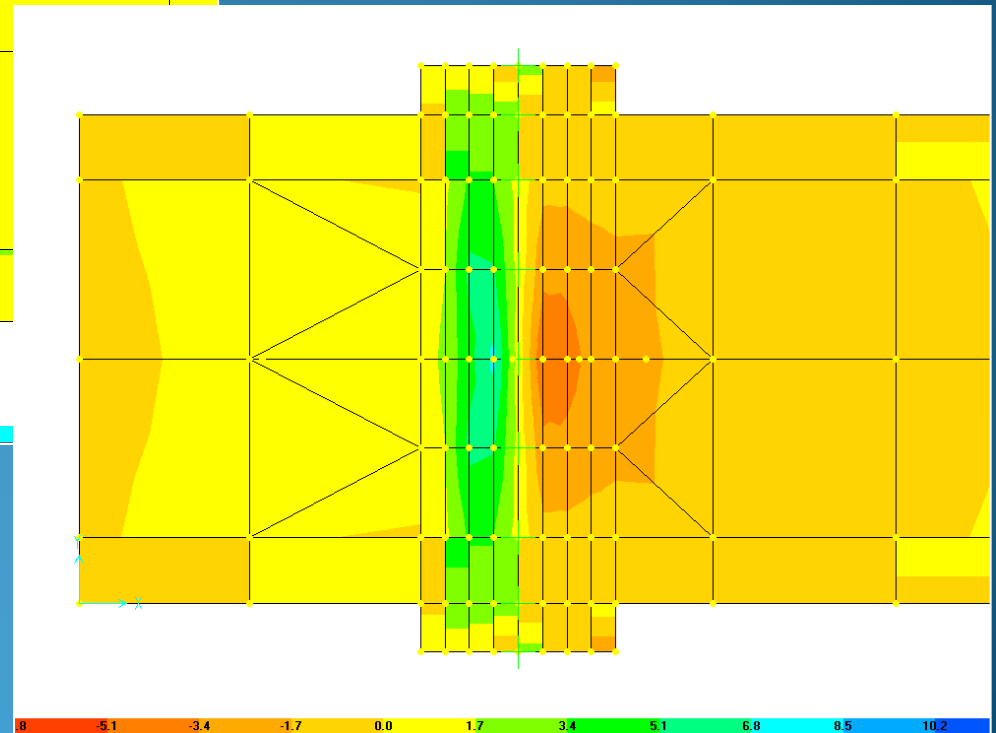
17.5 ksi Allowable Okay

Abutment Misalignment

- Rocker Plate Weld Stress Investigation

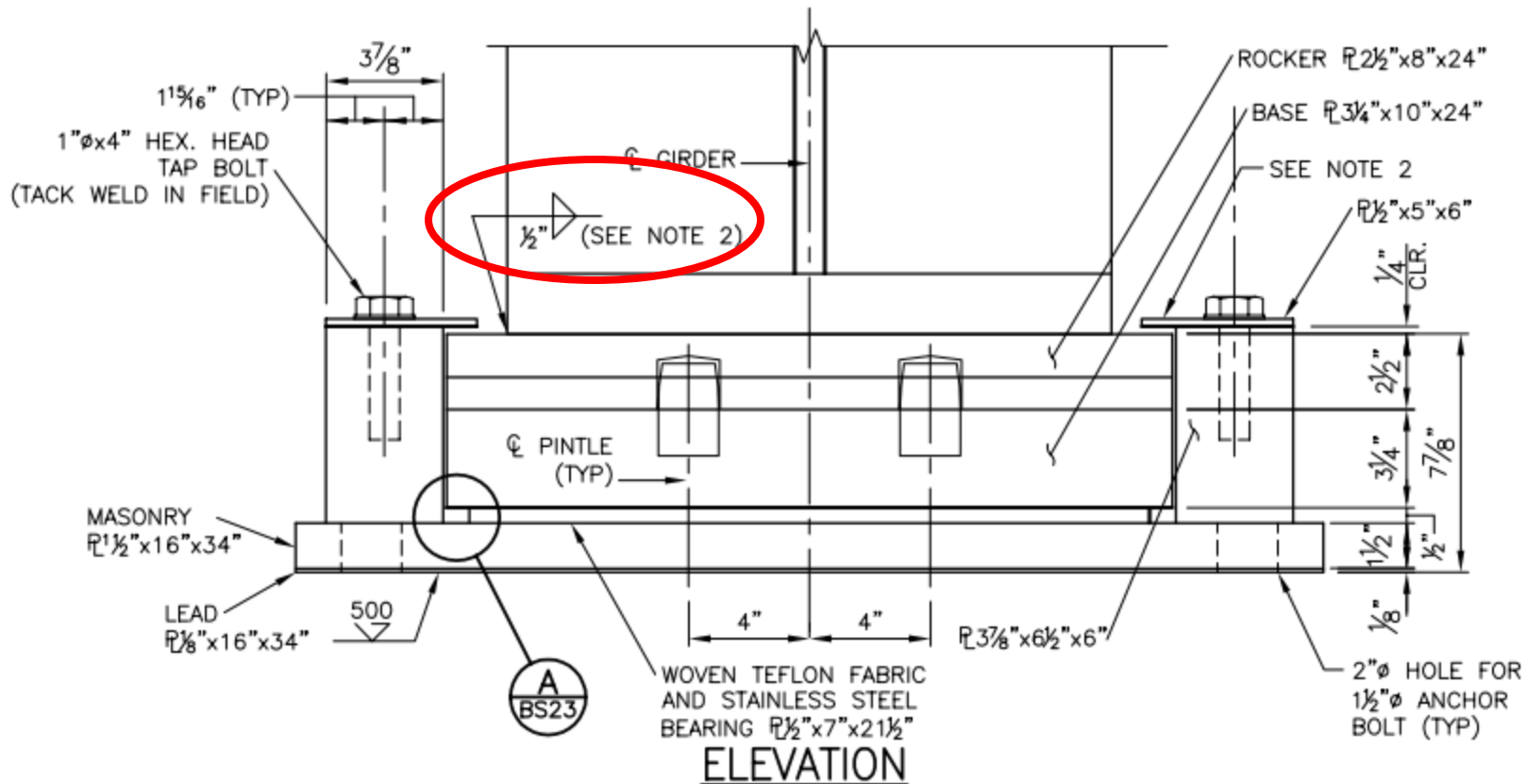


Misalignment created increase in weld stress for fatigue loading



Abutment Misalignment

- Increase flange to rocker plate weld size to $\frac{3}{4}$ "



2. AT ABUTMENT 4, GIRDER "F" & "E", TRIM THE BEARING KEEPER PLATES $\frac{1}{2}$ " AND INCREASE THE SIZE OF THE LONGITUDINAL WELDS BETWEEN THE BOTTOM FLANGE OF THE GIRDER AND THE ROCKER PLATE FROM $\frac{1}{2}$ " TO $\frac{3}{4}$ ".

Pacific Ave Bridge - Preconstruction



Pacific Ave Bridge - Construction



Pacific Ave Bridge - Final



Thanks to:

- Sound Transit
- Parsons Brinckerhoff
- D to M Streets Team:
 - Shannon & Wilson
 - Cosmopolitan Engineering
 - AHBL
 - GHIL
 - Enviroissues
 - William Ott Construction Consultants

Questions?

