Presentation to:
2013 Western Bridge Engineers' Seminar
Bellevue, Washington
September 5th, 2013

Speakers: Nicholas Cioffredi, PE Frank Block, PE

DIEFENBAKER BRIDGE, PRINCE ALBERT,

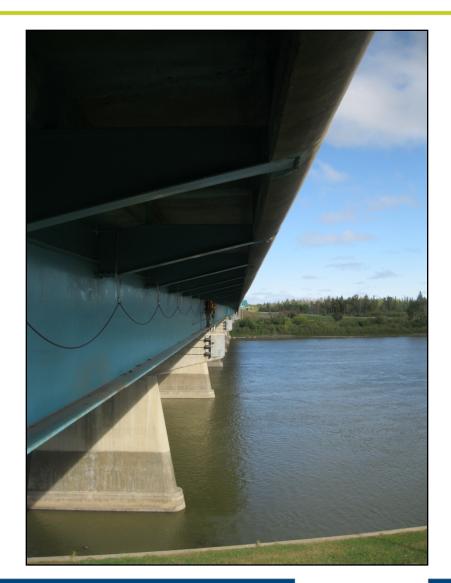
SK

FRACTURE INVESTIGATION & REPAIR



Agenda

- Structure Overview
- Observation
- Emergency Response
- Rope Access Investigation
- Verification of Detail
- Fracture Retrofit
- Preventative Mitigation



Structure Overview

Parallel Twin 6 ½ foot Girders on Common

Substructure

- 7 Span
- 1000 ft
- Fracture Critical
- Non-Composite
- Year Built 1959
- HS20-S16-44Design Loading
- A373-56T Steel



Structure Overview

- Prince Albert is SK 3rd Largest City
- Hwy 2 is Major Arterial
- North SK River is
 Historic Fur Trade
 Waterway
- Nearest Crossing –
 ~125 miles

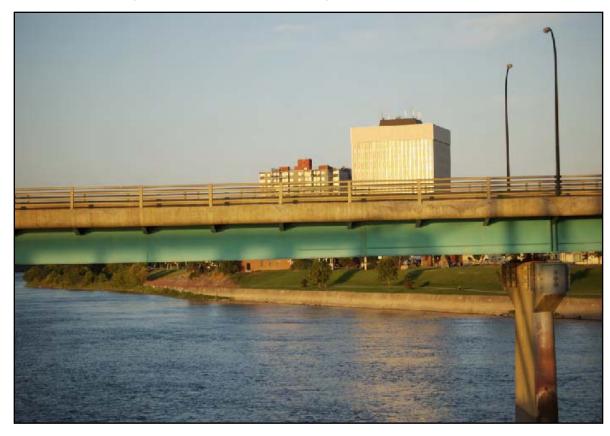


Structure Overview

- Structure Vital to Industry & Tourism
 - Agriculture
 - Forestry
 - Tourism
 - Hunting
 - Fishing
 - Mining
 - Diamonds
 - Uranium
 - Forestry



- August 29th, 2011
- What would you think if you looked up
 - and saw this?
 - Notify Police!











Emergency Response Scope of Work

- Close SB Bridge/Restrict NB
- Phase I
 - Make Travel Arrangements
 - Review Permits/Inspection Reports
 - Survey Monitoring
 - Initial Analysis for Stability and Safety
- Phase II
 - Rope Access Arm's Length Inspection & NDE
 - 3D FEA
 - Load Transfer, Continuity

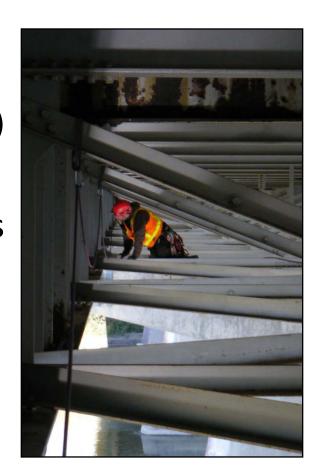


Emergency Response Scope of Work

- Phase III
 - Determine Cause
 - Design Major Repair
 - Implement / Open to Traffic
- Phase IV
 - Risk Management Strategy
 - Design Preventative Repair
- Phase V
 - Long Term Program Strategy

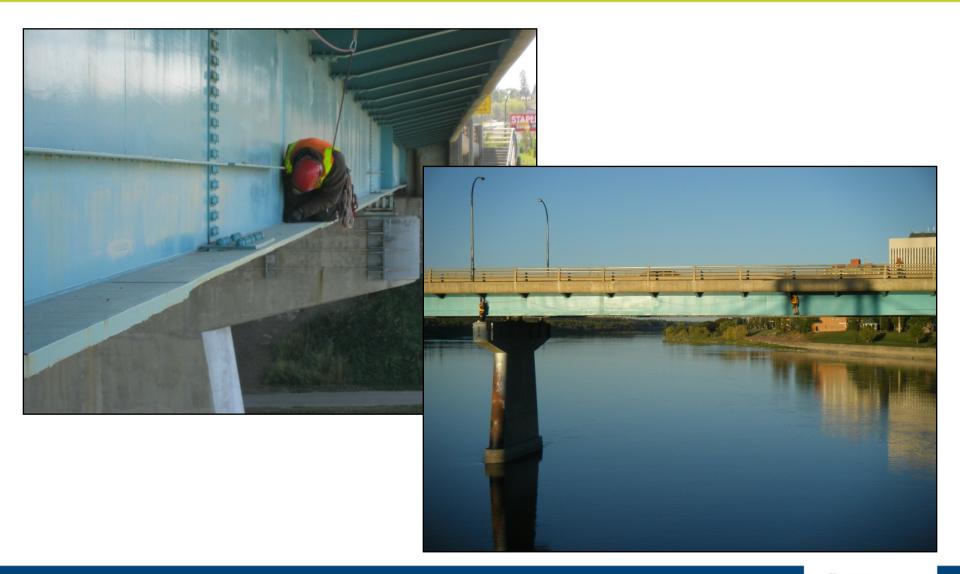


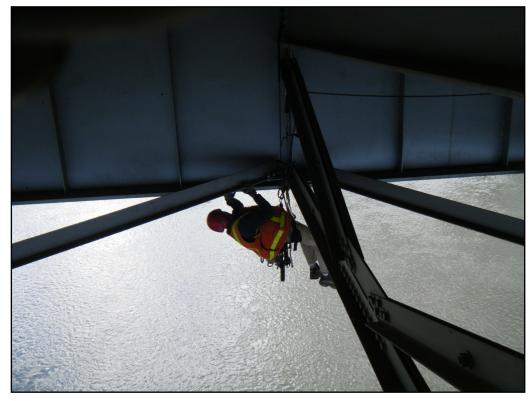
- 3D FEA proved
 - Structure stable
 - No vehicular loading allowed (obvious)
- Rope Access was only choice
- Team of 4 SPRAT Certified Engineers
- Lead Climbing/Belay Techniques
- In-Depth Inspection
- Less than Arm's Length at Critical Detail
- NO JUMPING!

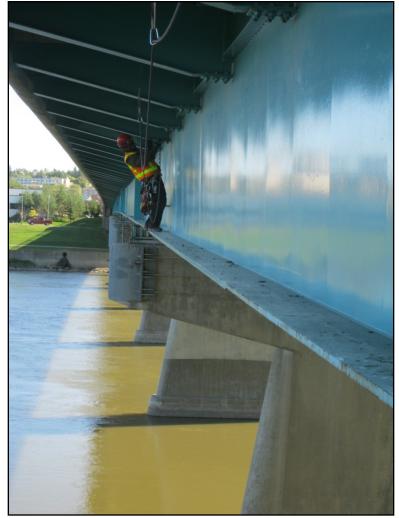




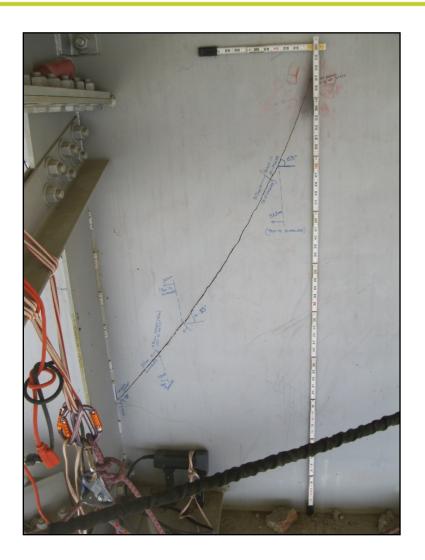






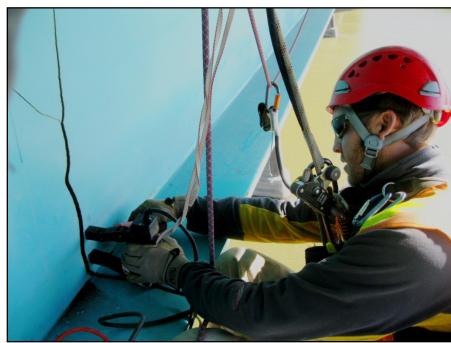




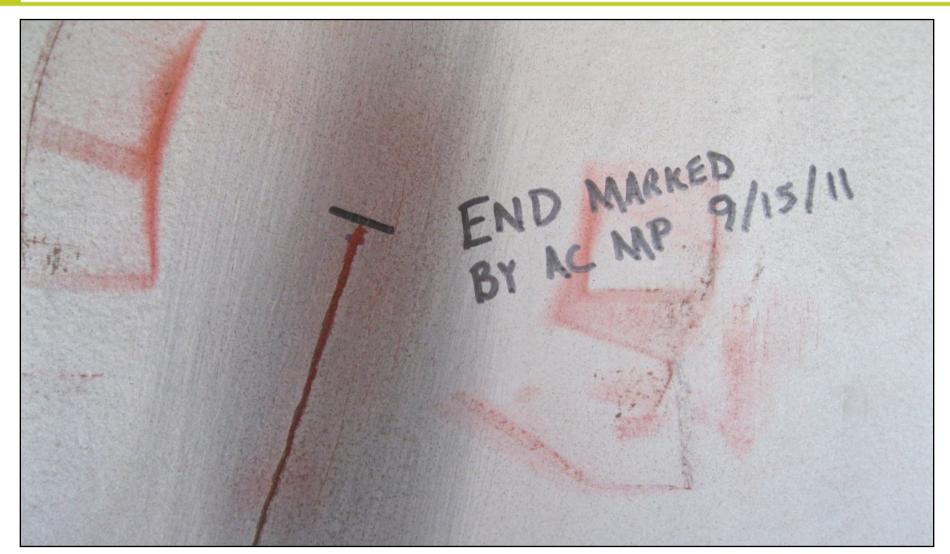










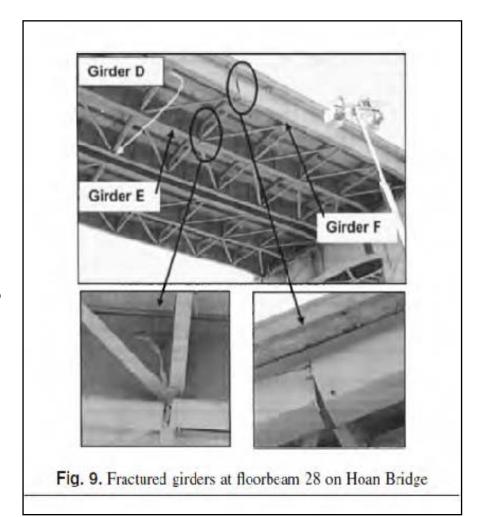








- Hoan Bridge Failure
 - Milwaukee, WI
 - Dec 13, 2000
- Fracture at Gusset Plate
- Detailed Study (Fisher)
- Highly Constrained Stress
- Intersecting Welds
- Crack Like Geometry
- No Fatigue Growth





- US 422 Bridge
 - Schuylkill River
 - Pottstown PA
 - May 20, 2003
- Fracture at Gusset Plate
- Detailed Study (Connor)
- Highly Constrained Stress
- Intersecting Welds
- No Fatigue Growth
- Partial Height Web Crack

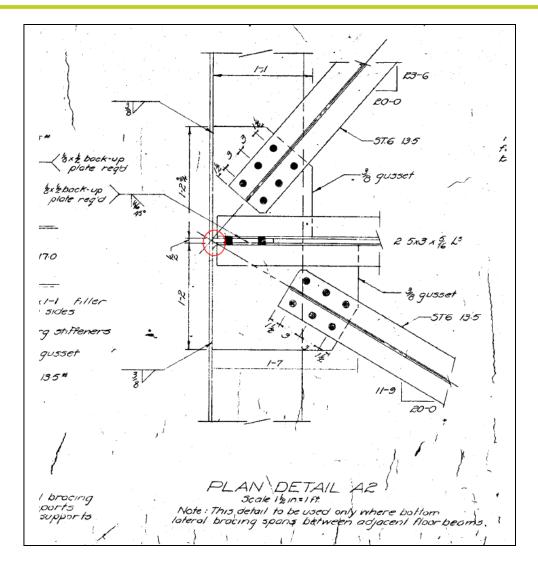


- Diefenbaker Bridge
 - Overwhelming Similarities
- Fracture at Gusset Plate
- Gussets Connected via Vertical Stiffener
- Gusset-to-Web, Top Fillet
 Only

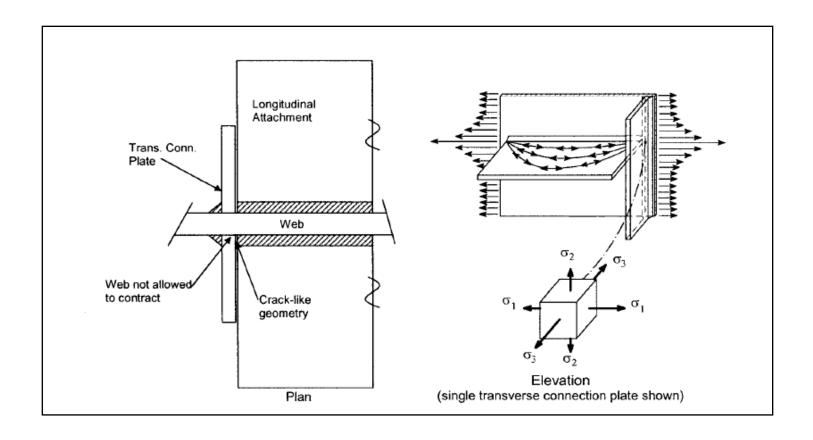


Vertical Stiffener Stitch Welded Above, Cont. Below GP

- Little Fatigue Growth
- Highly Constrained
 Stress
- Intersecting or Nearly
 Intersecting Welds
- Brittle Fracture ...
- CONSTRAINT INDUCED FRACTURE (CIF)
- Not Fatigue

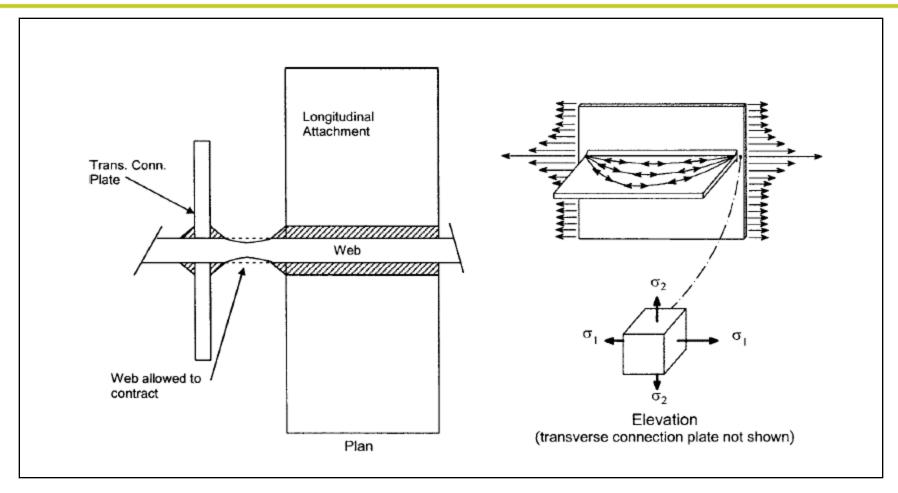






Insufficient Yielding Allowed by Small Web Gap





Sufficient Yielding Allowed by Larger Web Gap



Alberta Transportation

- Repairing Steel Bridges with CIF Potential
- Several CIF Structures Repaired
- Procedures Developed
 - Remove & Replace Section of Girder at Midspan
 - Splice In New Section
 - Bridge to be Open By December 23
 - Less Than 4 mths from Discovery

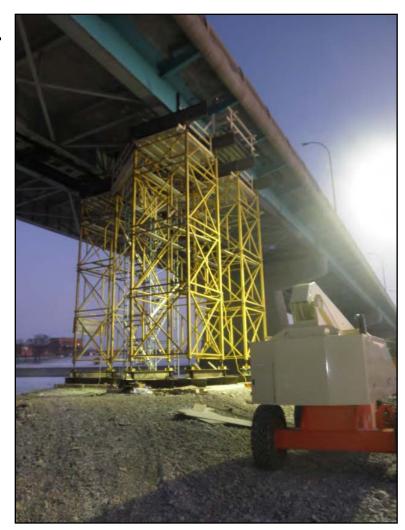


- Mid-Winter Retrofit in Northern Canada
 - Engineering
 - Permitting
 - Berm Design
 - Construction
 - Tower Erection
 - Jacking
 - Repair
 - Load Testing/Monitoring
- 3 Months For A Christmas Present!



Fracture Repair Procedures

- Support Structure From River Berm
- Remove Web & Bottom Flange
- Pre-determined Load & Displacement Graph
- Constant Monitoring of Strains
- Load Testing after Splice in Place





Not Unless You Have To!











NATIONAL COOPERATIVE HIGHWAY RESEARCH PROGRAM

Inspection and Management of Bridges with Fracture-Critical Details

A Synthesis of Highway Practice

TRANSPORTATION RESEARCH BOARD
OF THE NATIONAL ACADEMIES

Prevention and Mitigation Strategies to Address Recent Brittle Fractures in Steel Bridges

Robert J. Connor, M.ASCE¹; Eric J. Kaufmann²; John W. Fisher, Hon.M.ASCE³; and William J. Wright, M.ASCE⁴

Abstract: Brittle fracture results in unplanned loss of service, very costly repairs, concern regarding the future safety of the structure, and potential loss of life. These types of failures are most critical when there is no evidence of fatigue cracking leading up to the fracture and the fracture origin is concealed from view. Hence, the failure occurs without warning and the details are, essentially, noninspectable. In these cases, it appears desirable to take a proactive approach and introduce preventative retrofits to reduce the potential for future crack development. These efforts will help ensure that the likelihood of unexpected fractures is minimized. This paper examines the behavior of two bridge structures in which brittle fractures have developed in recent times, discusses the causes of the failures, and offers suggested design strategies for prevention and retrofit mitigation techniques. In situations where considerable uncertainty exists in the prediction of accumulated damage or in the ability to reliably inspect critical details, preemptive retrofit strategies appear to be highly desirable.

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CE Database subject headings: Fracture; Fatigue; Bridge failure; Forensic engineering.

Introduction

Compared to fatigue cracking, the number of brittle fractures in highway bridges has been relatively small over the past 40 years (Connor et al. 2005). However, brittle fracture results in unplanned loss of service, very costly repairs, concern regarding the future safety of the structure, and potential loss of life. These types of failures are most critical when there is no evidence of fatigue cracking leading up to the fracture and the fracture origin is concealed from view. The failure occurs without warning and the details are essentially noninspectable.

Field instrumentation and in-service monitoring is a very useful tool in estimating the remaining fatigue life in a bridge. However, for the fracture limit state, many details are very difficult to inspect and instrumentation cannot provide the needed information to make a meaningful evaluation. In these cases, it appears desirable to take a proactive approach and introduce preventative retrofits to reduce the potential for future unstable crack development. These efforts will help ensure that the likelihood of unexpected fractures is minimized.

This paper examines the behavior of two bridge structures in

which brittle fractures have developed in recent times, discusses the causes of the failures, and offers suggestions for mitigation techniques. In situations where considerable uncertainty exists in the prediction of accumulated damage or in the ability to reliably inspect critical details, preemptive retrofit strategies appear to be highly desirable.

Constraint-Induced Fracture

In many cases, brittle fractures in highway bridges have been preceded by fatigue crack growth that eventually reached a critical size (Fisher 1984). However, the absence of stable crack growth at the fracture origin in both of the case studies discussed herein confirmed that fracture was not due to the presence of a large fatigue crack that subsequently became unstable. In both cases, fracture was attributed to what is referred to as constraint-induced fracture (CIF).

In highway bridges and other welded structures, details susceptible to high levels of triaxial constraint are typically avoided through good detailing. However, in some structures, large welds connecting multiple plates cannot be avoided and special care is taken during fabrication (i.e., preheat, inspection, etc.) to ensure robust performance. In cases where thick plates have been welded to form complex joints, brittle fractures have been observed after fabrication is complete or shortly after being placed into service (Barsom and Rolfe 1999; Dexter and Fisher 1997; Fisher 1984). In some cases, geometric effects combined with the large restraining forces produced by differential cooling of welds was not properly accounted for, leading to fracture of the connection under no external load. However, such fractures are far less common when thin plates, like those in the webs of highway bridge girders, are used due to the inherent flexibility of the plates, lower restraining forces, good detailing, and generally higher toughness of the material. However, in the presence of large crack-like geometrical conditions (e.g., at the intersection of a gusset plate and vertical

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Georgetown Pike, McLean, VA 22/01. E-mail: bill.wright@Hwa.dot.gov. Note. Discussion open until August 1, 2007. Separate discussions must be submitted for individual papers. To extend the closing date by one month, a written request must be filed with the ASCE Managing Editor. The manuscript for this paper was submitted for review and possible publication on January 27, 2005, approved on February 15, 2006. This paper is part of the Journal of Bridge Engineering, Vol. 12, No. 2, March 1, 2007. @ASCE I.SSN 108.4.1007/2007/21.54.1.73455 0

160 Similar Locations

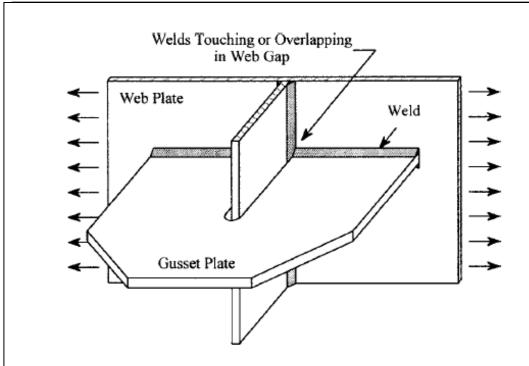


Fig. 11. Illustration of typical lateral gusset intersection with transverse connection plate susceptible to CIF

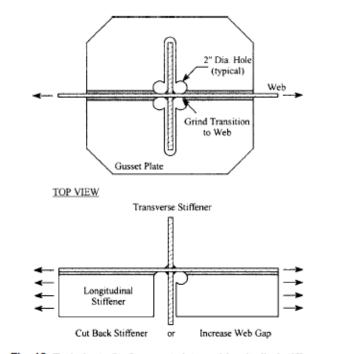
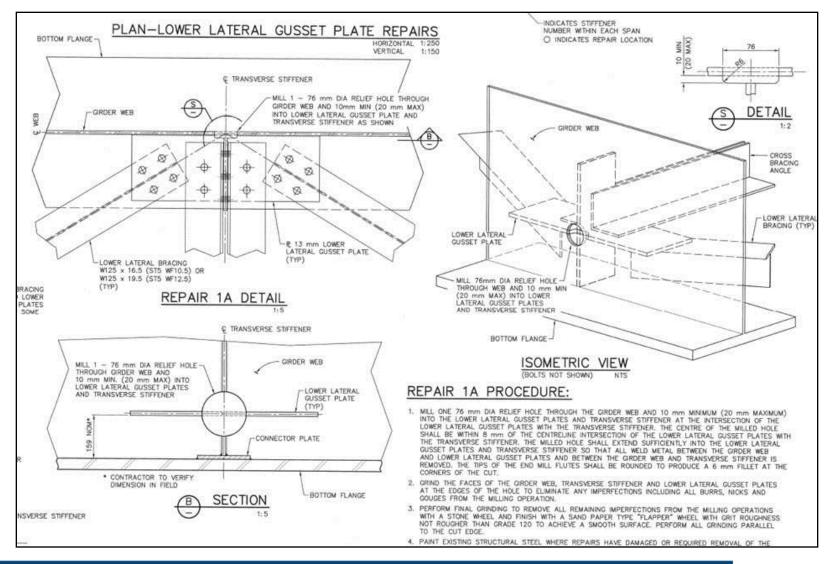


Fig. 12. Typical retrofits for gusset plates and longitudinal stiffeners to address CIF (in the above examples, the gusset plate and longitudinal stiffener are not welded together)









Crack Indications Found at Multiple Locations



Summary

- Rope Access is Viable Means
- Constraint Induced Fractures are Likely On-Going
- Occurs Below Anticipated Fatigue Levels
- Emergency Repairs Require Large Team Effort
- Mitigation Repair Documentation Exists
- Inspectors Beware!
- Owners Review Your Inventory!

Stantec = Bridge Solutions

QUESTIONS?

