



Genesee Avenue Pedestrian Overcrossing

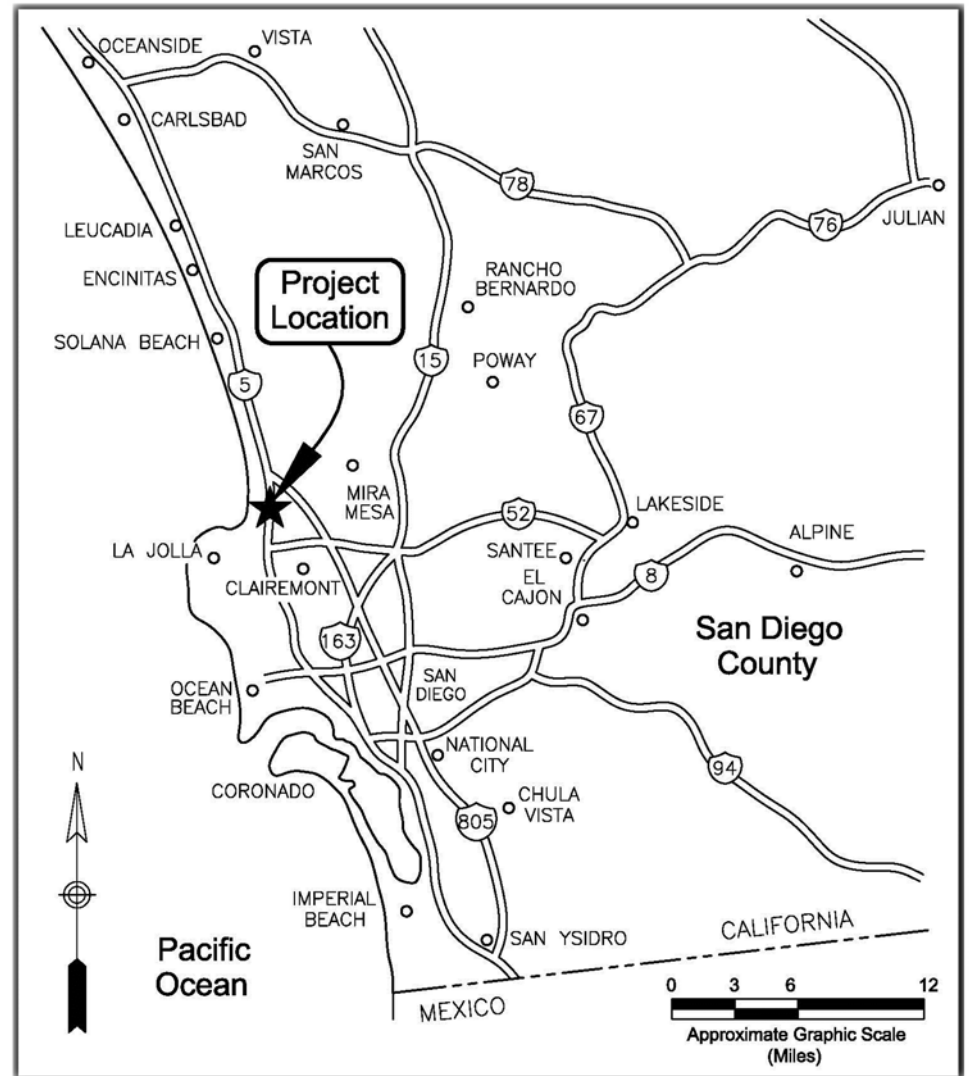
(a concrete bridge with a high degree of curvature)



PRESENTED BY:
Paul Morel, PE and Nathan Johnson, PhD, PE

Project Location

- Interstate 5
- City of San Diego
(Between La Jolla & Del Mar)



Genesee POC Overview

- Component of the I-5 / Genesee Ave Interchange Project
- Will serve as a grade separation to carry pedestrians and bicycles over Genesee Avenue
- Unique project due to high curvature

Bridge Location



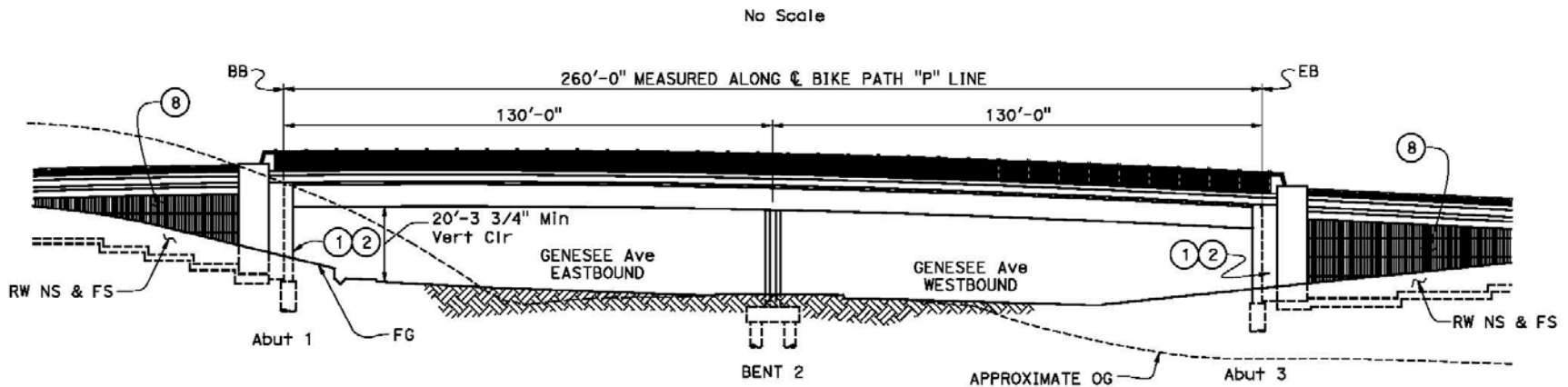
The Design Team

- Kimley-Horn: Prime Consultant – Civil Design
- Simon Wong Engineering: Major Sub – Structures Design
- Caltrans District 11
 - Geotechnical
 - Landscape
 - ROW
 - Existing Utilities



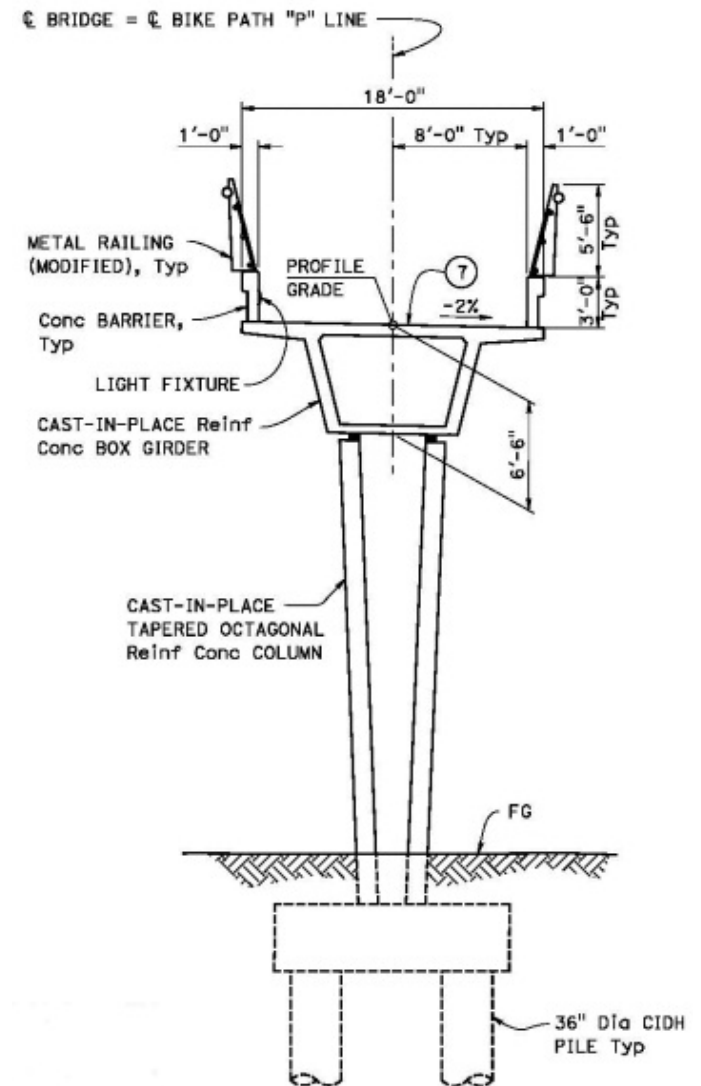
Bridge Description

- 2-span CIP reinforced concrete box girder
- Two equal spans of 130'-0"



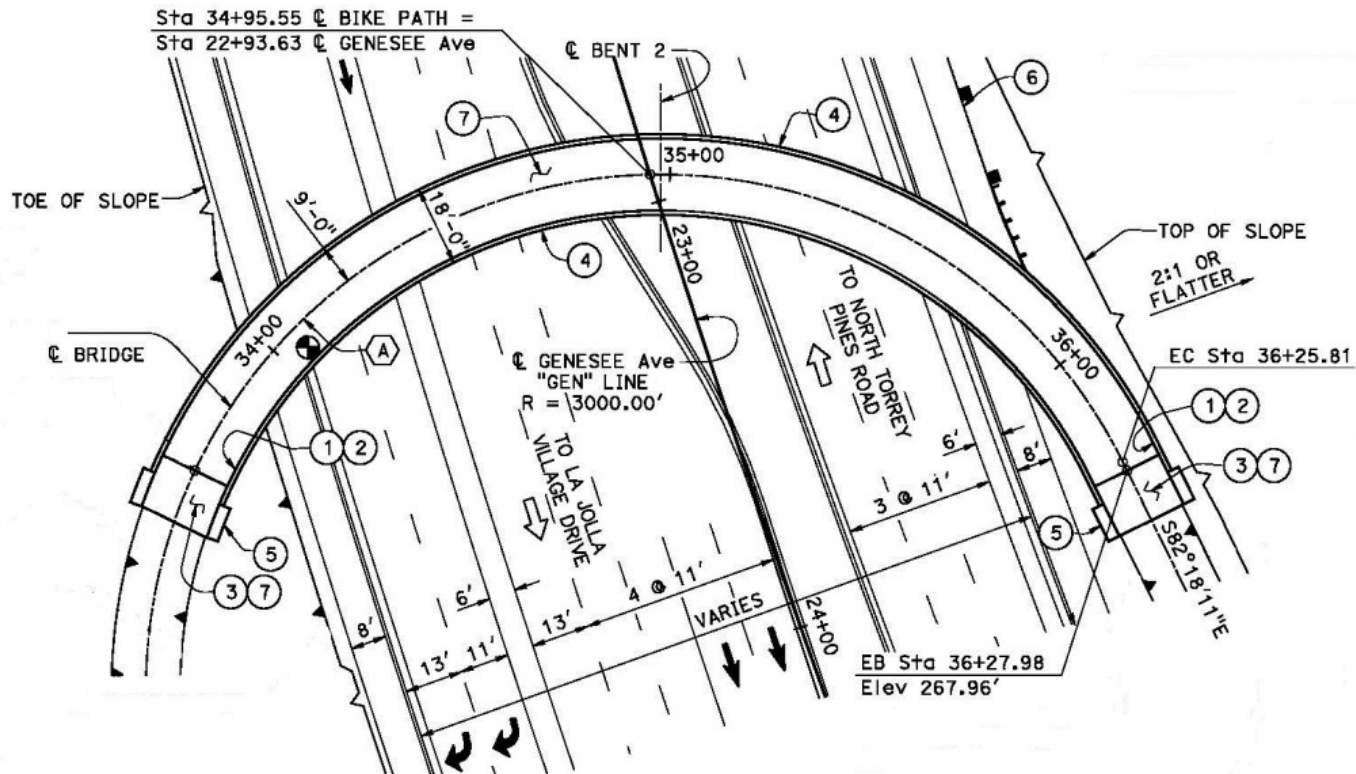
Bridge Description

- Supported on a single-column bent and diaphragm abutments



Bridge Description

- Highly curved R = 115'-0"



Architectural Features

- Curve to provide a uniquely shaped signature structure

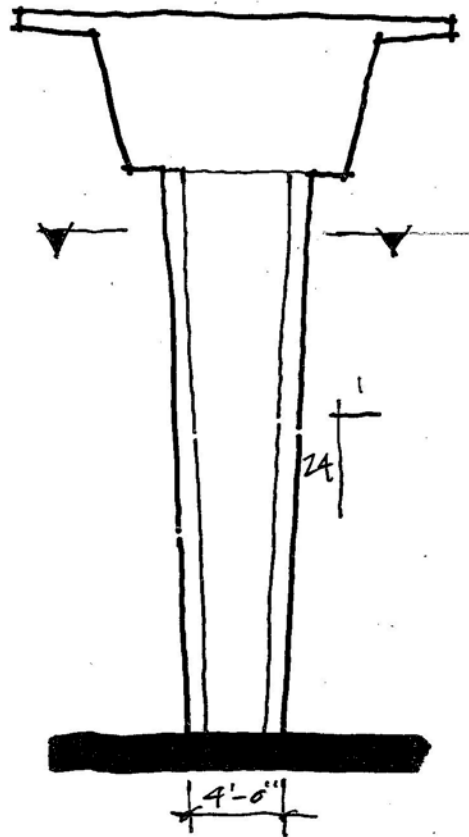


○ Can we clear span the roadway?



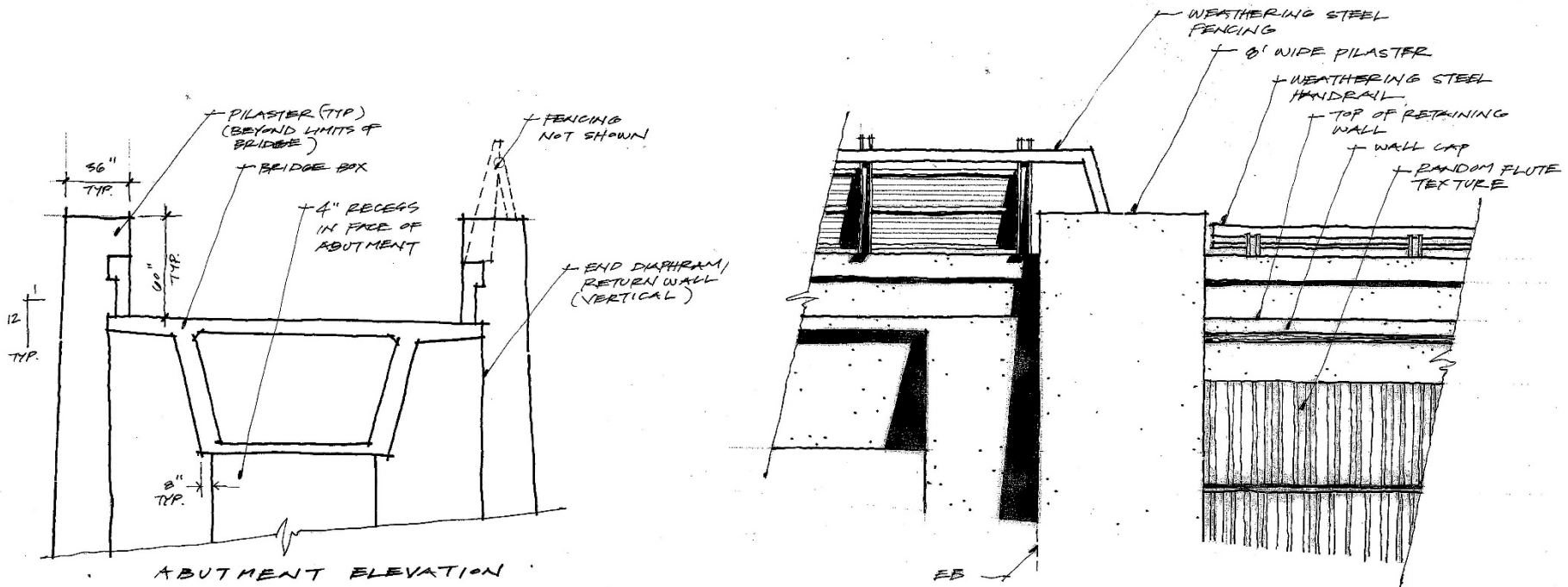
Architectural Features

○ Tapered octagonal column



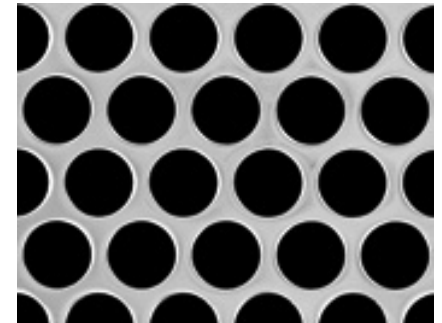
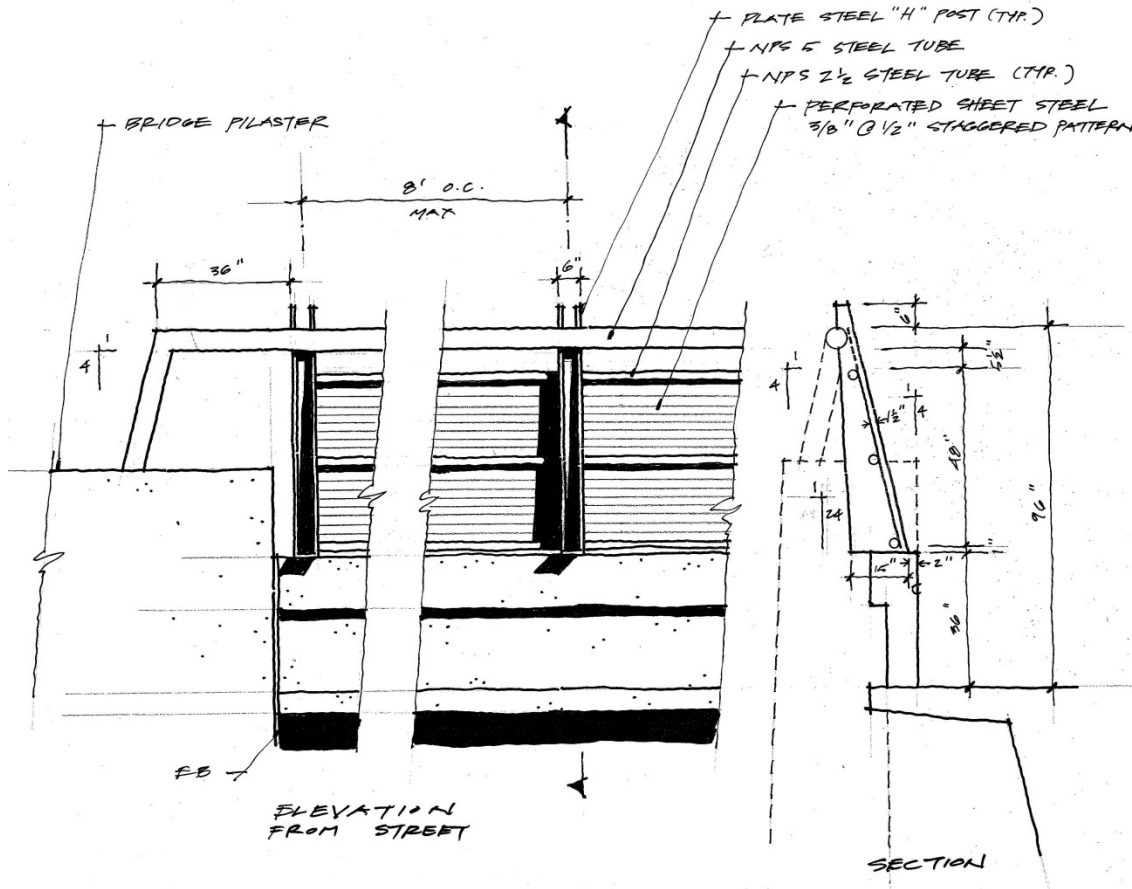
Architectural Features

○ Pilasters behind each abutment



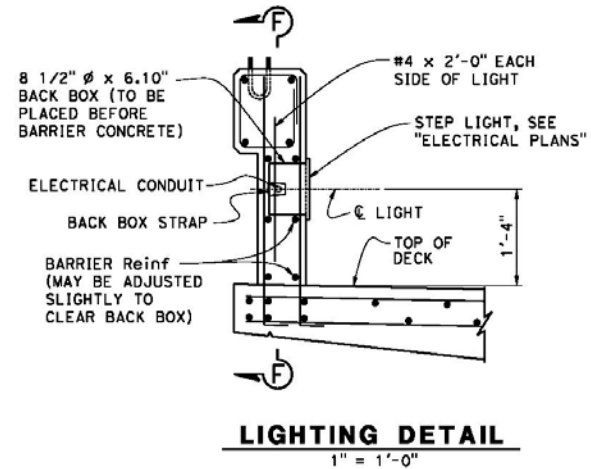
Architectural Features

○ Weathering “Cor-ten” steel railing

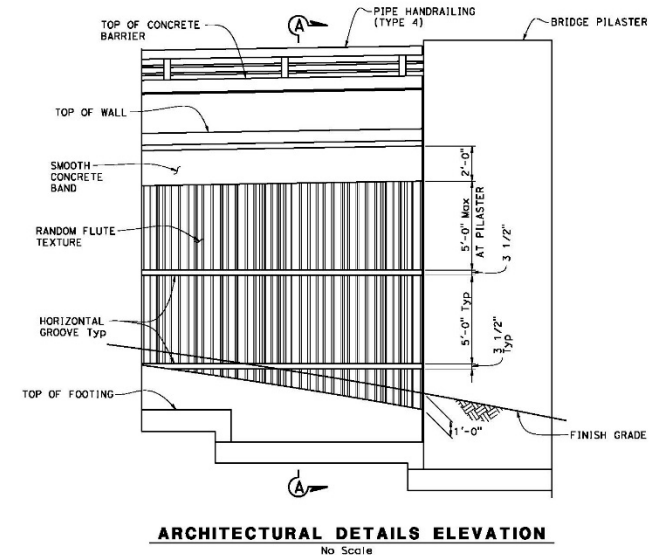


Architectural Features

- Lighting integrated into exterior concrete barrier face

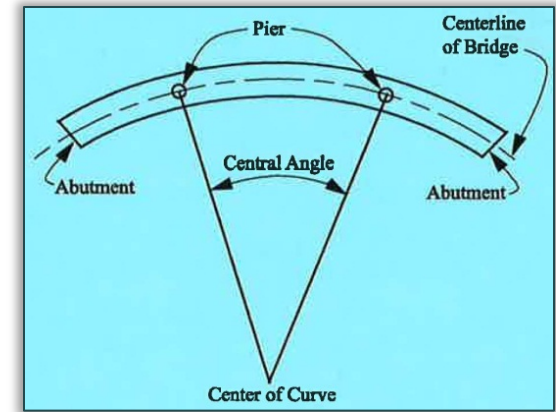


- Formliners
“Random Flute Texture”
- Integral color concrete
“Mesa Buff”



Design Methodology

- AASHTO LRFD Bridge Design Specifications (4th Edition) with Caltrans Amendments



- Central angle of each span (64°) $>$ 34°

2011 CA Amendment to AASHTO 4.6.1.2.3 requires the use of a 6 degrees of freedom 3-D analysis method

- AASHTO Commentary refers to NCHRP Report 620 as the basis for this new requirement

Design Methodology

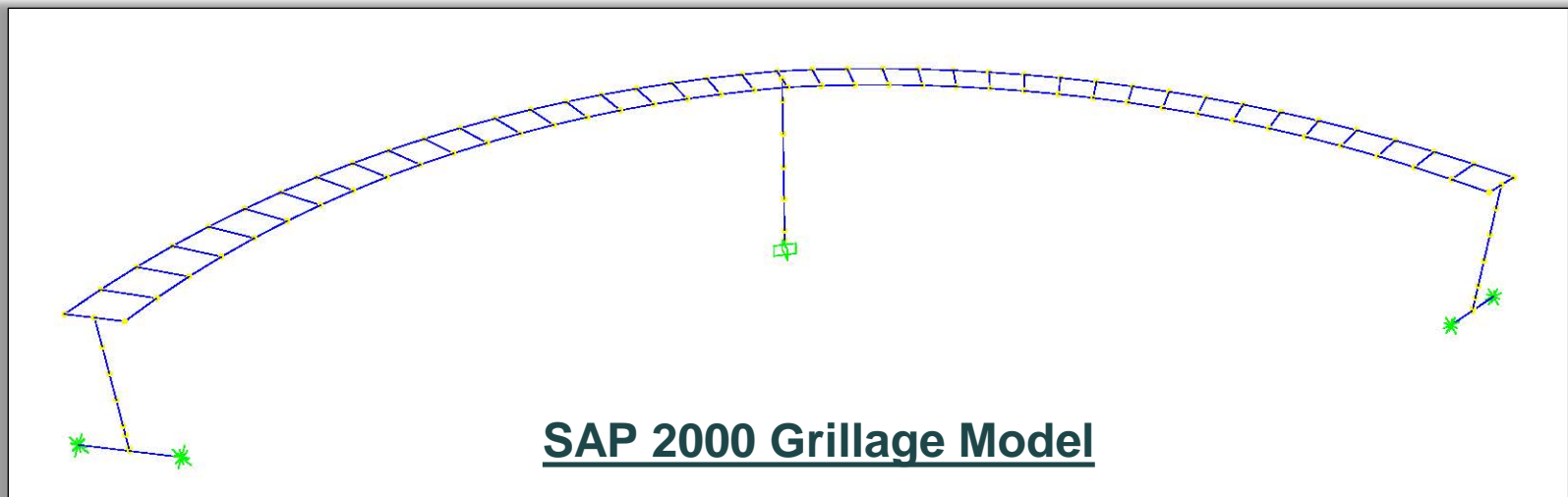
- NCHRP Report 620 was adopted as a design guideline
- Report shows that results of 3-D finite element models and grillage models under gravity loads are close

Grillage Model Used for Design
3-D Finite Element Model Used for Independent Check



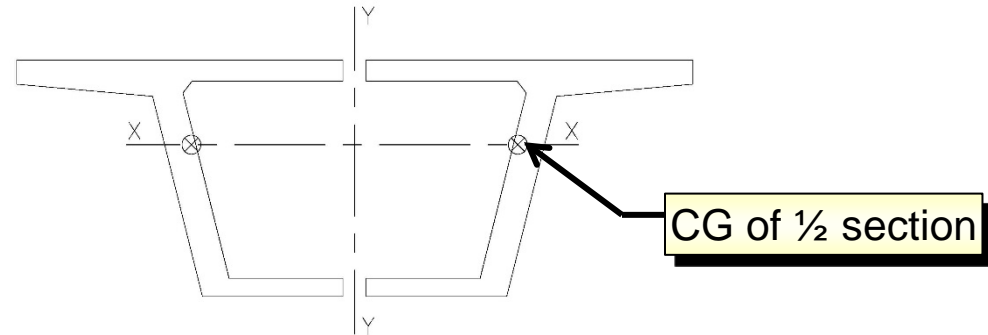
Grillage Model

- Longitudinal beams along each girder line located at the CG of half-section
- Transverse beams model bridge deck, soffit and all diaphragms along span

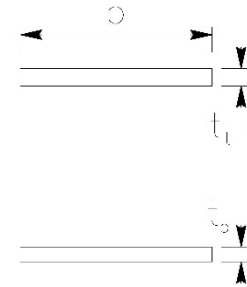


Grillage Model

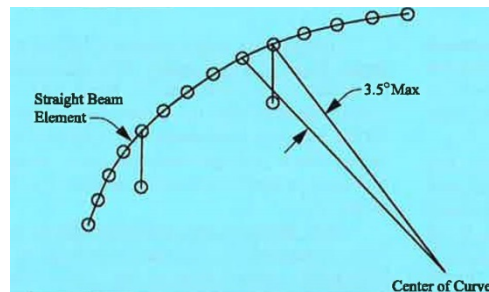
○ Longitudinal elements:



○ Transverse elements:



○ b tributary such that each segment central angle $< 3.5^\circ$



Grillage Model

○ Using gross section properties:

$$T_{\text{permanent}} = 90\% T_{\text{crack}}$$

$$T_{\text{serv I}} = 120\% T_{\text{crack}}$$

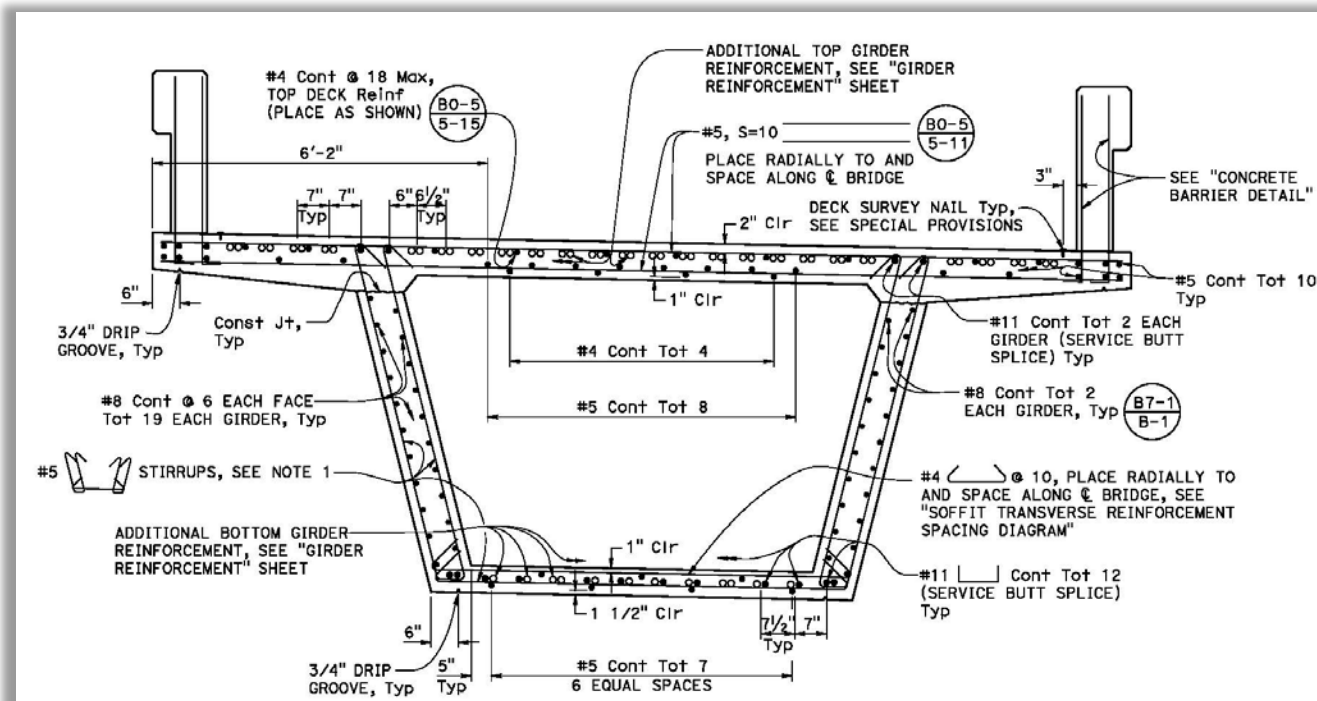
What torsional stiffness to use?

Grillage Model

- 2 boundary conditions to design for shear and torsion:
 - $J_{\text{crack}} = 5\% J_{\text{gross}}$ (typically used for seismic design)
 - $J_{\text{crack}} = 20\% J_{\text{gross}}$

Detailing for Torsion

- Torsional reinforcement forms a closed loop
- Anchored by 135° standard hooks

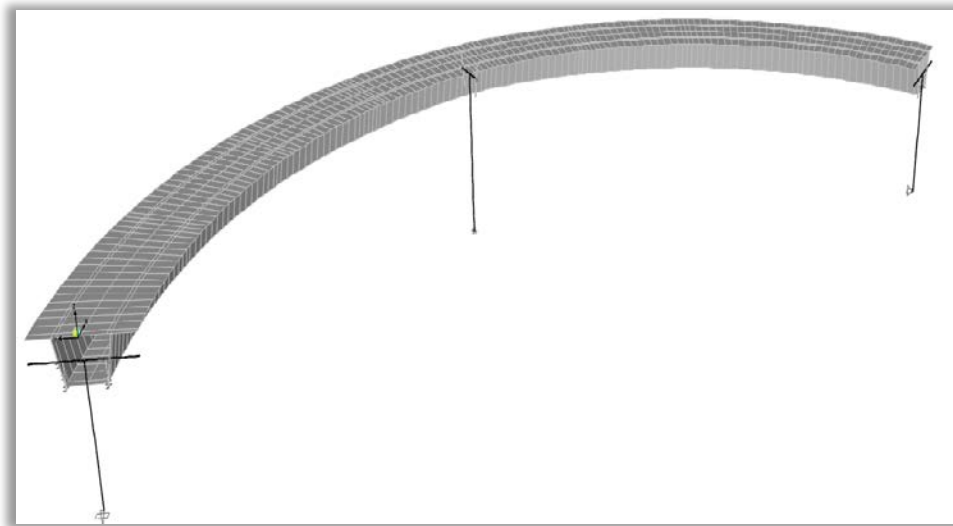


Camber

- Long-term creep factor of 4.0 applied to deflections calculated with J_{gross}
- Two camber diagrams provided (one for each girder)
- Additional deflections due to cracked torsional stiffness checked, but not applied to camber

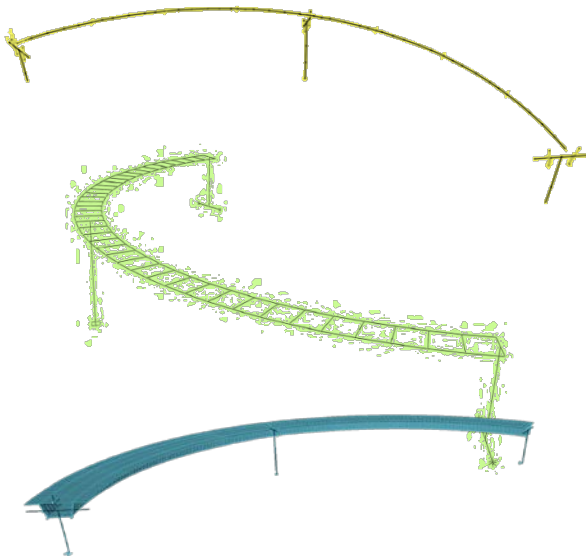
3-D Finite Element Model

- Created with CSI Bridge using thin shell elements
- Used to confirm adequacy of grillage
- Used for independent check



CSI Bridge 3-D Finite Element Shell Model

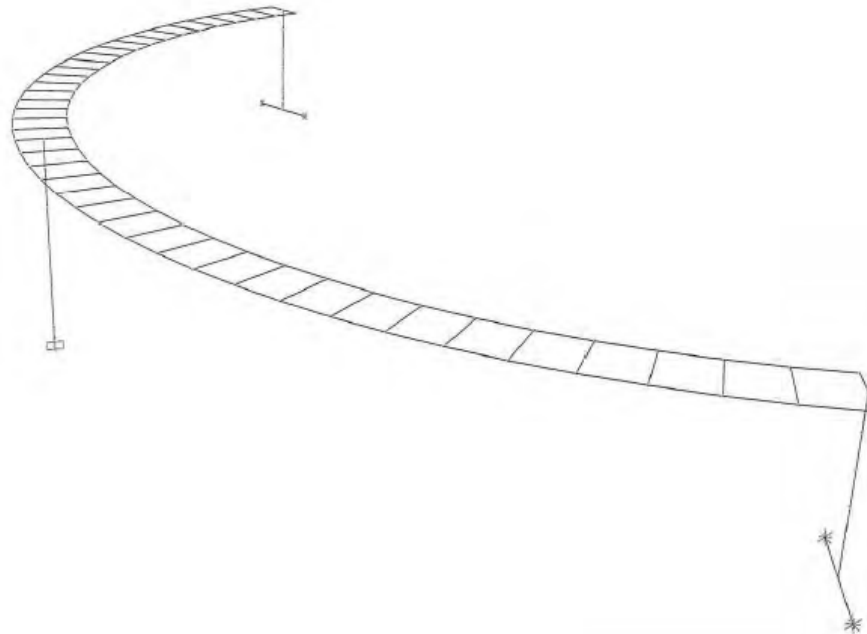
Initial Vertical Deflection Comparison



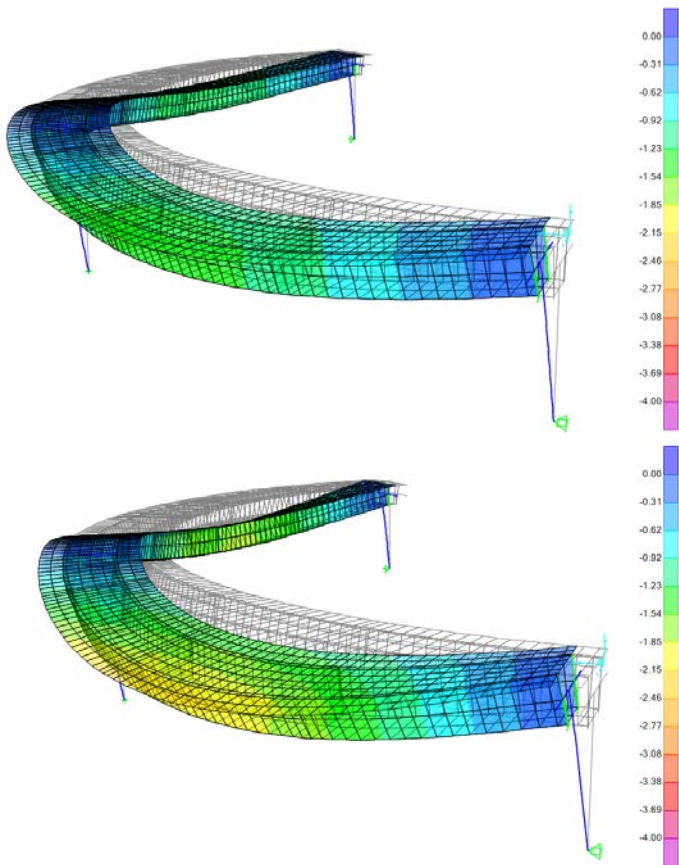
Analysis Method	Stiffness Modification	D Average (in)
Spine model	$J_{eff} = 0.05 * J$	-1.98
Grillage model	$J_{eff} = 0.05 * J$	-1.45
Shell model	$F_{12eff} = 0.05 * F_{12}$	-3.33

- Grillage vs. Spine – grillage 30% lower
- Shell vs. Spine – shell 68% higher
- Qualitatively should be Spine < Grillage < Shell
→?!?%?#?

- Initial approach for grillage based was only softening “J” for longitudinal girder elements.
- Also need to reduce vertical shear stiffness of longitudinal members



Vertical & Torsional Deflection Comparison

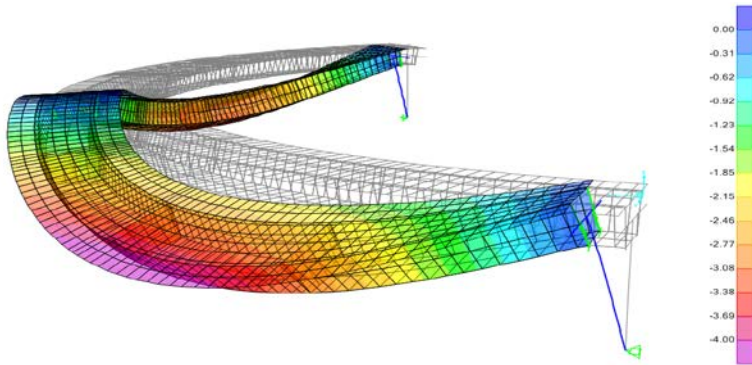


Analysis Method	Stiffness Modification	D Interior Girder (in)	D Exterior Girder (in)
Spine model	None (gross)	-1.10	-1.33
Grillage model	None (gross)	-1.09	-1.32
Shell model	None (gross)	-1.19	-1.41

Analysis Method	Stiffness Modification	D Interior Girder (in)	D Exterior Girder (in)
Spine model	$J_{eff} = 0.2 \cdot J$	-1.16	-1.69
Grillage model	$J_{eff} = 0.2 \cdot J, A_{eff} = 0.2 \cdot A_v$	-1.44	-1.90
Shell model	$F_{12eff} = 0.2 \cdot F_{12}$	-1.58	-2.10

Dead load deflection (x50 scale) of shell model

Vertical & Torsional Deflection Comparison



Analysis Method	Stiffness Modification	D Interior Girder (in)	D Exterior Girder (in)
Spine model	$J_{eff} = 0.05 * J$	-1.45	-1.62
Grillage model	$J_{eff} = 0.05 * J, A_{veff} = 0.05 * A_v$	-2.95	-3.43
Shell model	$F_{12eff} = 0.05 * F_{12}$	-3.335	-3.90

- Comparison of deflections showed reasonably close results between grillage and 3-D model for all torsional stiffness assumptions

- Since deflections of grillage are similar to shell model, grillage approach is appropriate
 - Use grillage for design (with spreadsheets)
- Use solid CSIBridge model for Independent Check (superstructure design)

Peer Review

- Performed by bridge expert from University of Nevada, Reno
- Reviewed analysis of grillage and 3-D finite element models
- Reviewed deflections and flexure/shear/torsion demands
- Provided recommendations for box girder detailing

References

- AASHTO LRFD Bridge Design Specifications (4th Edition) with Caltrans Amendments
- NCHRP Report 620
- “Bridge Deck Behavior” by Edmund Hambly
- “ACI Shear and Torsion Provisions for Prestressed Hollow Girders” by Thomas Hsu

Lessons Learned

- Design beyond what common software can handle
 - Use of spreadsheets → budget
- Variation of approach for non-standard design
 - (Grillage vs. FEM, etc.) → methodology check
- Value of Independent Check
- Value of Peer Review Process

Future Work

- Monitor torsional deflections and disseminate case study information

Questions?

