

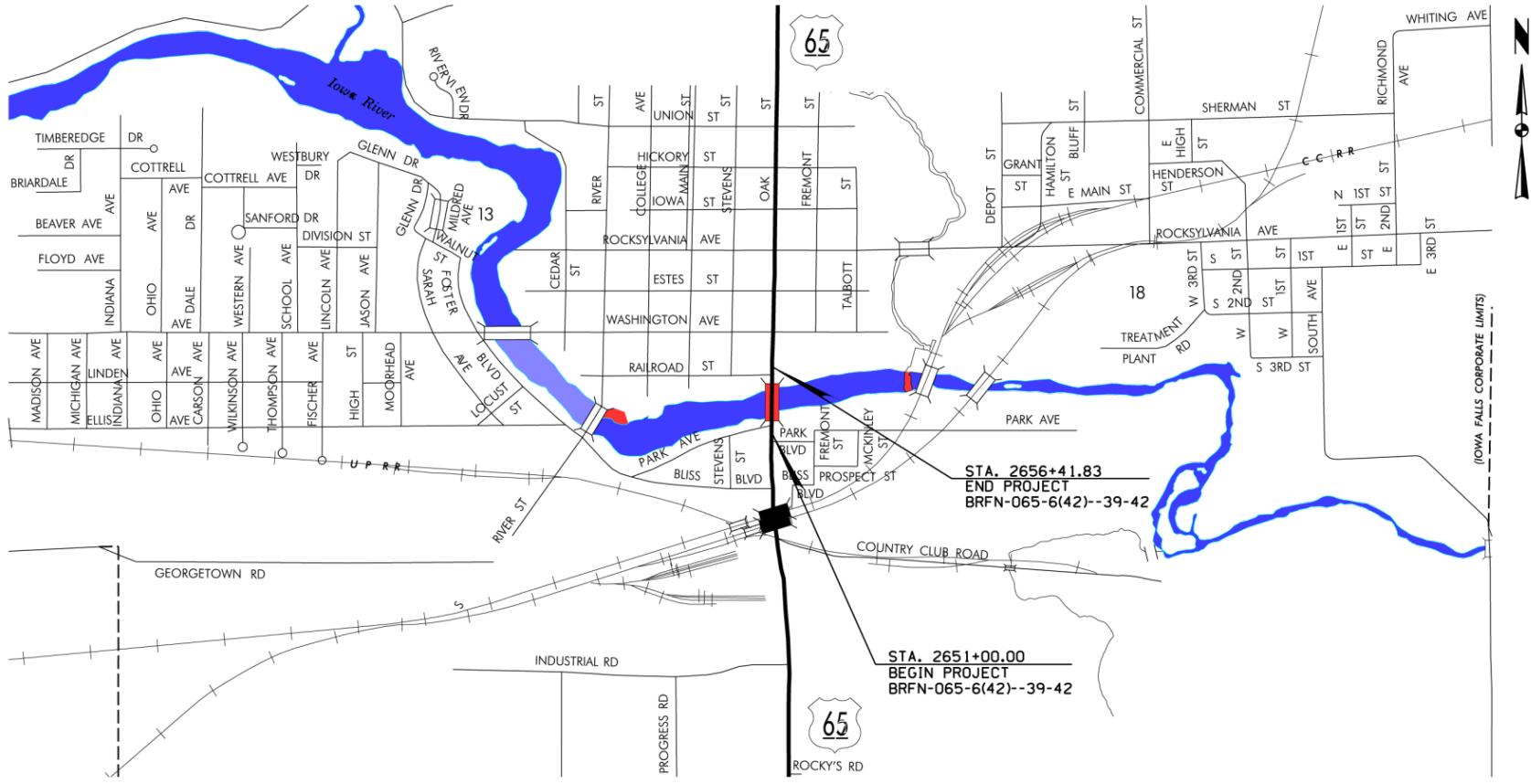


US 65 Oak Street Bridge

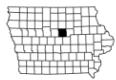
DESIGN, CONSTRUCTION & STRUCTURAL HEALTH
MONITORING OF A STEEL ARCH BRIDGE

Iowa Falls, Iowa

Location of Project



Part of City of Iowa Falls, Iowa



Introduction

- » Demolition Concepts
- » Concept Design
- » Final Design
- » Construction
- » Health Monitoring

Existing Bridge

- » Built in 1928
- » 255-foot Open Spandrel Concrete Arch Bridge
- » 24-foot Roadway and Two Sidewalks
- » Deck Supported by R/C Floor Beams



Existing Bridge

- » Rehabilitated 7 Different Occasions
- » Needed Widening and Strengthening
- » Replace Rather than Rehabilitate

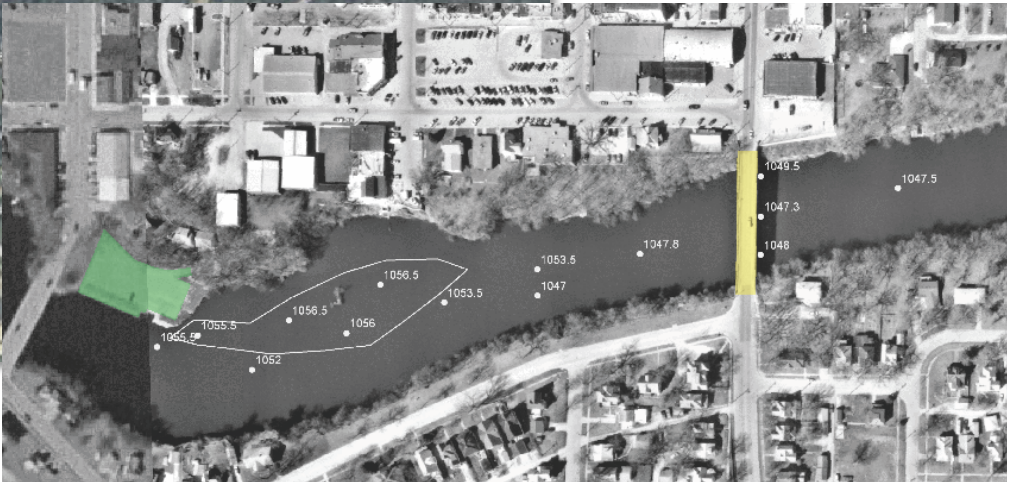
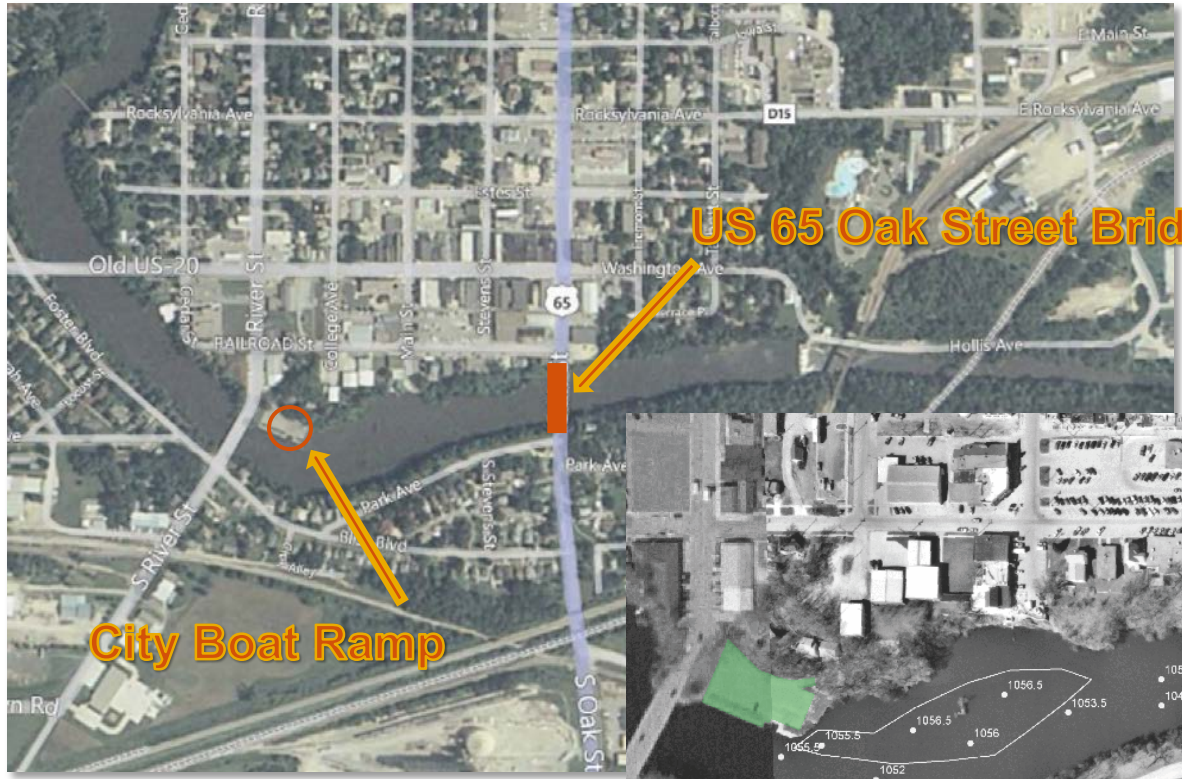


Concept Stage Type Study

- » Identify Constraints and Constructability Concerns
- » Identify Feasible Demolition Concepts
- » Identify Feasible Replacement Alternatives
- » Cost
- » Timeline for Construction

Constraints and Constructability Issues

» Site Access



Constraints and Constructability Issues

- » Historic Church
 - NW Corner of Bridge
 - Listed on the National Register of Historic Places

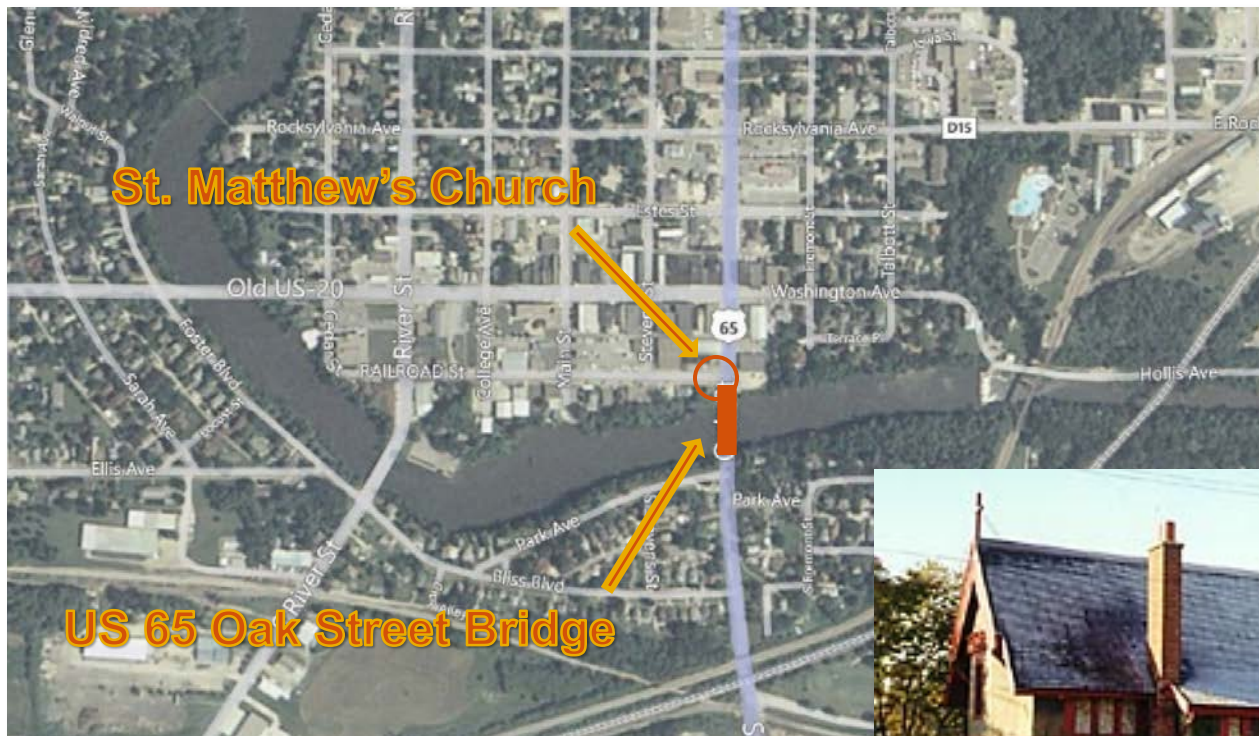


Photo by: iafalls.com

Constraints and Constructability Issues

- » Dam
 - Maintain Water Level



Demolition Concepts Assumptions

- » No Environmental Restrictions
- » Access to River is Available
- » No Prohibition on Use of Engineered Explosives
- » Vibration Monitoring Required
- » Cost versus Clean up

Actual Demolition



- » Started mid October 2010 and Finished mid December 2010.
- » Lowered the Iowa River with Cooperation of the Downstream Dam
- » Constructed an Access Road and Causeway Utilizing a System of Steel Bridge Beams and Crane Mats over the Open Water

Actual Demolition



- » Constructed a System to Protect the Sanitary Sewer Lines
- » Demolished the Bridge using the Causeway
- » Deck and Columns were Demolished using two Excavators with Hydraulic Breakers
- » Each excavator started at the Center of the Bridge

Actual Demolition



- » Demolished the Arches Using the same Excavators with a Mounted Hammer
- » Arch Pieces were Broken Down and Hauled Off-Site by Truck
- » Vibration Monitoring was Provided at the Adjacent Church and Residences

Bridge Replacement Alternatives

- » City of Iowa Falls
 - Scenic City
 - River Cruises is a Major City Attraction
 - Several Types of Bridges that Span Across Iowa River



Bridge Replacement Alternatives

Washington Avenue Concrete Arch Bridge



Bridge Replacement Alternatives Assumptions

- » No Environmental Restrictions
- » Access to River
 - Launch Segmental Barges
 - Erect a Suitable 150-ton Crane
- » Vibration Monitoring Required

Bridge Replacement Alternatives

Two Span Prestressed Concrete Alternative

- » Easiest to Construct
- » Drilled Shaft at Pier Eliminates Need for Cofferdam
- » Drilled Shaft at Abutments Reduces Vibration Impacts
- » Less Rock Excavation than other Alternatives
- » Most Economical Option



Bridge Replacement Alternatives

Simple Span Haunched Girder Alternative

- » Non-conventional Super Type
- » Heavy Girder Pieces
- » Require Temporary Bents or Falsework
- » Substantial Rock Excavation
- » Require Lead Time for Fabrication



Bridge Replacement Alternatives

Partial Thru Steel Arch Alternative

- » Easier to Construct Relative to Concrete Arch
- » Shorter Construction Period than Concrete Arch
- » Require Temporary Bents, Falsework or Tied-Back Systems to Construct
- » Additional Inspection and Maintenance of Suspenders
- » Requires Construction Engineering



Bridge Replacement Alternatives

Concrete Deck Arch Alternative

- » Most Difficult/Complex to Construct
- » Rib Shortening Issues
- » Requires Temporary Bents or Falsework or Tied- Back Systems
- » Longest Construction Period
- » Requires Construction Engineering



Bridge Replacement Alternatives

The Alternatives



Existing Concrete Deck Arch



Prestressed Concrete Girder



Haunched Steel Girder



Partial Thru Steel Arch



Concrete Deck Arch

New Bridge – Aerial View



Final Design Considerations

- » Tight Geometrics
- » Bridge Footprint
- » Retaining Walls and Rock Cuts
- » Substructure Sizing and Sustainability
- » Protection of the Superstructure

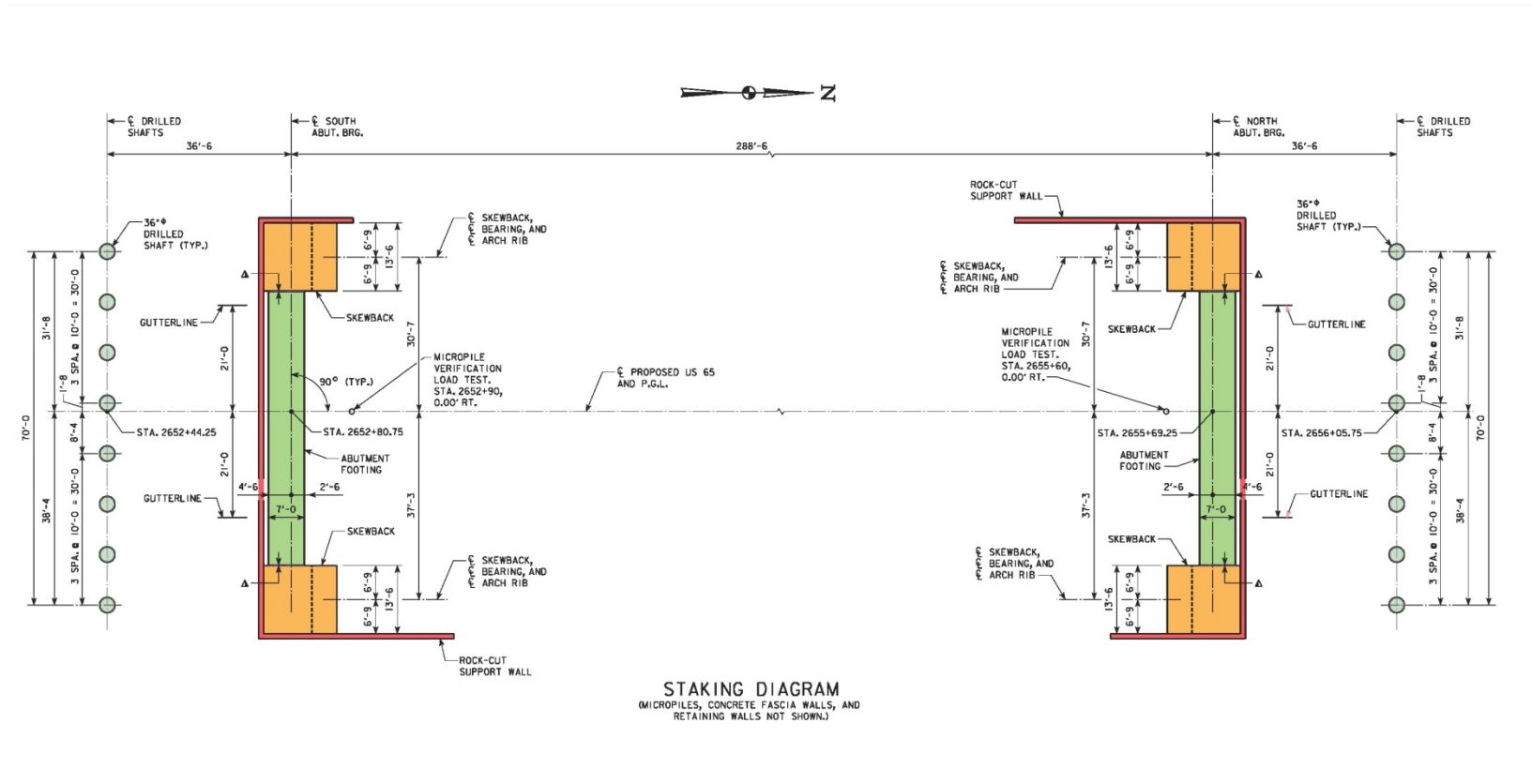
Existing Church Retaining Wall



Micropile Retaining Wall



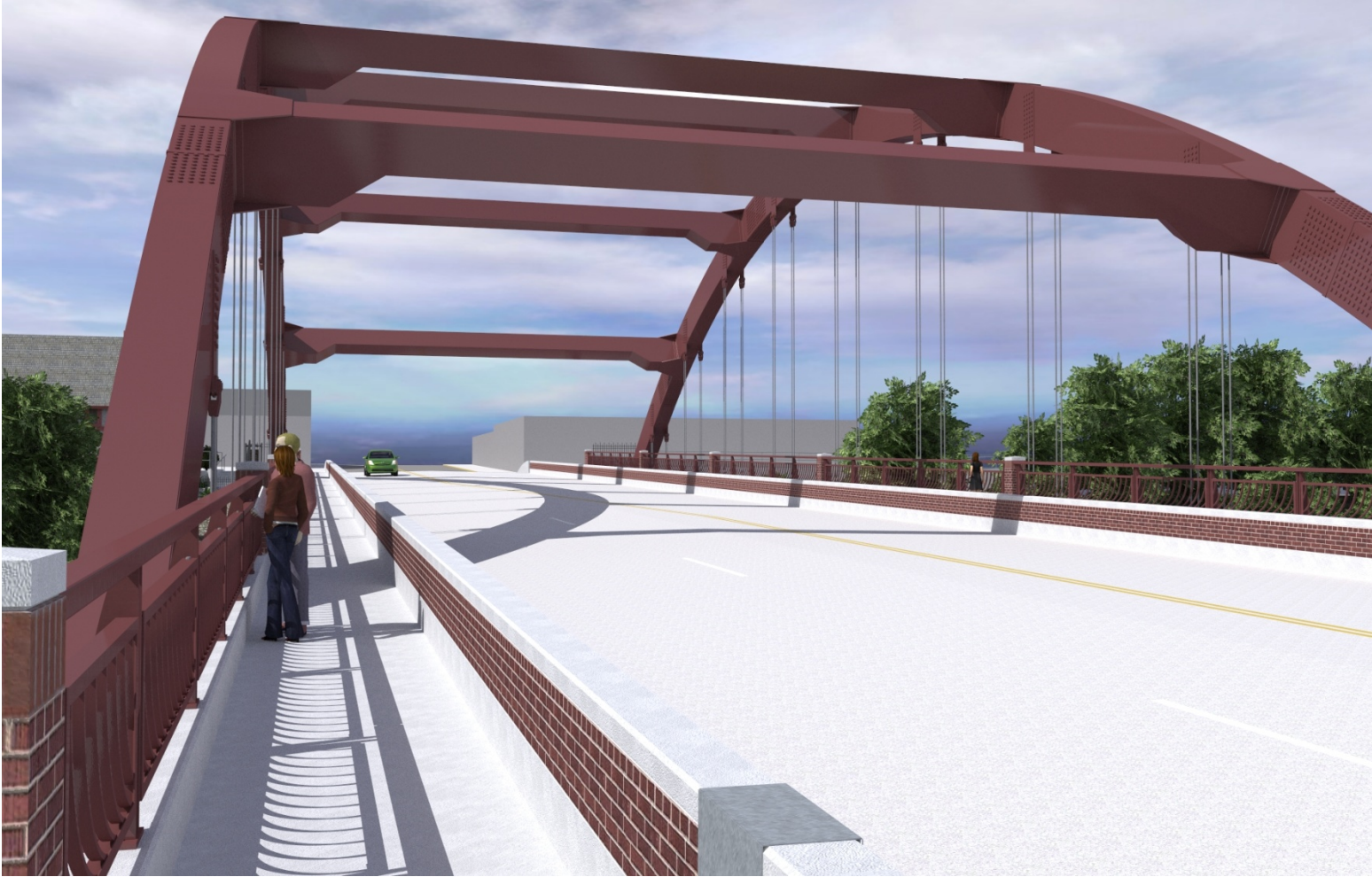
Rock Cut Support Walls



Aesthetics and Renderings

- » Kimball Olson
Aesthetics coordinator – Iowa DOT
- » Used to convey
 - Size
 - Perspective
 - Spatial relationships
- » Useful in Design and Presentation to the General Public

Rendering – Showing Trail



Actual Bridge



Deck and Hanger Cables

- » Floor Beam and Stinger system suspended from the Arch Rib
- » End Floor Beams frame directly into the Arch Rib
- » Deepened Exterior Stringer / Stiffening Girder
 - Distributes vehicular loads from deck to multiple hanger cables
 - Minimize local live load deflections

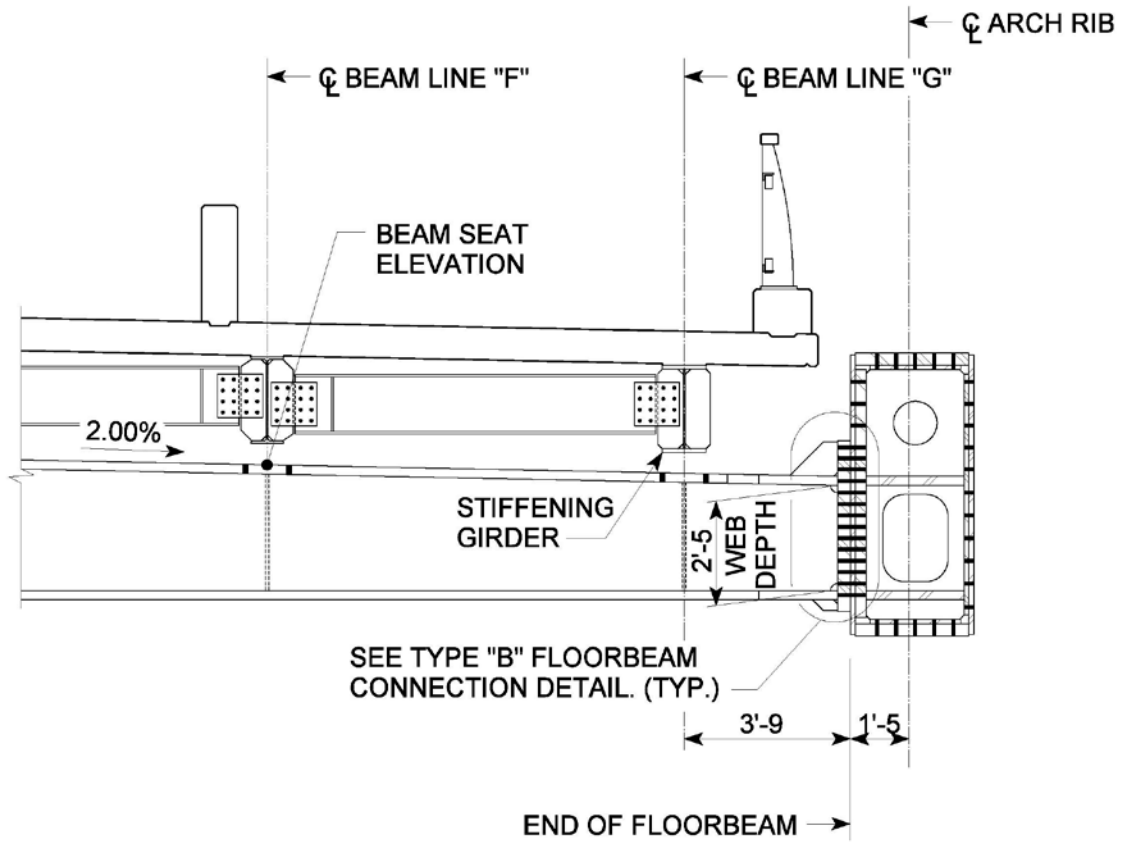
Arch Design

- » Grade 50 Weathering Steel with Protective Coatings
- » Built in Replacement of Hanger Cables
- » Pinned Bearings
- » Wide aspect ratio
 - Length to Width ratio = 4
 - No trussed sway bracing.

Interior Floor Beam and Hangers



End Floor Beam



TYPE "B" FLOORBEAM ELEVATION

(LOOKING NORTH)

Pinned Bearings

- » Net Zero Change in Steel Weight from a Fixed Connection
- » Reduced Footing Size
- » Minimized Impacts to Surrounding Properties



Foundations

- » Issues:
 - Existing Bridge Showed Signs of Undermining
 - Arch Skew Back Behave Differently than the Retaining Wall Abutment.

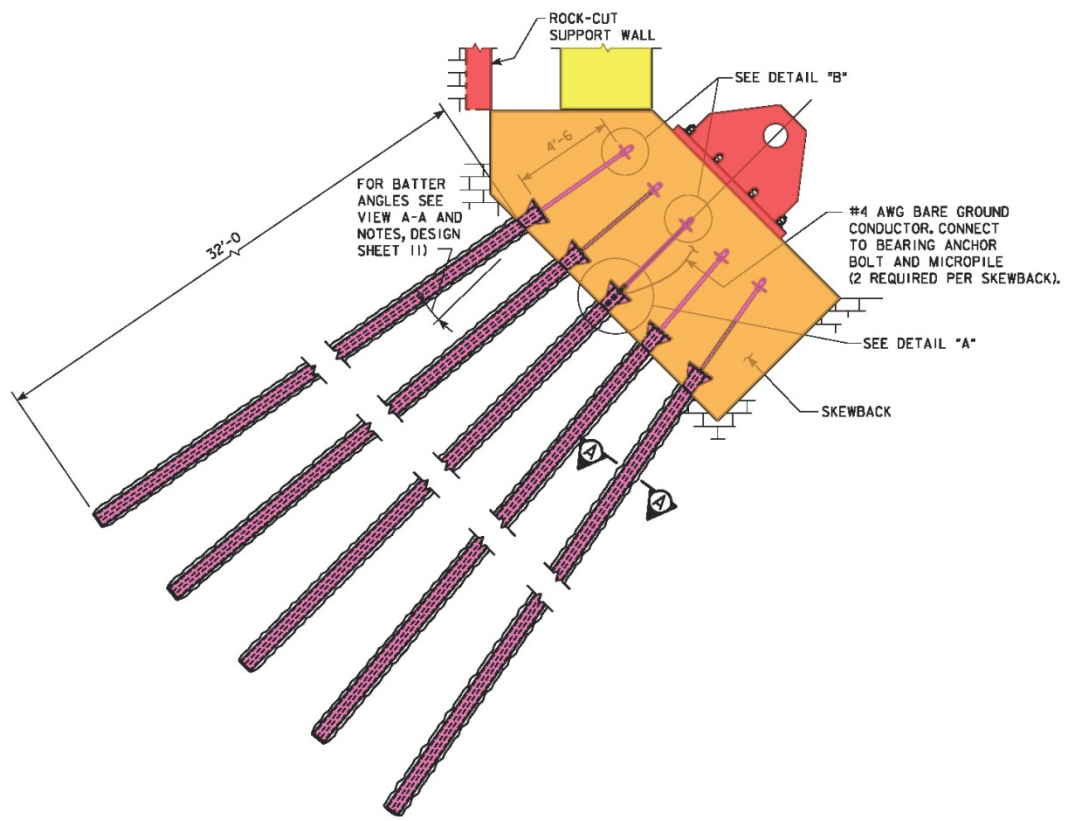
- » Solutions:
 - High Capacity Micropiles
 - Separate Foundations
 - Tied-back Abutment
 - Lightweight Backfill

Foundation Issues

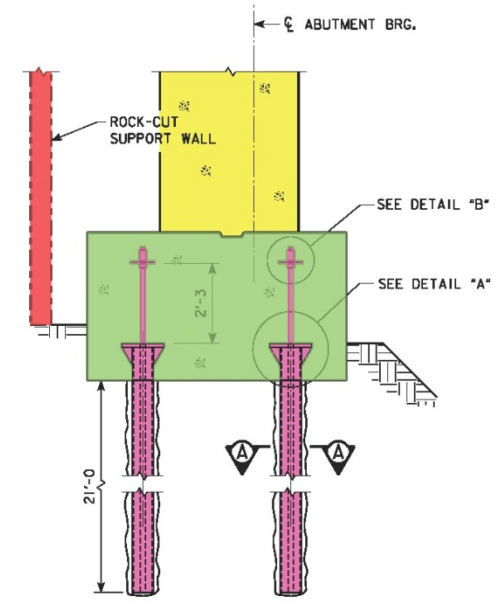
» Existing Bridge Undermining



Micropiles

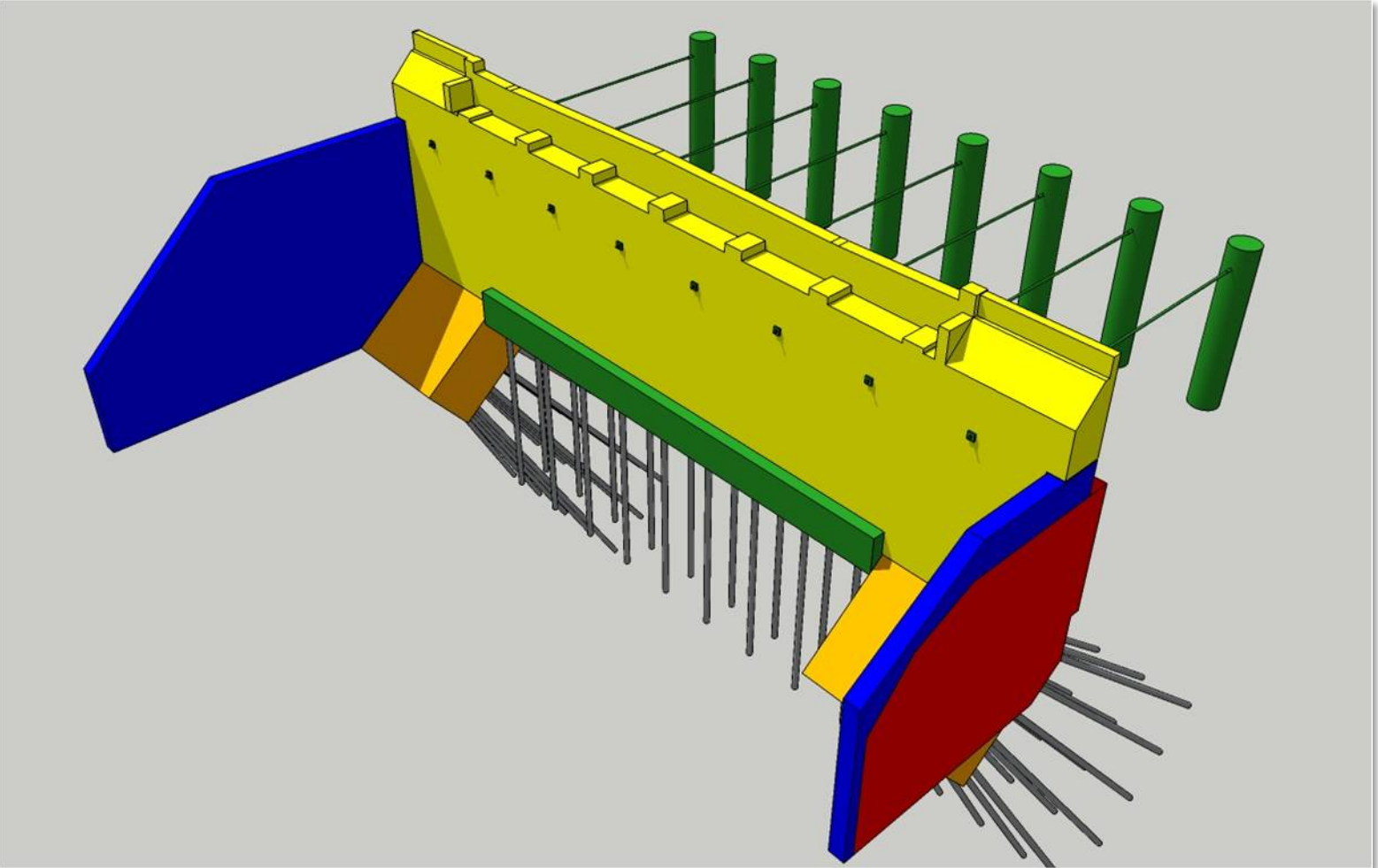


TYPICAL SECTION AT SKEWBACK (SHOWING MICROPILES)



TYPICAL SECTION AT ABUTMENT FOOTING (SHOWING MICROPILES)

Abutment and Micropile Schematic



Pin and Hanger Steel Tolerances

- » Construction tolerance issues during fabrication of the Pins and Hangers:
 - ASHTO 6.8.7.3
 - Requirement: 0.031”
- » Maximum Difference
- » As Fabricated
- » Pin to Pin Plate: 0.04”
- » Pin to Socket: 0.14”



Pin and Hanger Steel Tolerances

- » Resolution – Perform additional tests on the Pin to Socket connection to quantify permanent deformation under load.
 - 55% Proof load – No permanent deformation allowed as measured to nearest 0.001”
 - Contractor also tested two connections to 100% load



Pin and Hanger Steel Tolerances

- » Observed Deformations
 - Proof load = 0.00"
 - 100% load = 0.04"

- » Contractor was allowed to use the pins and sockets as fabricated.



Fabricated Bearing Tolerances

- » Bearing Side Plates
 - Warped out of tolerance
 - Would not allow upper unit to fit with the lower unit
- » Masonry Plate
 - Curved upward on the edges
 - Would not allow full bearing on the concrete skew back



Fabricated Bearing Tolerances

- » Bearing Side Plates
 - Total conflict 1/4"
 - Fabricator milled 1/8" from upper and lower units
 - Difference was evaluated and deemed acceptable
 - Complicated fit



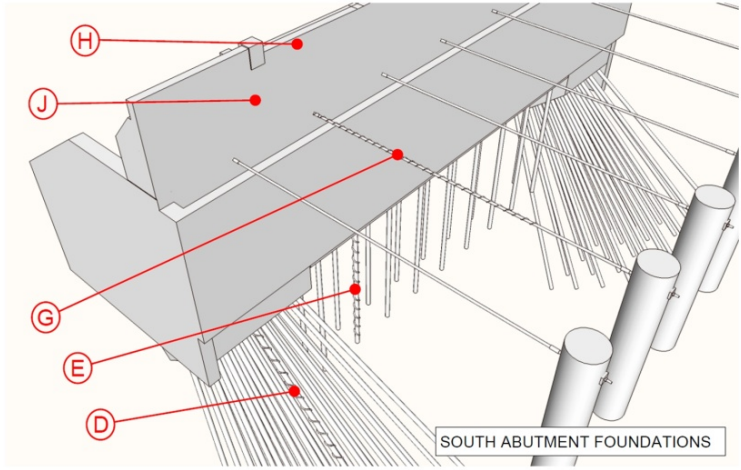
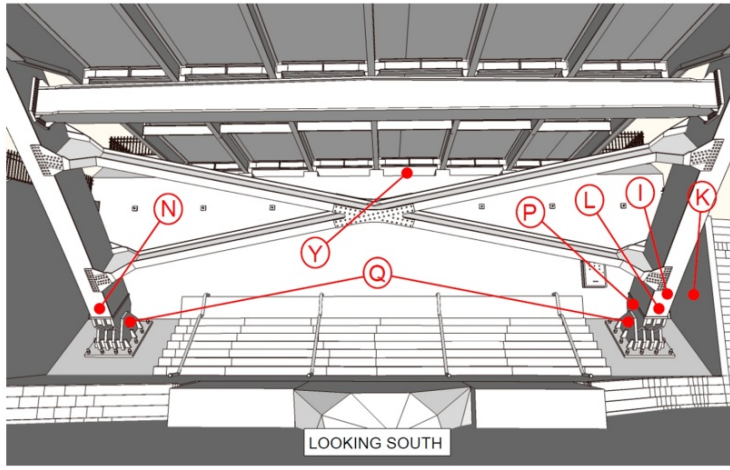
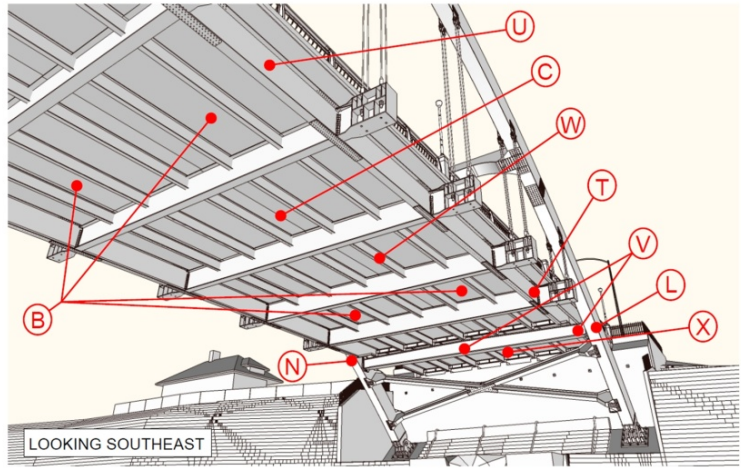
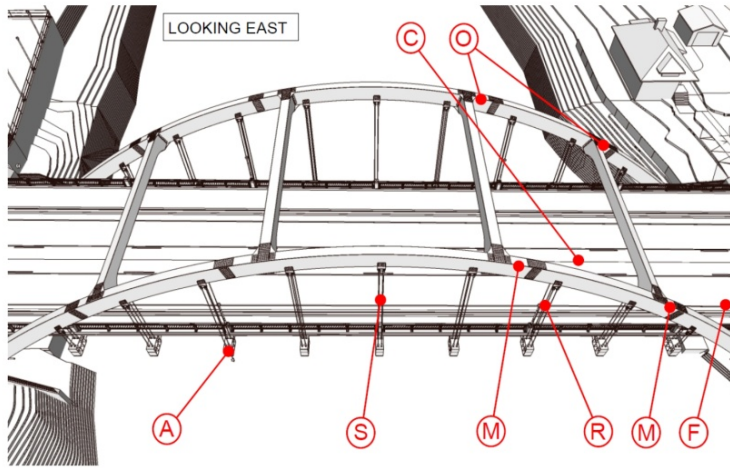
Fabricated Bearing Tolerances

- » Masonry Plate
 - Maximum gap of 3/4" at the edge
 - Steel erection allowed to proceed
 - Jacked and grouted prior to pouring the concrete deck



Health Monitoring

» Iowa State University - Dr. Brent Phares





US 65 Oak Street Bridge

QUESTIONS?