



**Western
Bridge
Conference
2007**

**Load Rating of Prestressed
Concrete Girder Bridges:
Interior vs. Exterior Girders**

Introduction

- **Importance of Bridge Evaluation**
 - **Viaducts within the U.S. Highway infrastructure are on average 40 years old with a theoretical design life of 50 years.**
- **2006 National Bridge Inventory: Deficient/Obsolete**
 - **Nationwide: 26%**
 - **New Mexico: 692 Bridges (291 – Obsolete, 401 – Deficient)**
- **Vehicle Miles of Travel (VMT) have increased 148% in the last 30 years.**

Objective

- **Support the AASHTO Subcommittee on Bridges and Structures implementation of load and resistance factor design by continuing the transition from LFR to LRFR.**
- **Rate 5 prestressed concrete girder bridges, courtesy of the NM bridge inventory, for LFR and LRFR using the Bridge Rating and Analysis of Structural Systems (BRASS) Software.**
- **Specific Objectives**
 - **Identify differences and trends in LFR and LRFR rating factors.**
 - **Compare rating factors for interior and exterior girders.**
 - **Examine trends in rating factors as affected by bridge geometry.**

Bridge Rating and Analysis of Structural Systems (BRASS) Software

- Used to load rate superstructure elements.
- BRASS-GIRDER is current with the 16th edition of the AASHTO Standard Specifications for Highway Bridges (1996), including the 1997 thru 2000 Interims.
- BRASS-GIRDER (LRFD) is current with the 2nd edition of the AASHTO LRFD Bridge Design Specifications (1998), including the 2000 Interim.

Bridge Sample

Bridge 8852

1 Span, Length of 97'
 6 AASHTO-IV girders spaced at 7'
 10 harped & 34 straight low relaxation strands
 Conc. comp. strength of 5.5 ksi & 4.75 ksi initial



Bridge 7195

Span No. 3, Length of 107'
 5 AASHTO-V girders spaced at 97"
 8 harped & 44 straight stress relieved strands
 Conc. Comp. strength of 5 ksi & 4.5 ksi initial



Bridge 7390

Span No. 2, Length of 58'9"
 6 AASHTO-III girders spaced at 9'1"
 4 harped & 16 straight stress relieved strands
 Conc. Comp. strength of 5 ksi & 4.5 ksi initial



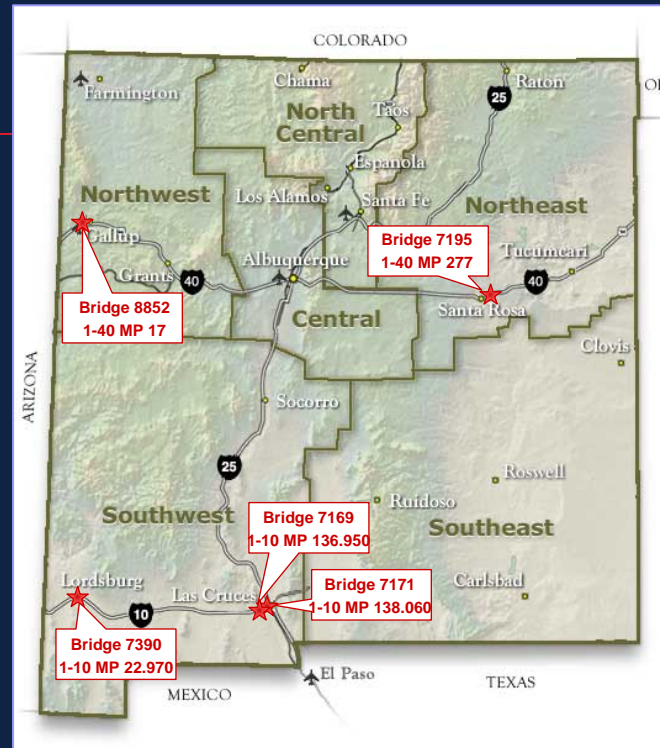
Bridge 7169

Span No. 3, Length of 38'3"
 5 AASHTO-II girders spaced at 9'9"
 4 harped & 14 straight stress relieved strands
 Conc. Comp. strength of 5 ksi & 4.5 ksi initial



Bridge 7171

12 Spans: all similar, Length of 80'6-1/4"
 7 AASHTO-III girders spaced at 6'8"
 3 harped & 30 straight stress relieved strands
 Conc. comp. strength of 5 ksi & 4.5 ksi initial



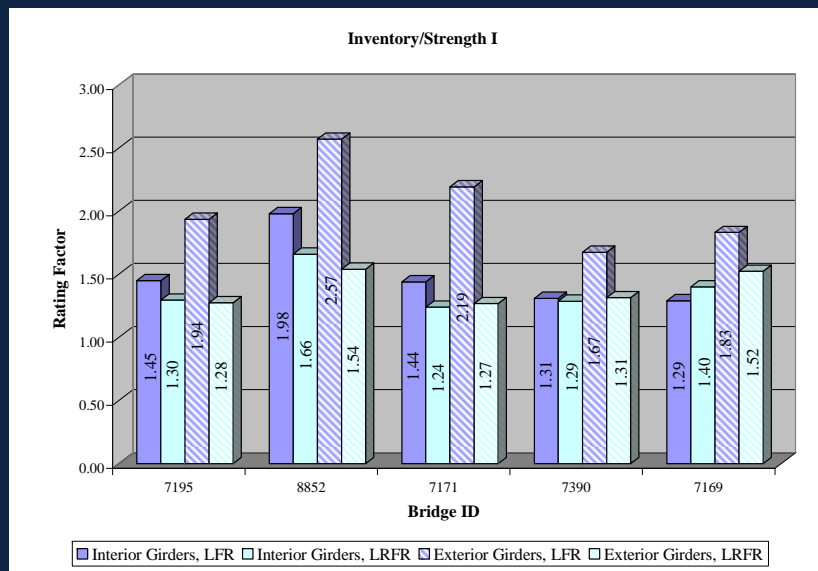
Bridge Description

| | Bridge ID | | | | |
|--------------------------|-----------------|----------------|-----------------|-----------------|-----------------|
| | 7195 | 8852 | 7171 | 7390 | 7169 |
| Span Length | 107' | 97' | 80' 6 ¼ " | 58 ¾' | 38 ¼' |
| Girder Type | AASHTO-V | AASHTO-IV | AASHTO-III | AASHTO-III | AASHTO-II |
| No. of Girders | 5 | 6 | 7 | 6 | 5 |
| Girder Spacing | 9' 7" | 7' | 6' 8" | 9' 1" | 9' 9" |
| No. of Harped Strands | 18 | 10 | 8 | 4 | 4 |
| No. of Straight Strands | 44 | 34 | 30 | 16 | 14 |
| Strand Type | Stress-relieved | Low-relaxation | Stress-relieved | Stress-relieved | Stress-relieved |
| Strand Diameter, in. | 7/16 | ½ | 7/16 | ½ | 7/16 |
| Stirrup Spacing, in. | 11 | 4 | 15 ¼ | 8 | 10 |
| f'_c , ksi | 5 | 5.5 | 5 | 5 | 5 |
| f'_{ci} , ksi | 4.5 | 4.75 | 4.5 | 4.5 | 4.5 |
| Slab thickness, in. | 7 ¼ | 8 | 6 7/16 | 8 | 7 9/16 |
| Skew, degrees | ~ 21 | ~ 19 | 20 | ~ 20 | 30 |
| FWS, lbs/ft ² | 15 | 30 | 15 | 15 | 15 |

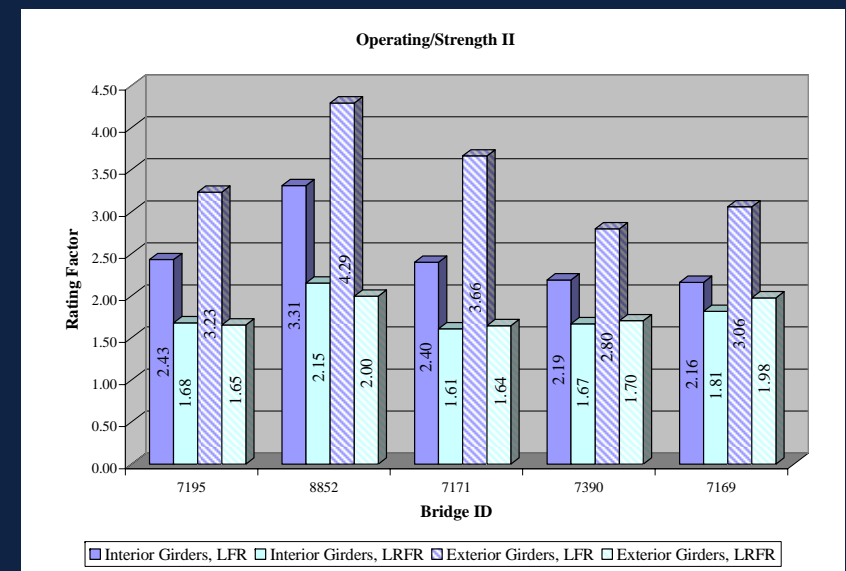
Note. Similar for all bridges: 1.) f'_{cslab} = 3 ksi and 2.) transverse reinforcement consists of #4 double leg stirrups.

Results

Critical Rating Factors - Flexure



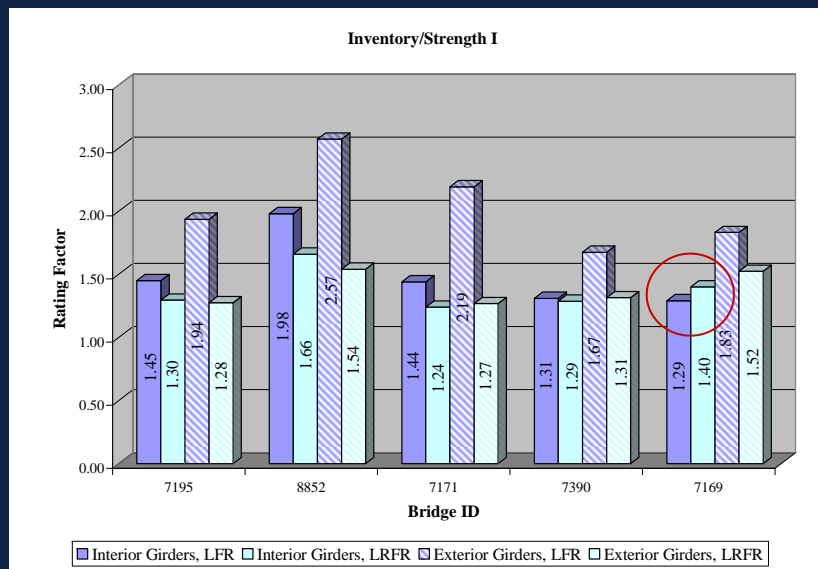
Inventory / Strength I



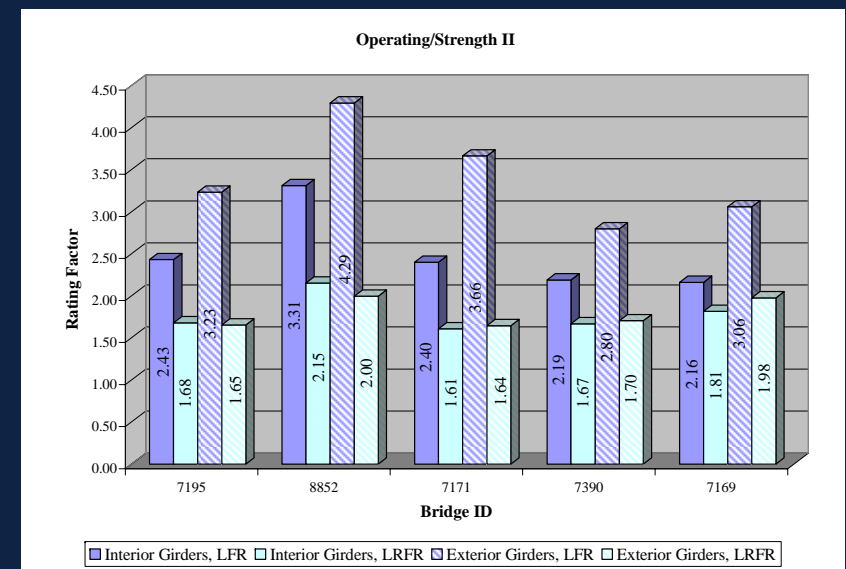
Operating / Strength II

Results

Critical Rating Factors - Flexure



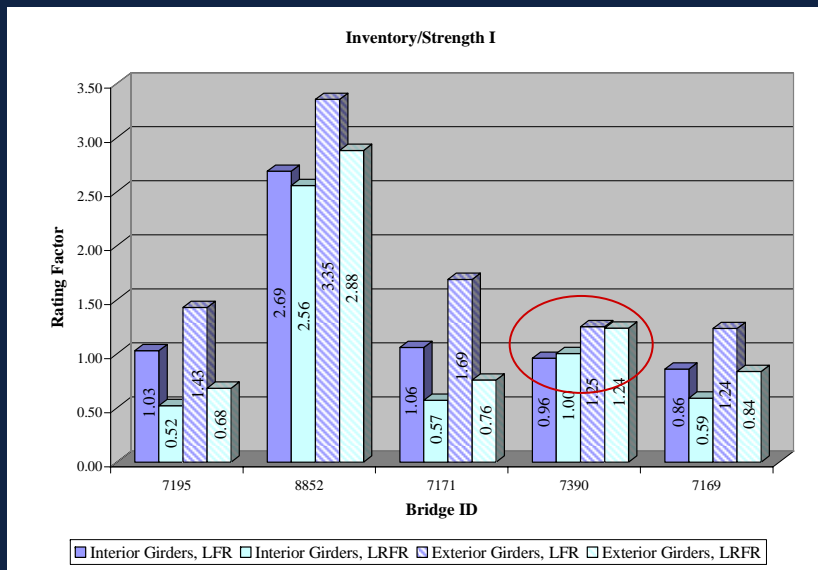
Inventory / Strength I



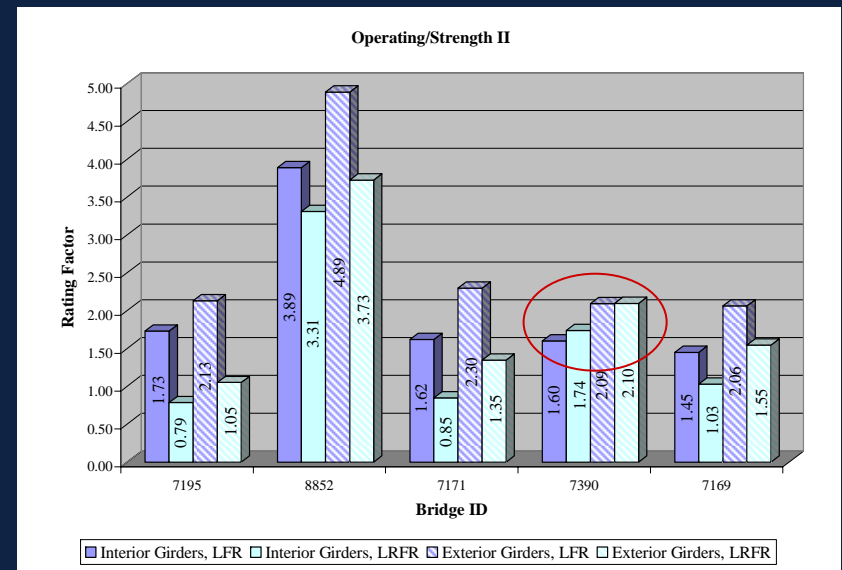
Operating / Strength II

Results

Critical Rating Factors - Shear



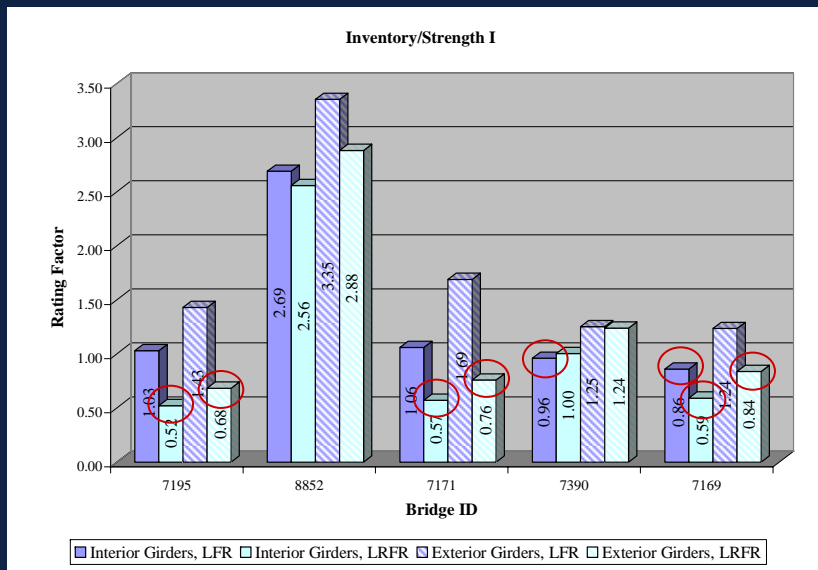
Inventory / Strength I



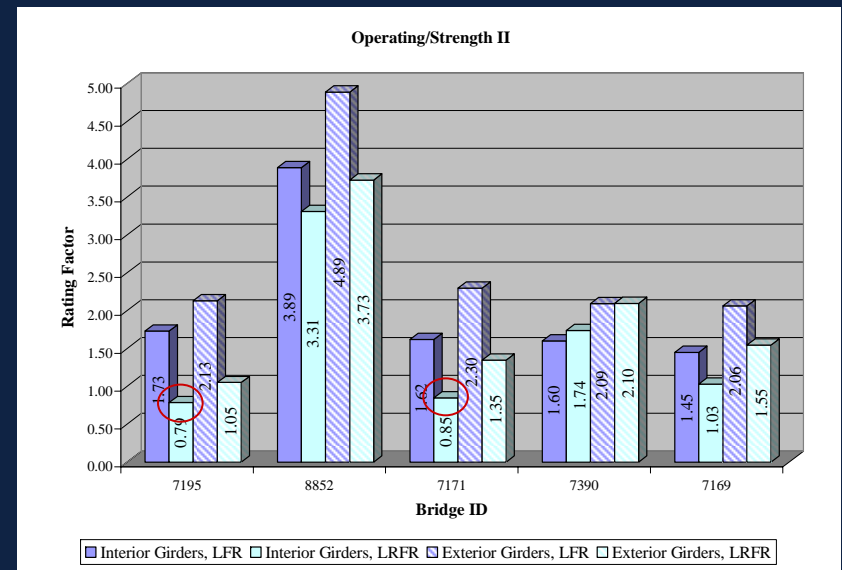
Operating / Strength II

Results

Critical Rating Factors - Shear



Inventory / Strength I

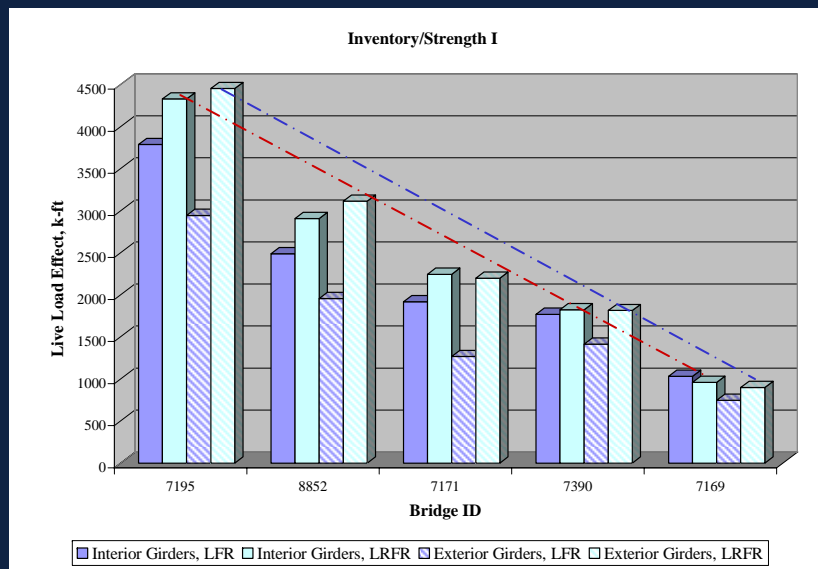


Operating / Strength II

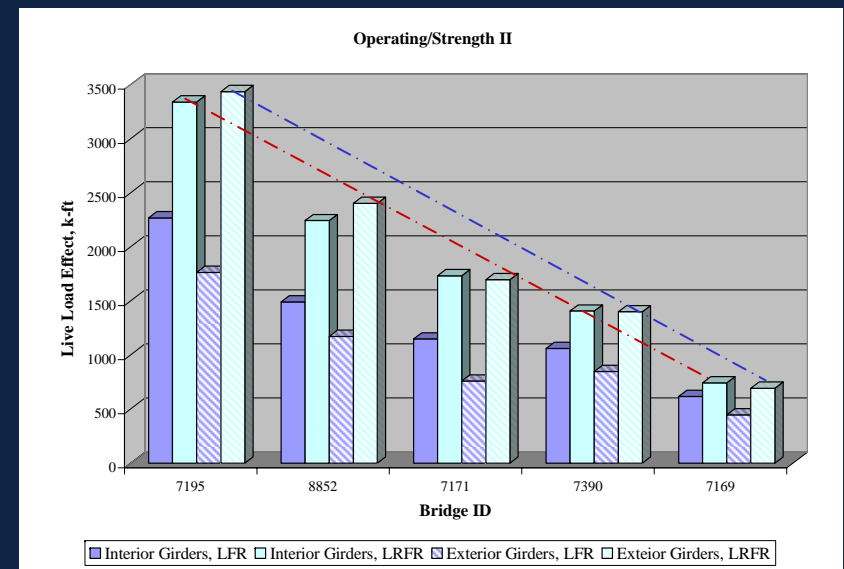
$$RF = \frac{\text{Capacity} - \text{DL Effects}}{\text{LL Effects}}$$

Results

Critical Live Load Effect - Flexure



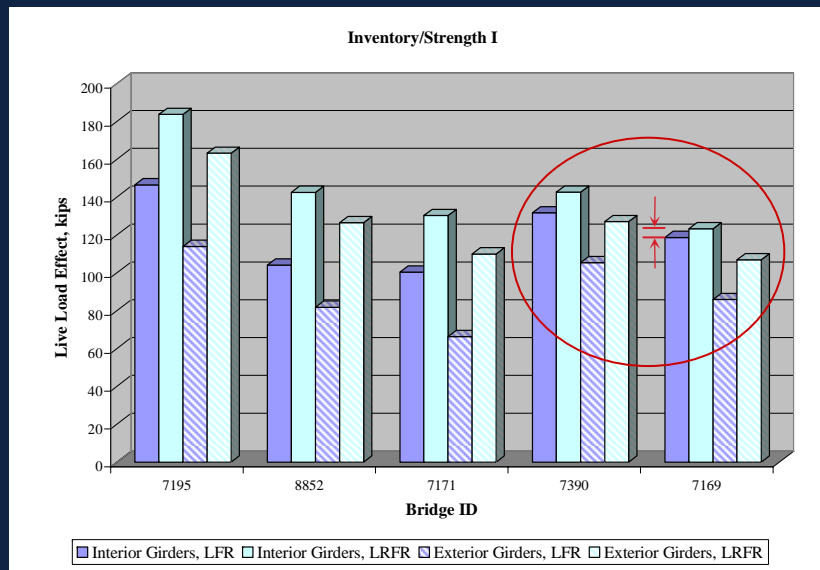
Inventory / Strength I



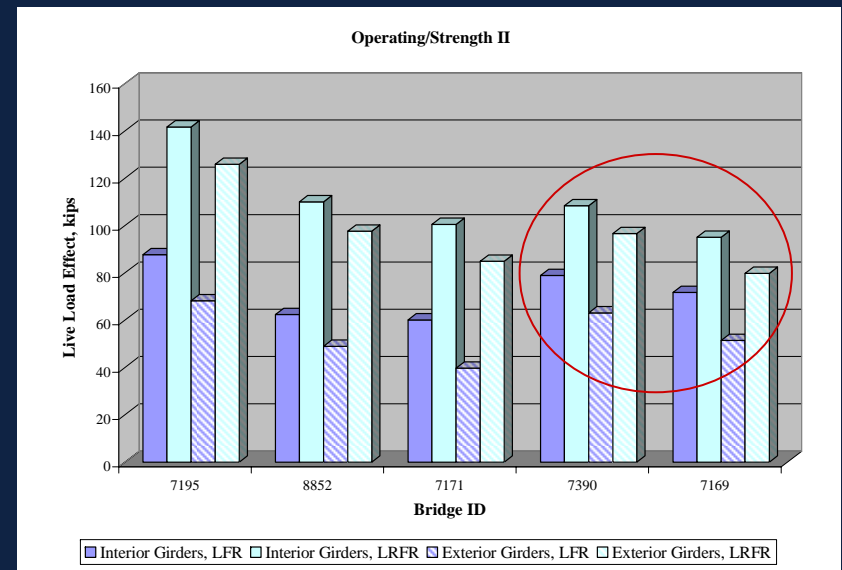
Operating / Strength II

Results

Critical Live Load Effect - Shear



Inventory / Strength I



Operating / Strength II

Results

Live Load Effects

- **Dynamic Load Allowance or Impact Factor**
 - **LFR:**
 - Based on span length
 - Ranges from 21.6% to 30% for the bridges under consideration
 - Shorter span bridges produce larger impact factor, therefore producing effects similar to LRFR
 - **LRFR: 33%**
- **Live Load Factors**

| LFR | LRFR |
|------------------|--------------------|
| Inventory – 2.17 | Strength I – 1.75 |
| Operating – 1.30 | Strength II – 1.35 |

Results

Live Load Effects

- Distribution Factors**

| Distribution Factor | Girder | 7195 | 8852 | 7171 | 7390 | 7169 |
|----------------------------|---------------|-------------|-------------|-------------|-------------|-------------|
| LFR | Interior | 0.871 | 0.636 | 0.606 | 0.826 | 0.886 |
| | Exterior | 0.677 | 0.500 | 0.400 | 0.661 | 0.641 |
| LRFR – Shear | Interior | 0.924 | 0.719 | 0.719 | 0.890 | 0.935 |
| | Exterior | 0.820 | 0.660 | 0.607 | 0.793 | 0.810 |
| LRFR - Moment | Interior | 0.798 | 0.616 | 0.620 | 0.797 | 0.834 |
| | Exterior | 0.820 | 0.660 | 0.607 | 0.793 | 0.780 |

Results

Live Load Effects

- Distribution Factors

| Girder Spacing | | S=9'7" | | | S=9'1" | S=9'9" |
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Live Load Effects

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LRFR – Flexure: Similar for Interior and Exterior Girders

Results

Live Load Effects

- Distribution Factors**

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LRFR – Flexure: Similar for Interior and Exterior Girders

LRFR – Shear: Smaller for Exterior Girder

Results

Live Load Effects

- Distribution Factors**

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LRFR – Flexure: Similar for Interior and Exterior Girders

LRFR – Shear: Smaller for Exterior Girder

LFR: Smaller for Exterior Girder

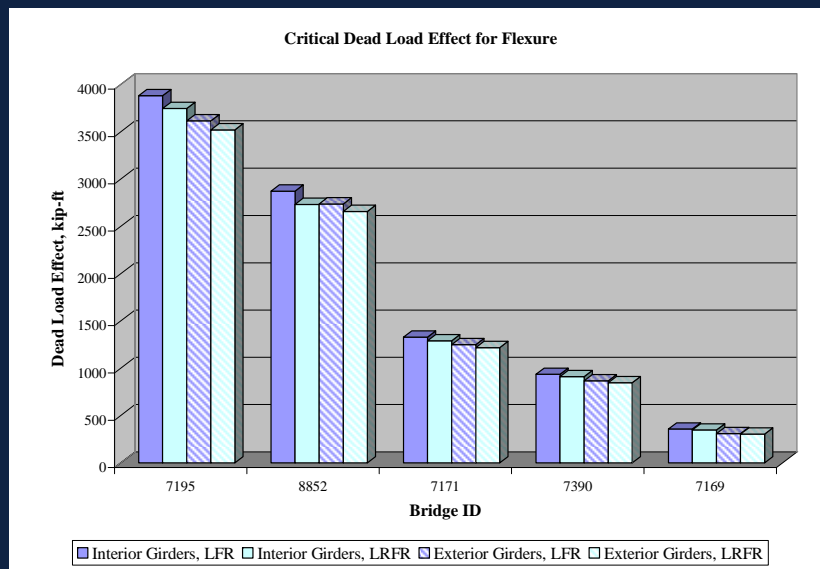
Results

Live Load Effects

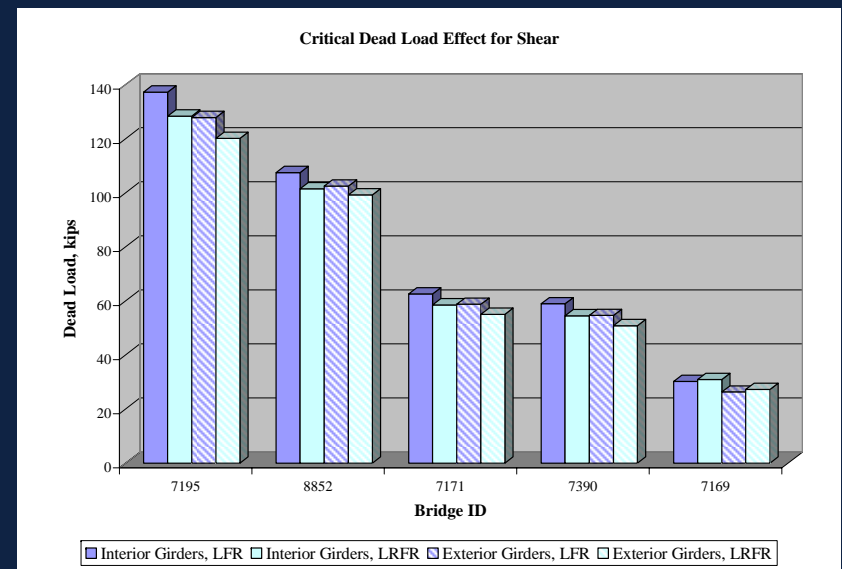
- **Design Loads**
 - **LRFR: HL-93**
 - **LFR: HS-20**
- **Effects of Skew**
 - **Only considered in LRFR for skews $\geq 30^\circ$**
 - **With the exception of Bridge 7169, the effects of skew are negligible.**
 - **Bridge 7169 was designed with a skew of 30° , therefore slightly reducing the distribution factor.**

Results

Critical Dead Load Effect



Flexure



Shear

Results

Critical Dead Load Effect

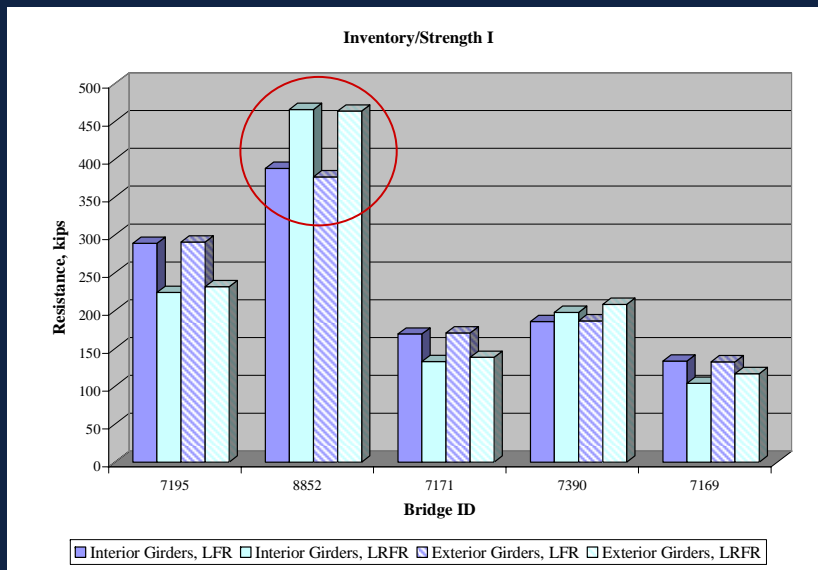
- **Dead Load Factors**
 - LFR: 1.3
 - LRFR: 1.25DC + 1.50DW
- **Dead load effects due to shear are affected by the location of the critical section.**

| Method | Level/ Limit State | Bridge ID | | | | |
|--------|---------------------|-----------|--------|--------|--------|--------|
| | | 7195 | 8852 | 7171 | 7390 | 7169 |
| LFR | Inventory/Operating | 100.27 | 100.46 | 100.26 | 100.38 | 100.95 |
| LRFR | Strength I | 100.42 | 100.49 | 100.44 | 100.60 | 100.73 |
| | Strength II | 100.46 | 100.46 | 100.48 | 100.70 | 100.73 |

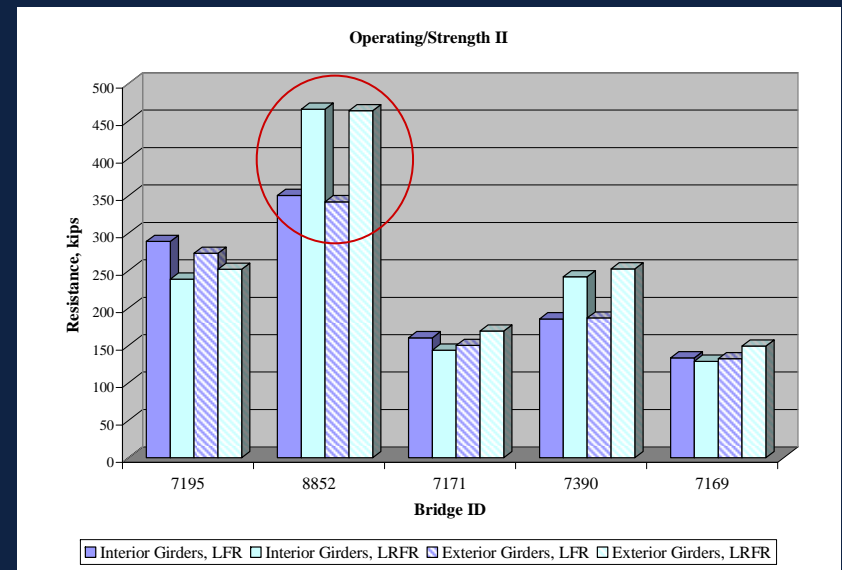
Larger critical sections result in smaller dead loads since the point of interest is further from the support.

Results

Critical Resistance - Shear



Inventory / Strength I



Operating / Strength II

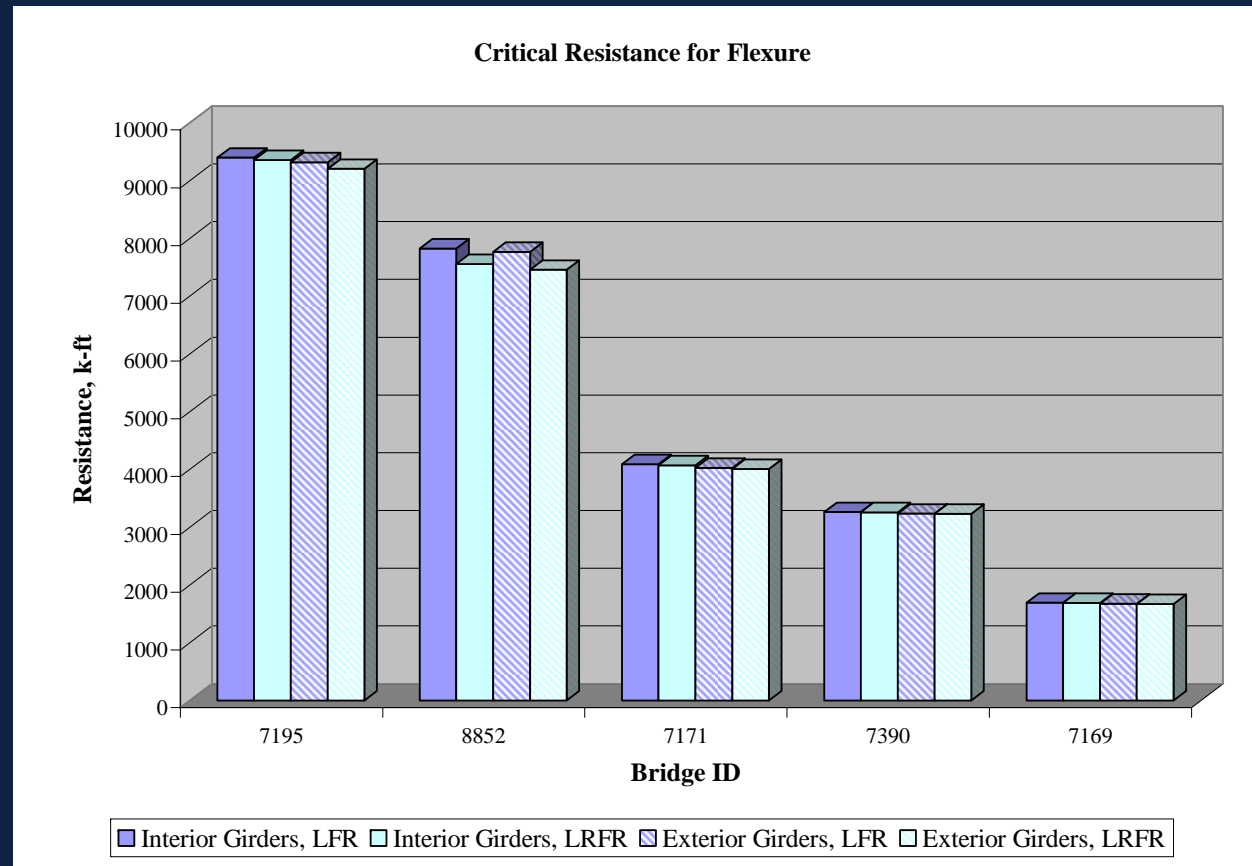
Results

Critical Resistance - Shear

- **Notable differences between LFR and LRFR**
 - Angle of compressive stresses, θ
 - Location of critical section
- **Notable differences in Figure (Critical Shear Resistance)**
 - Concrete Compressive Strength
 - Stirrup Spacing
 - Strand Type: low-relaxation vs. stress relieved
- **General Comparisons**
 - Shear resistance depends on an interaction of variables

Results

Critical Resistance – Flexure



Conclusions Contributing Parameters

- **Flexure**
 - **Contributing Parameters: Live Load Effects**
 - **Negligible Parameters: Dead Load Effects and Flexural Resistance**
- **Shear**
 - **Contributing Parameters: Live Load Effects and Shear Resistance**
 - **Negligible Parameters: Dead Load Effects**

Conclusions

Comparison of Rating Factors - Flexure

- LRF method yielded lower rating factors, with the longer span bridges demonstrating a larger deviation between LFR and LRF
- Operating/Strength II limit state showed greater variance between LFR and LRF when compared to Inventory/Strength I limit state
- LRF produced similar rating factors between the interior and exterior girders
- LFR yielded larger rating factors for the exterior girders
- Exterior girders showed a larger discrepancy between rating method (LFR vs. LRF)
- All five bridges are structurally adequate (i.e. rating factor > 1)

Conclusions

Comparison of Rating Factors - Shear

- LRF method yielded lower rating factors
- Operating/Strength II ratings displayed a more notable difference in rating method than Inventory/Strength I
- LFR and LRF rating factors are greater for the exterior girders with LFR yielding a larger discrepancy in values between the exterior and interior girders
- A number of bridges are structurally inadequate (i.e. rating factor < 1.0)

Conclusions

General Comparisons

- **LRFR method generally resulted in lower rating factors for flexure and shear**
- **The shorter span bridges were often controlled by the LFR method**
- **The shear ratings typically controlled over the flexure ratings**

Recommendations

- **Further investigation of the contribution of the concrete to the shear resistance is recommended**
- **Further research relating to LRFR is suggested. Parameters not studied in this research should be considered, in particular continuous span bridges. Larger samples are recommended**
- **Further comparison of the applied live loads, in particular permit loads, is recommended**

Acknowledgements

- **The authors would like to thank the New Mexico Department of Transportation (NMDOT) and the Wyoming Department of Transportation (WYDOT) for supplying the NM bridge plans/other supplementary information and the Bridge Rating and Analysis of Structural Systems (BRASS) software, respectively**
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Thank You