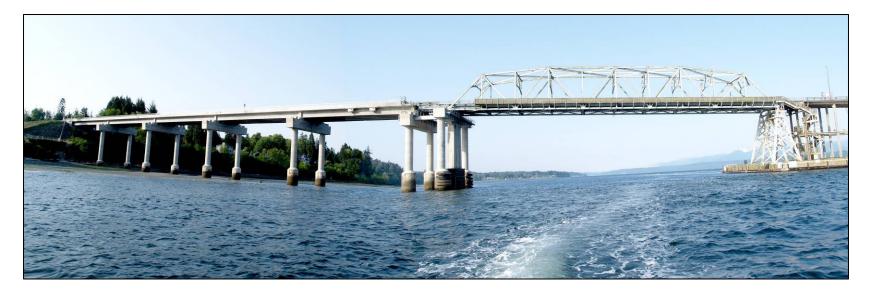
# **Hood Canal Bridge**

#### **East and West Approach Span Replacement**



Joseph Merth, P.E. Bridge Design Engineer

24 September 2007



## Overview

- Introduction
- Current Project
- Approach Design
- Approach Construction
- Challenges



Floating Structure 24 sept 07

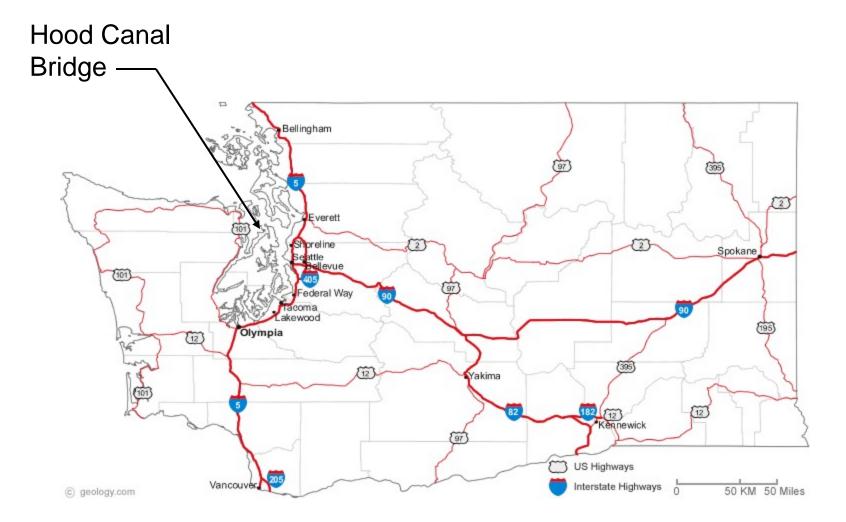


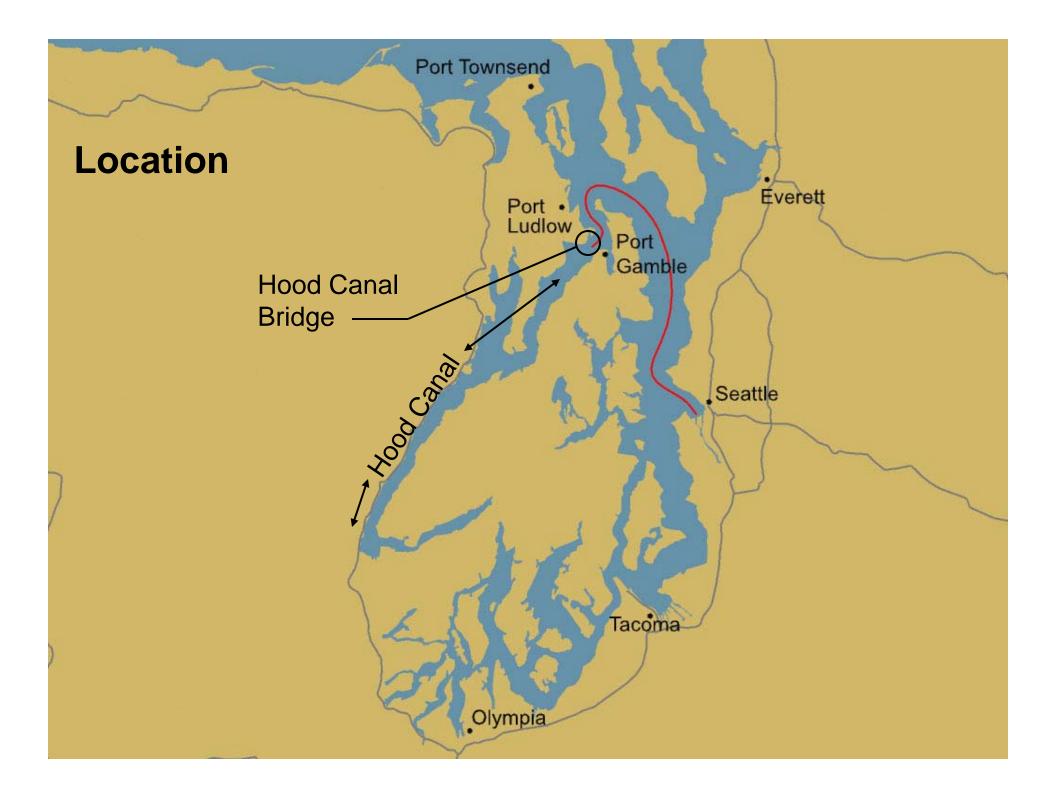
East Approach

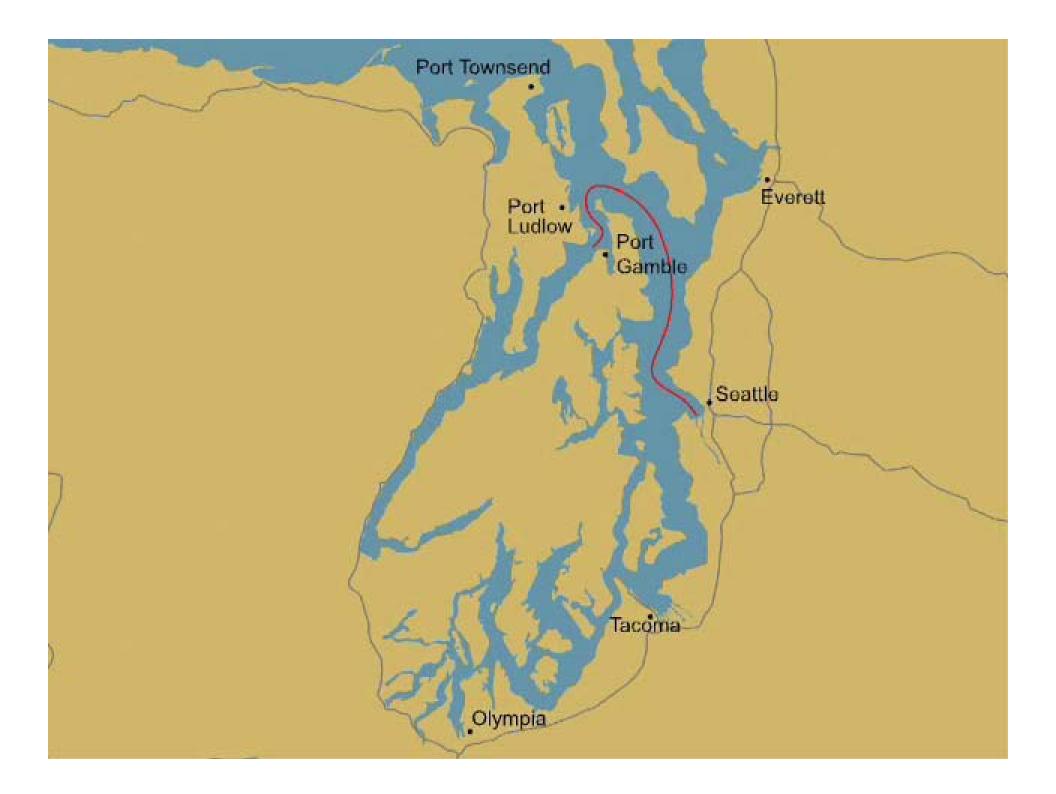


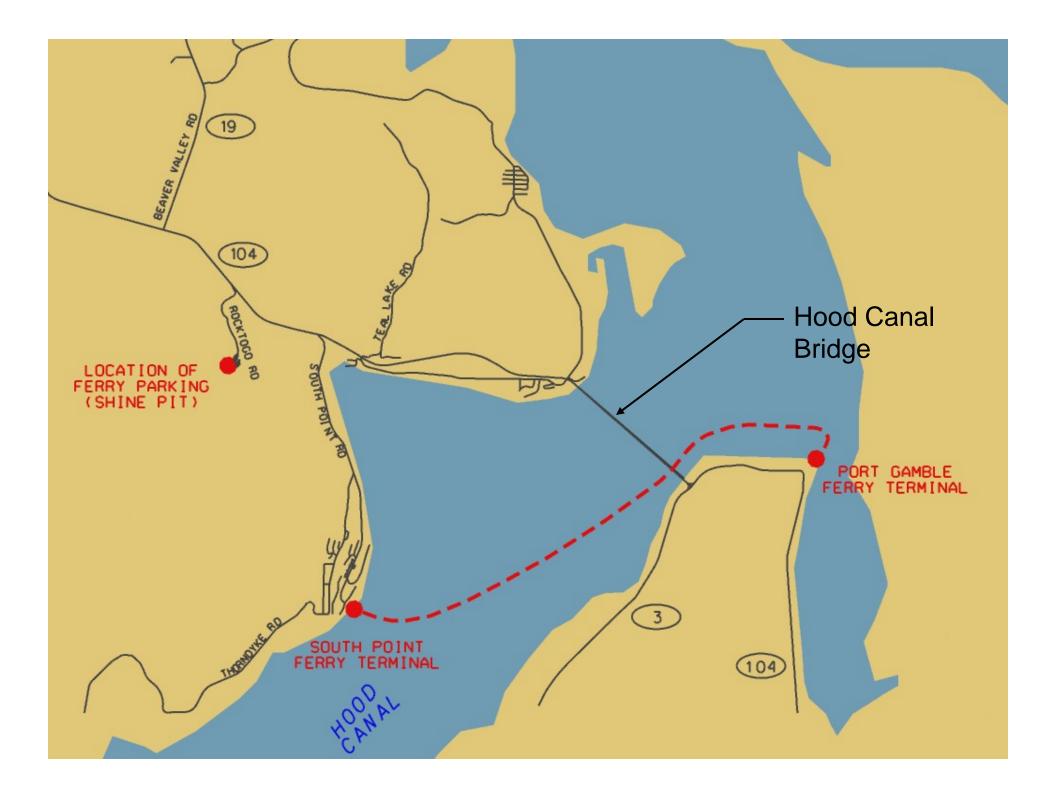
West Approach

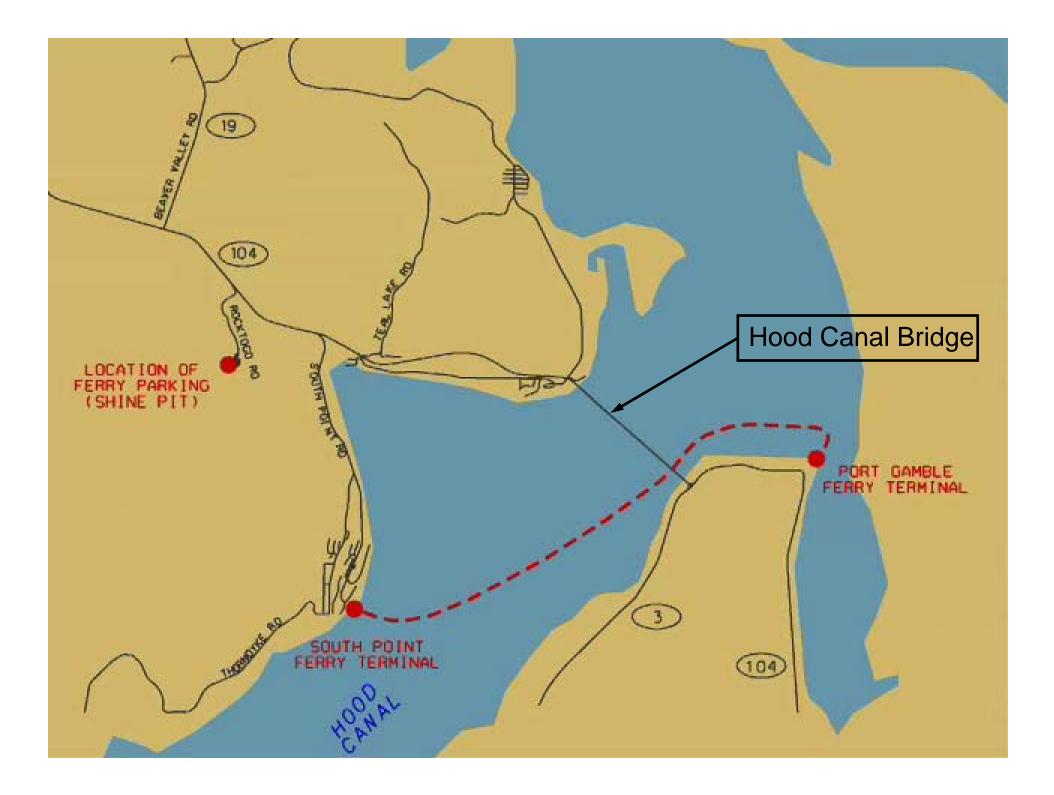
### Location

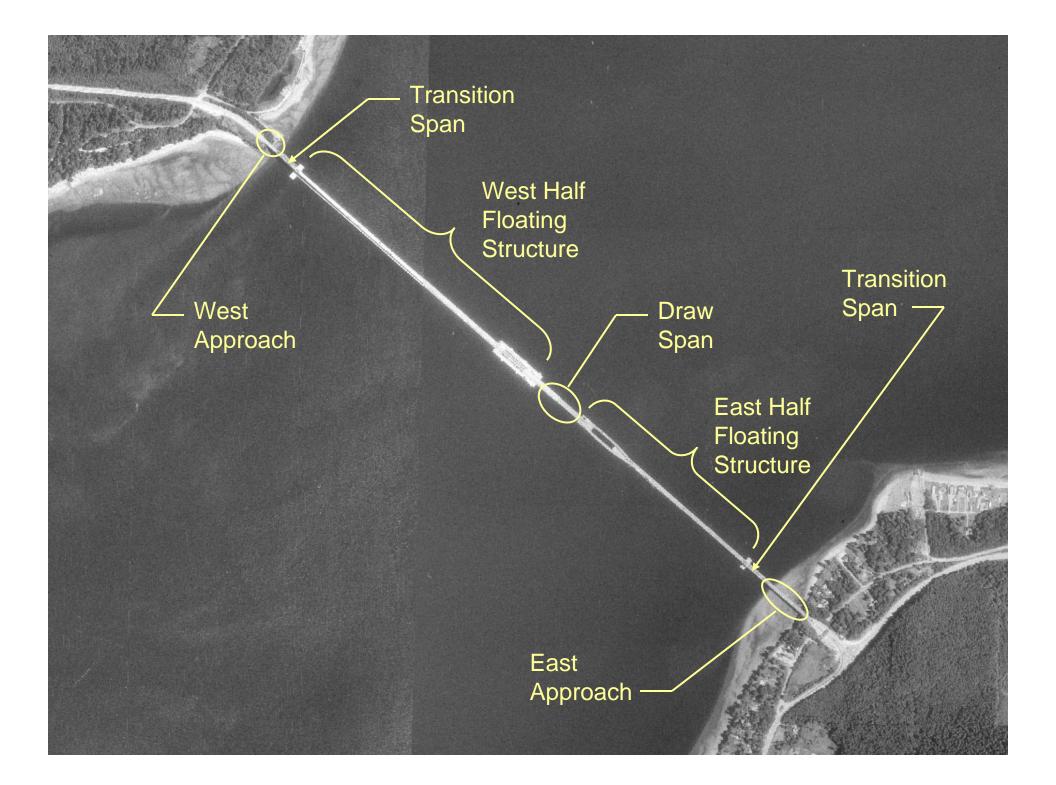












### **Bridge Facts**

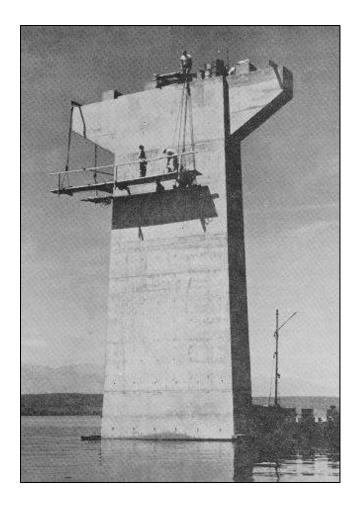


- Length 7869 feet
  (Longest floating bridge over salt water)
- Floating portion 6530 feet
- Max water depth 340 feet
- Tidal Variation 16.5 feet
- Center draw span opening 600 feet

## **Bridge History**

- Original Construction January 1958
- Open to traffic 12 August 1961





## **West Half Fails**

- February 13, 1979
- Sustained winds of 85mph
- 120mph gusts



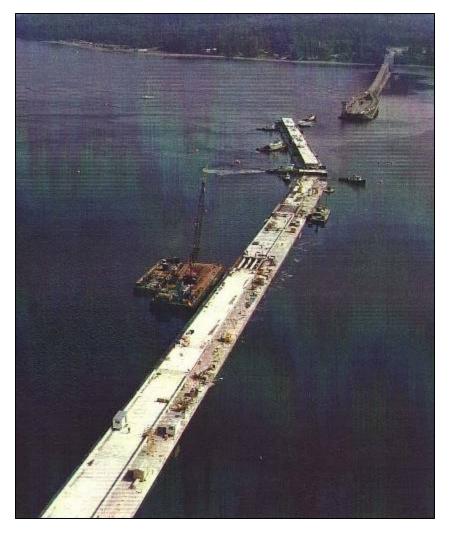




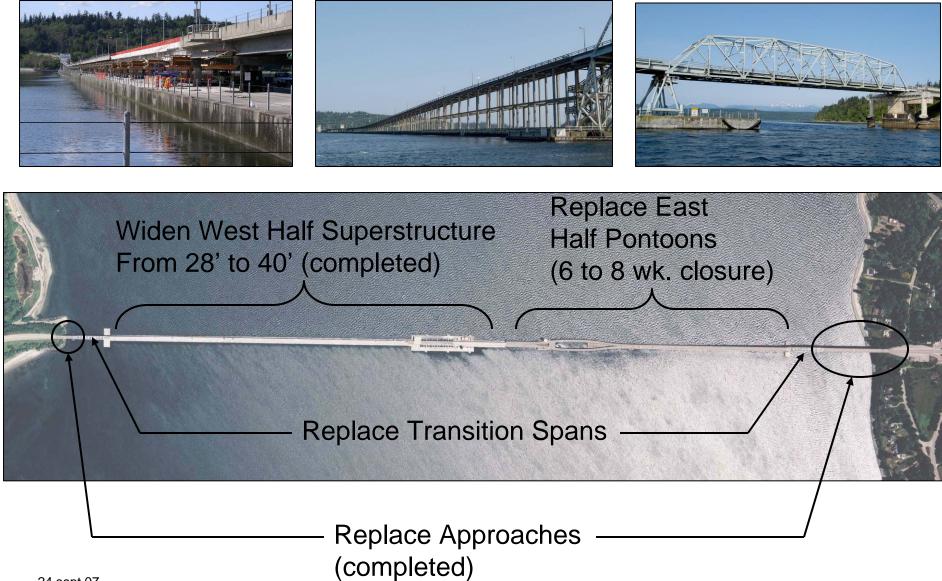
## West Half Replacement

- Reopened Oct. 25<sup>th</sup>, 1982
- Post-tensioned pontoons
- Increased anchor size



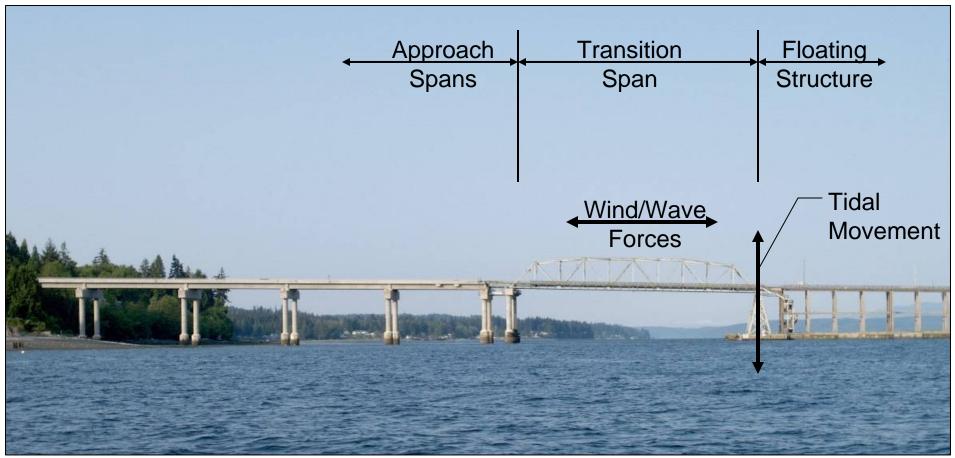


## **Current Project**



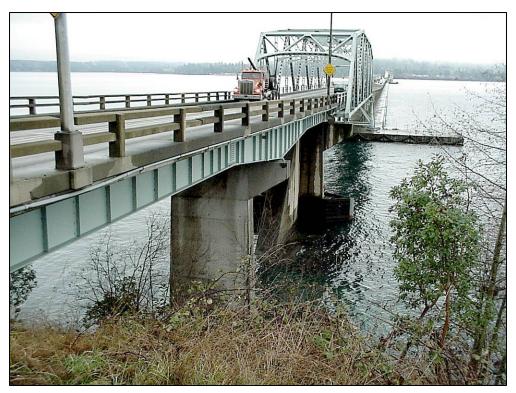
## Approaches

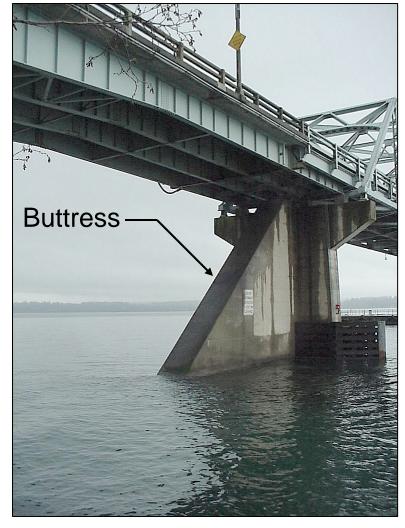
- Provide fixed link from shore to floating structure
- Help resist longitudinal wind and wave forces from the floating structure



## **Original West Approach**

- 2 span haunched steel PL Girder
- 190' length
- Buttress added for West half replacement

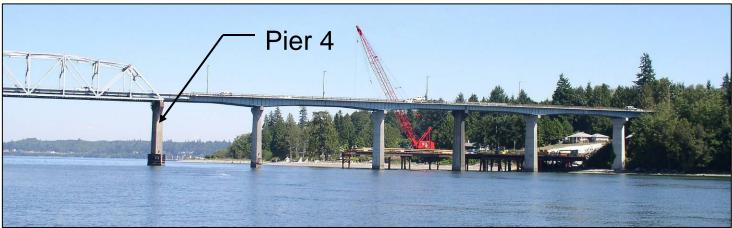




# Original East Approach

- 6 span haunched steel PL Girder
- 643' length
- Wind/Wave forces Pier 4





## **Approach Retrofit**

- Original Retrofit Requirement
  - Deck Replacement
  - Seismic Retrofit
  - Pier 4 retrofit (add buttress wall)
- Required 6-8 week closure





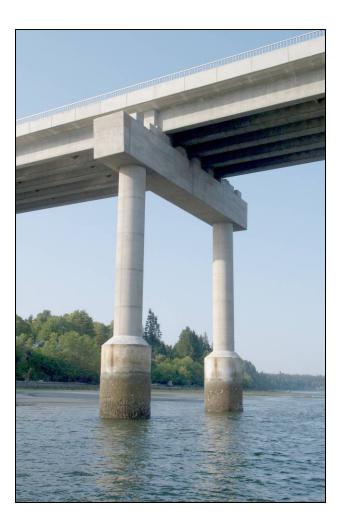
East

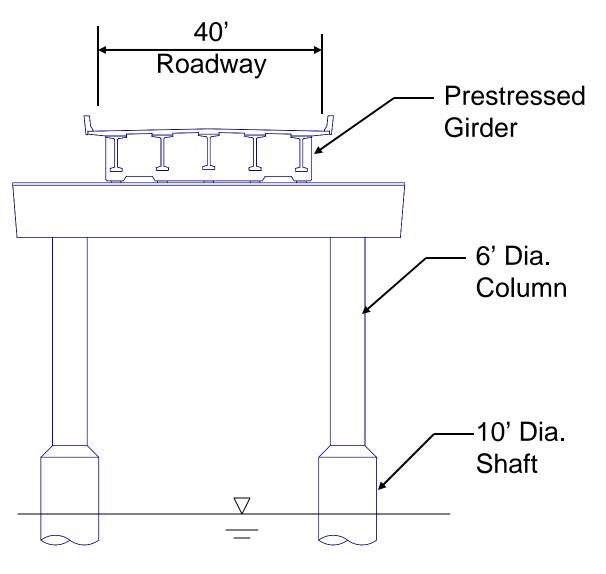
## **Approach Replacement**

- Replace entire approaches (superstructure/substructure)
- Build to current standards 40' roadway, seismic
- Ability to widen to 4 lanes (60') in the future



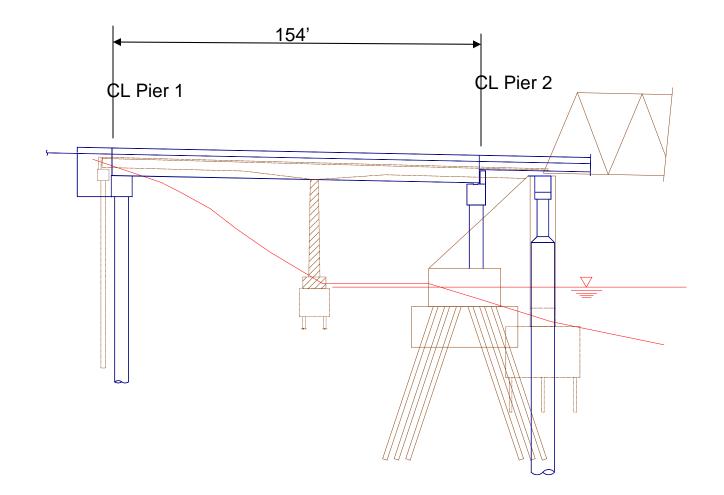
# Typical Section





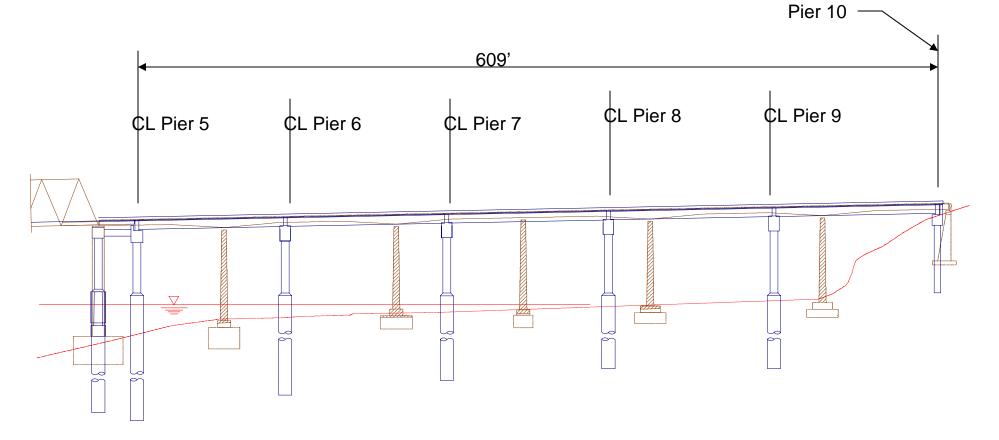
# **West Approach Elevation**

- 1 span (W83G Girders)
- 154' total length



## **East Approach Elevation**

- 5 spans (W74G Girders)
- 609' total length

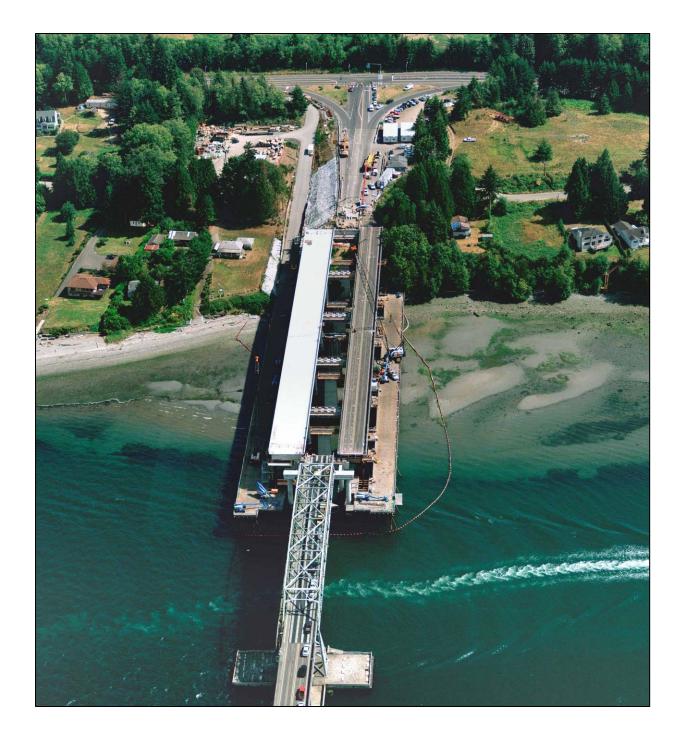


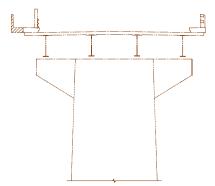
### **Replacement Challenges**

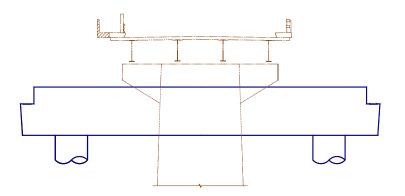
- Limited closure extended weekend
  - Construct superstructure adjacent to existing approach
- Distribute wind/wave forces into East Approach

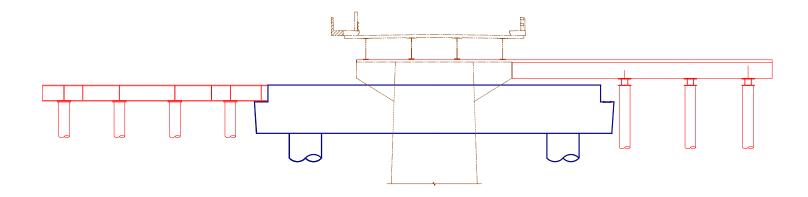


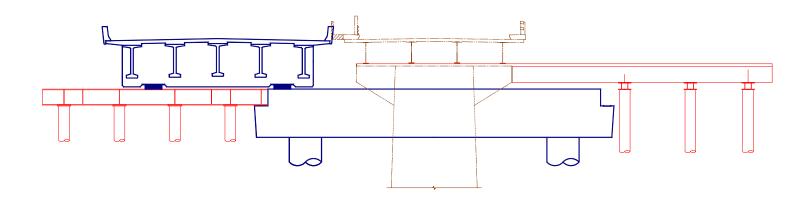
## Rolling Scheme

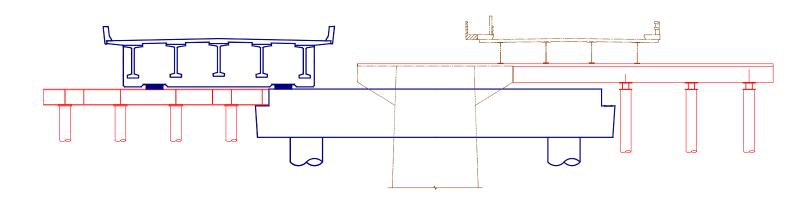


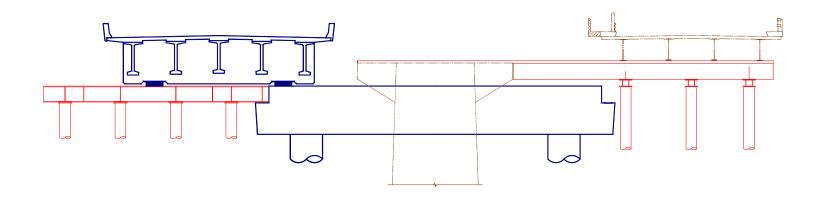


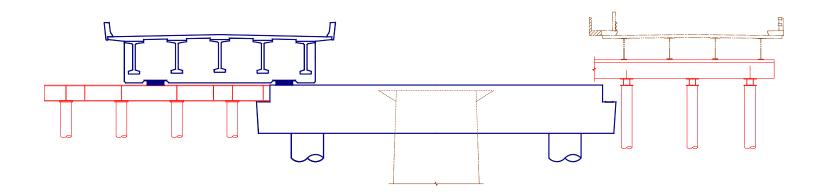


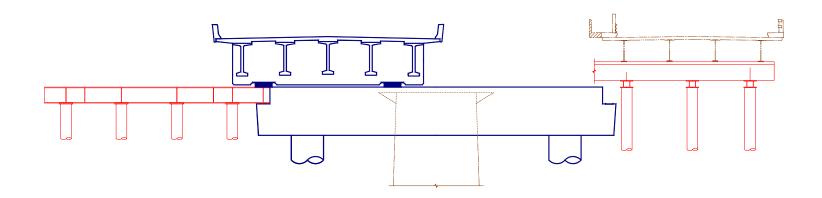


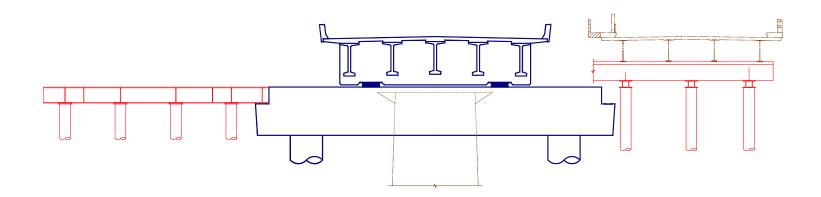




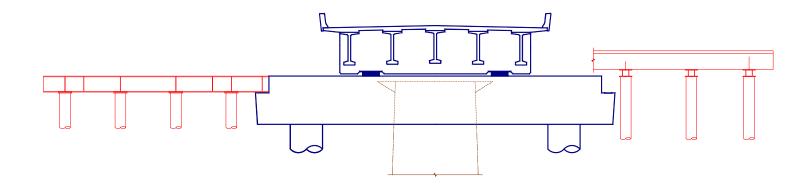




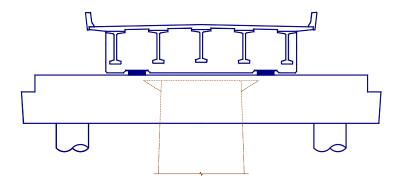




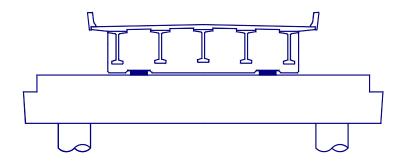
#### Rolling Scheme After Rollover



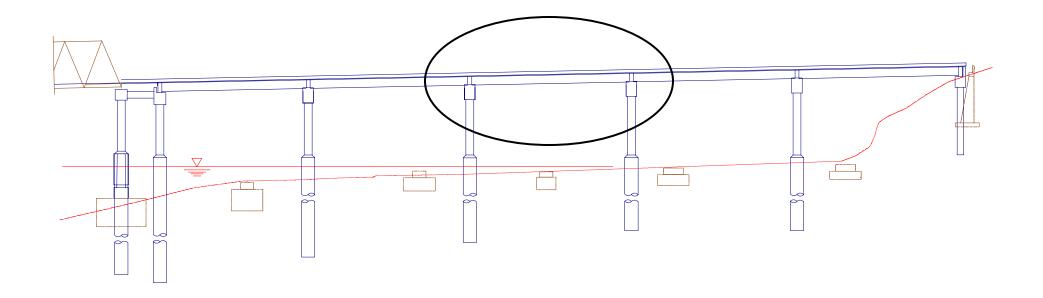
#### Rolling Scheme After Rollover

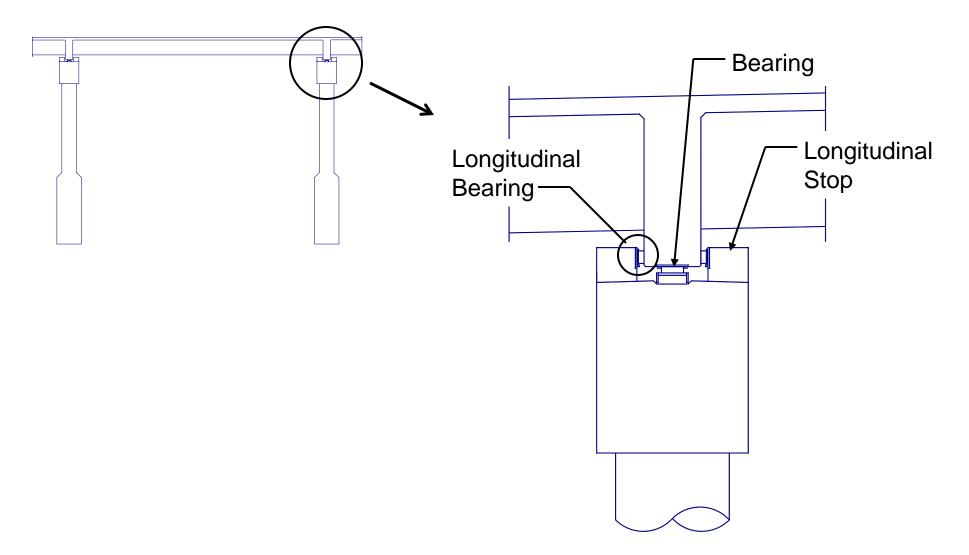


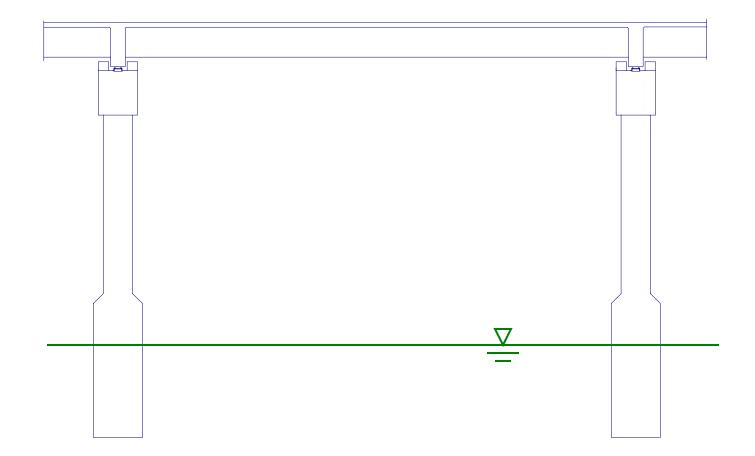
#### Rolling Scheme After Rollover

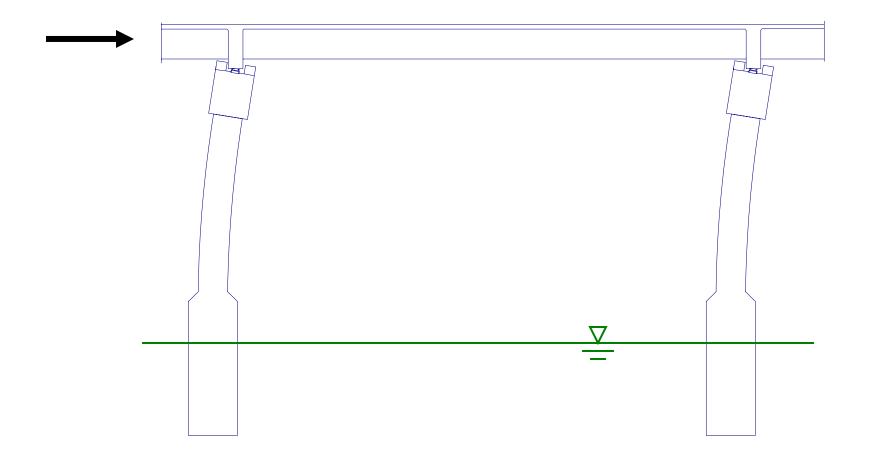


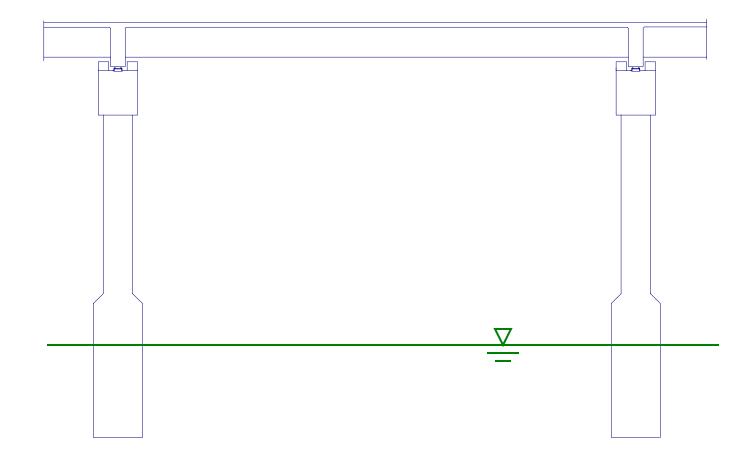
### Wind/Wave Forces

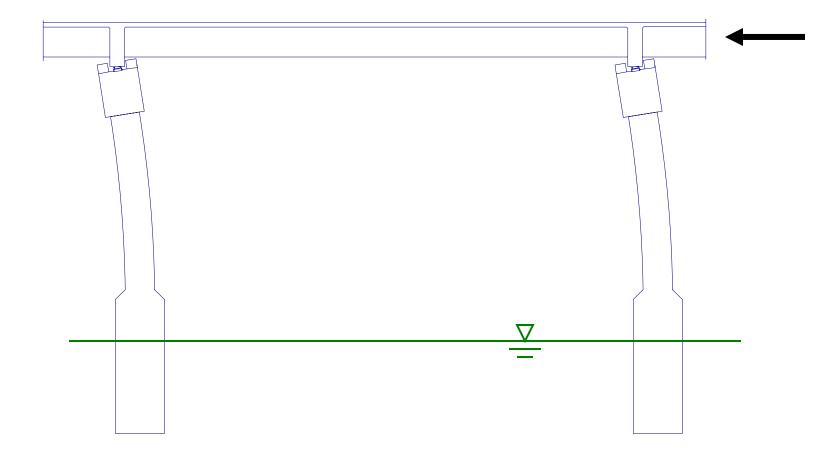


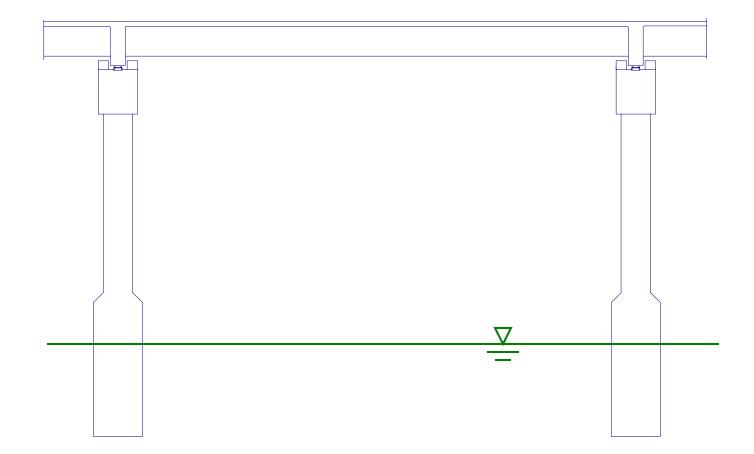




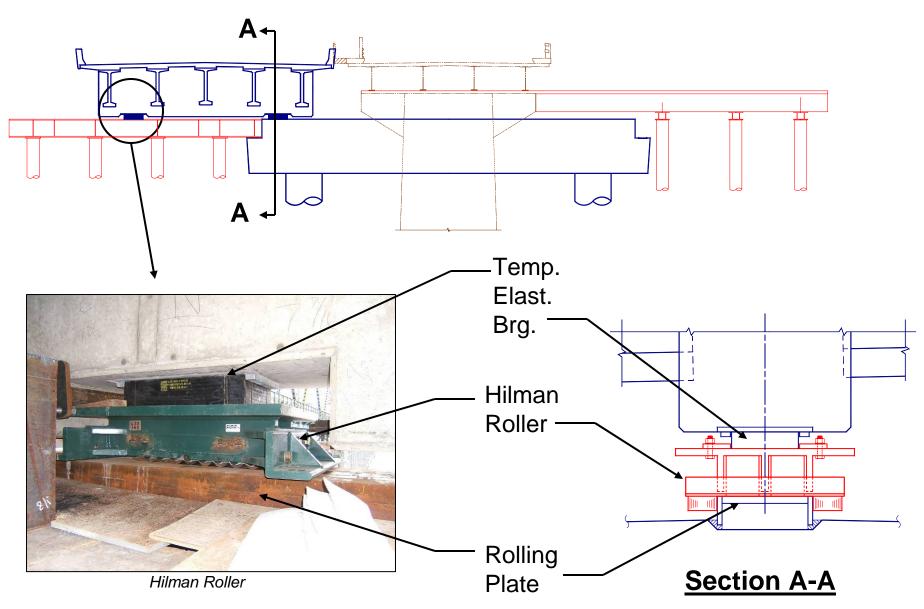




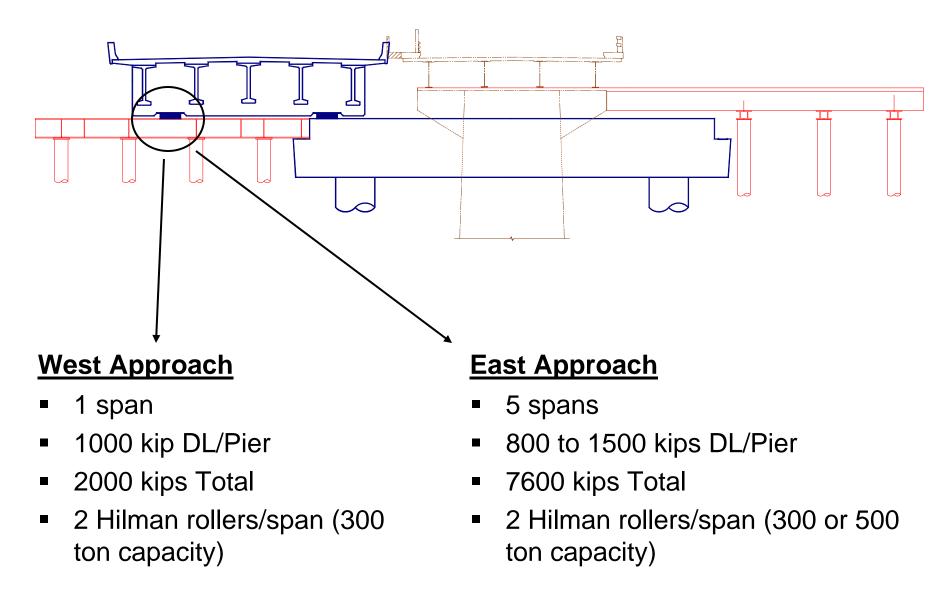




## **Rolling Assembly**



## **Hilman Rollers**

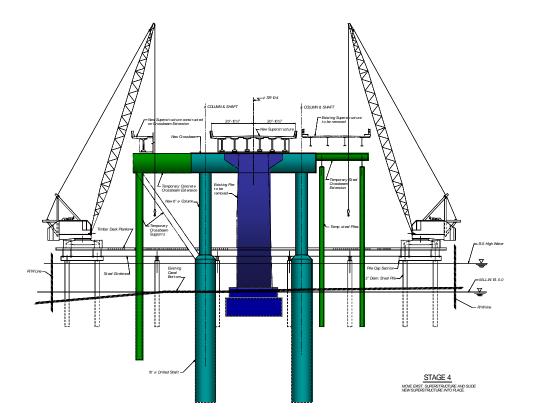


# Construction

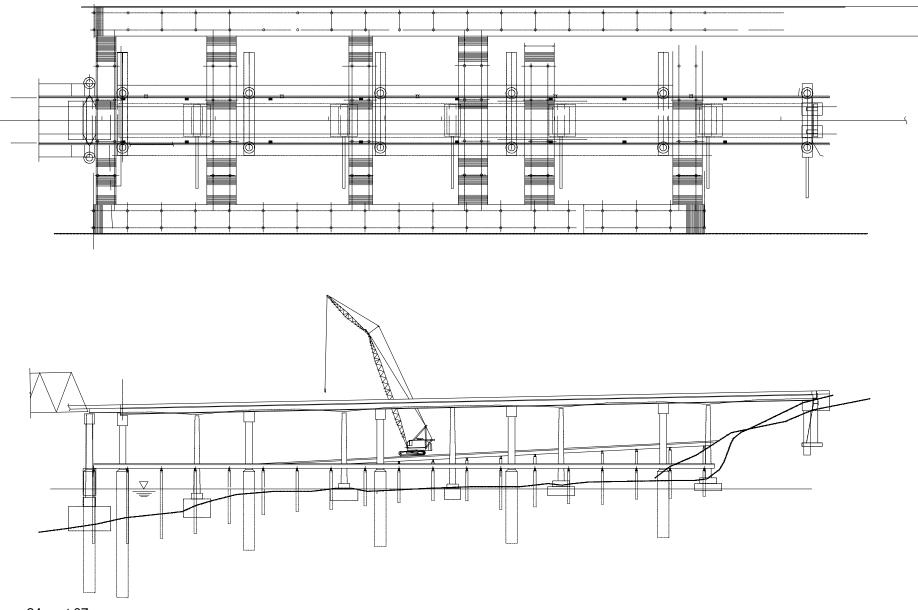


# **Work Trestle**

- Trestle and Falsework scheme included in Contract
- Contractor required to submit for review and approval
- Falsework system designed for ½ seismic acceleration (0.15g)

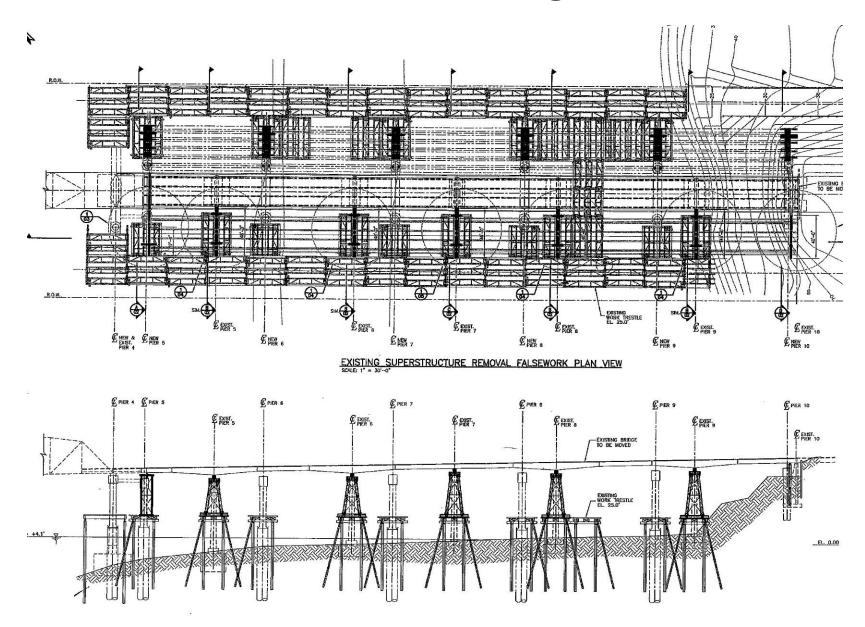


### **Work Trestle**



24 sept 07

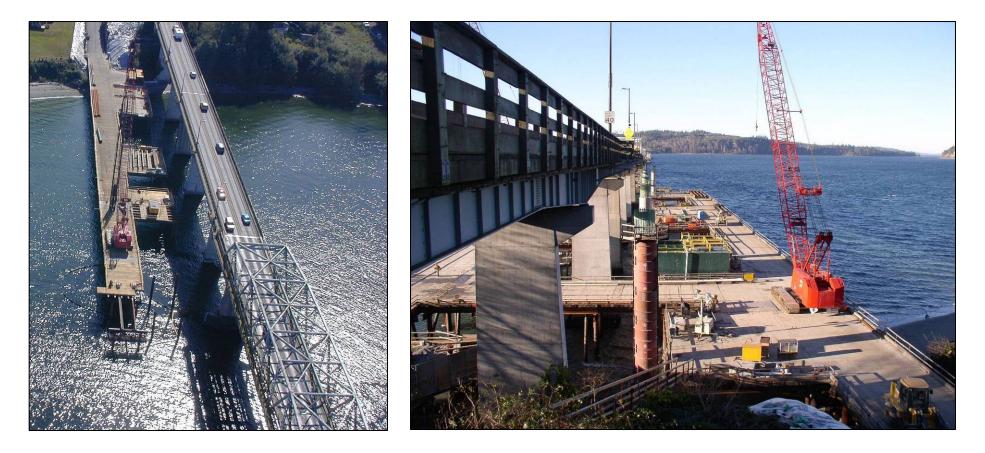
#### **Work Trestle – Contractor Design**



# **Work Trestle**

- 58,000 ft<sup>2</sup>
- 260 2' Diameter Piles
- 4 months to construct

#### East Approach



# Substructure

- 12 10' Diameter Shafts
- 5 ½ Months Construction
- Epoxy Coated Rebar Entire Structure





## Superstructure

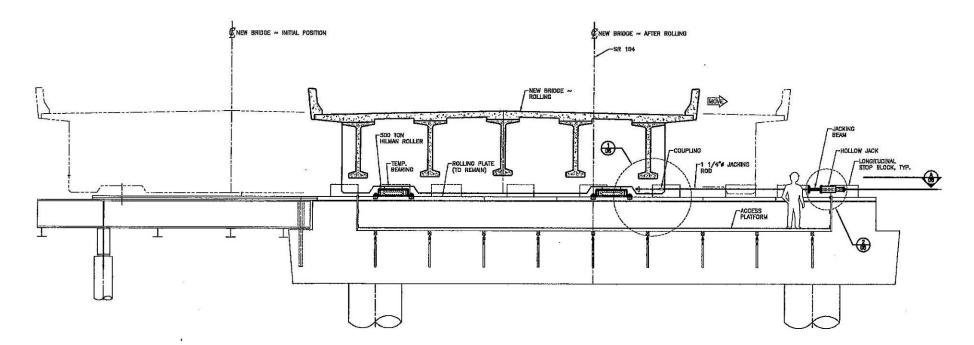


#### **The Rollover**

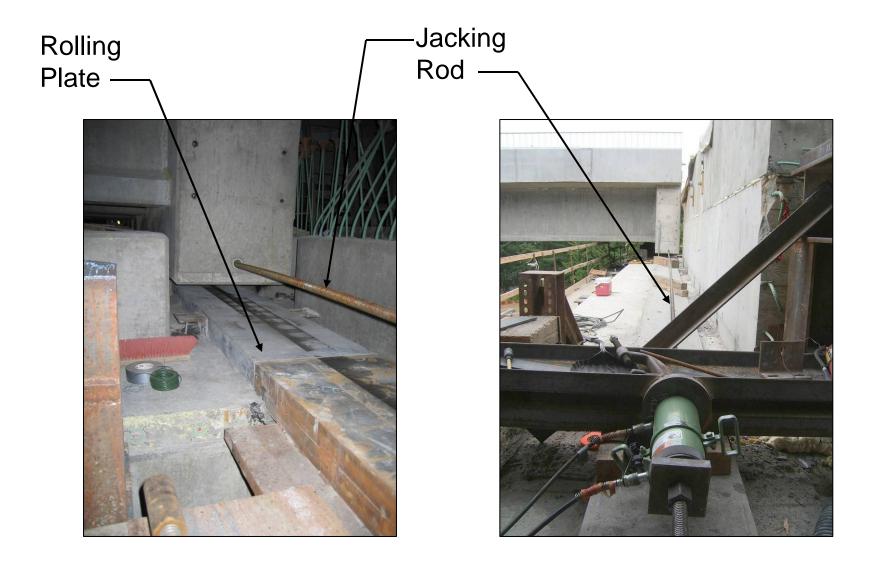


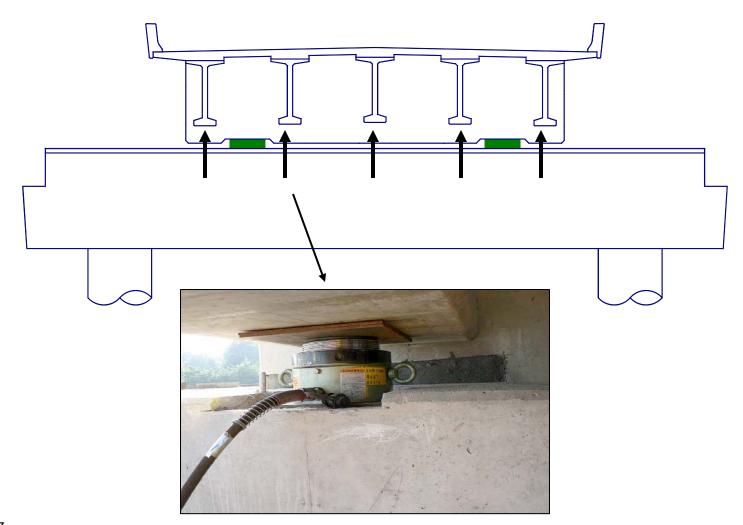
## Hydraulic Jacking – Horizontal

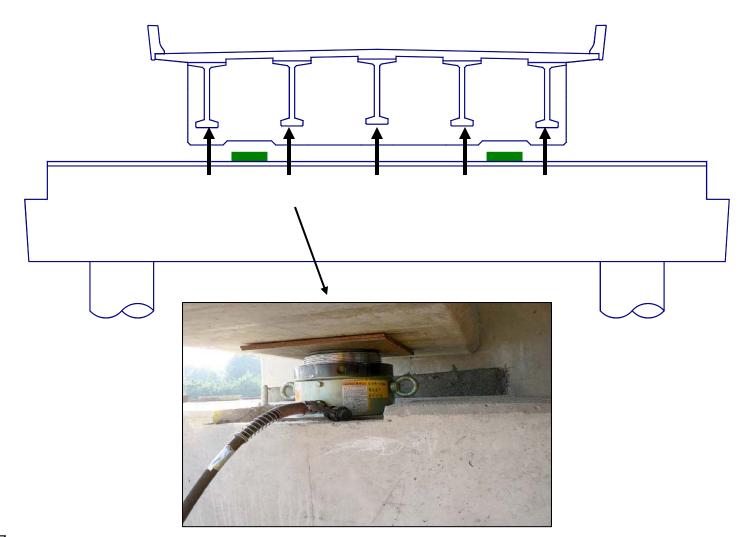
- West Approach 2 synchronized jacks
- East Approach 6 synchronized jacks
- Max horizontal force/jack 30 to 80 kips
- Max ¼" differential horizontal movement between adjacent piers during rolling

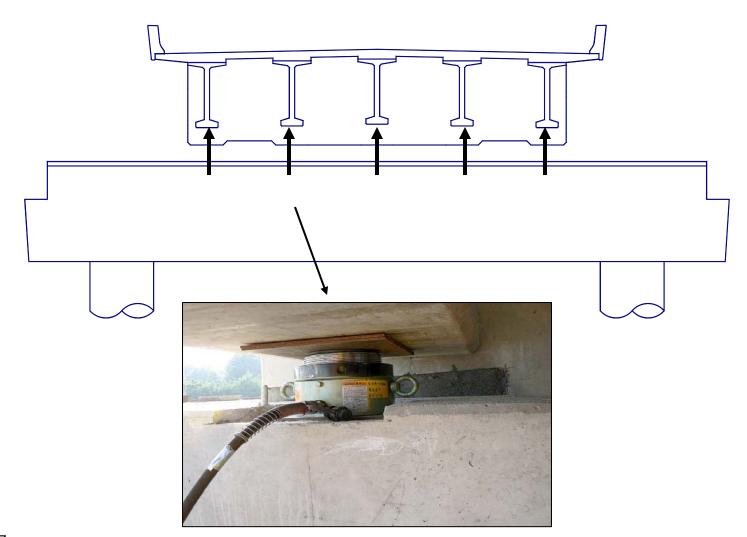


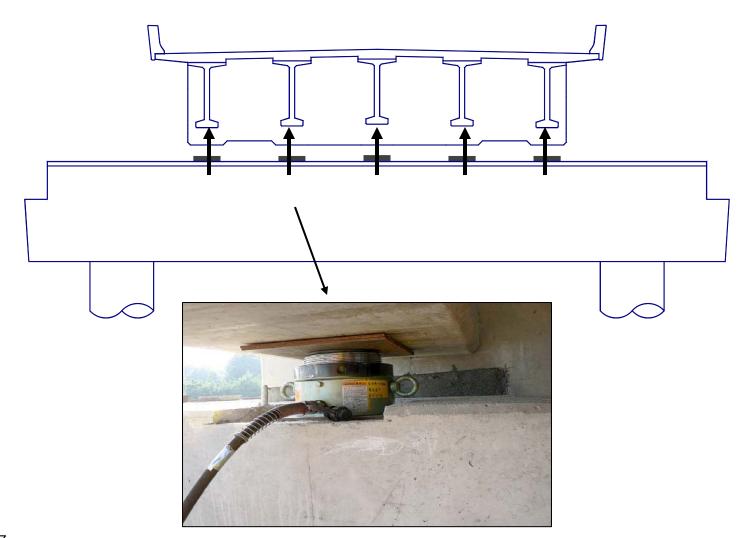
## Hydraulic Jacking – Horizontal

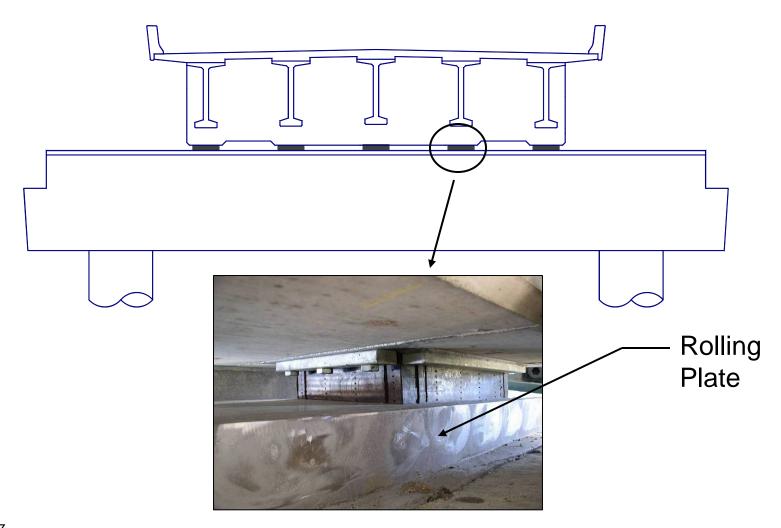




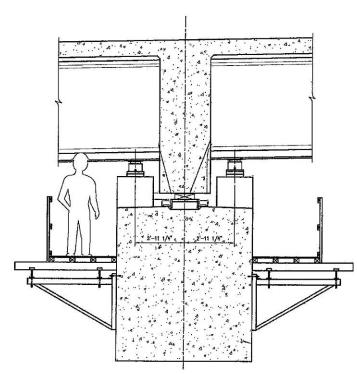


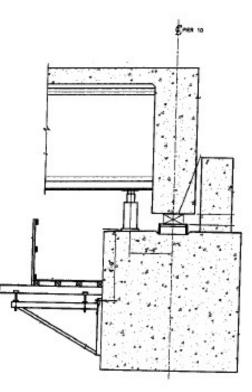




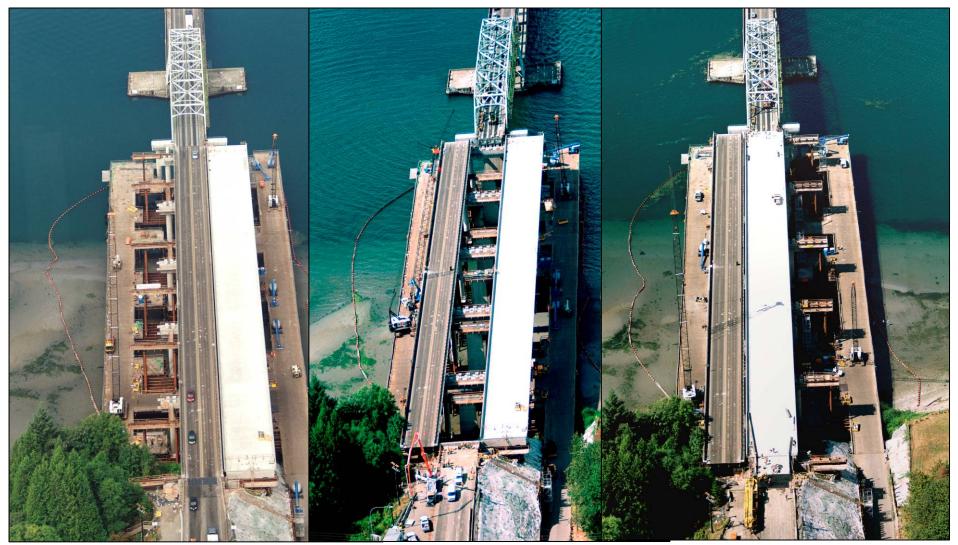


- Jacking performed pier by pier
- 10 synchronized jacks interior piers, 5 at end piers
- Max relative differential movement between jacks = ¼"
- Max relative differential movement between piers = 2"
- Pressure system used for vertical jacking





## **East Approach Aerial Photos**



Before

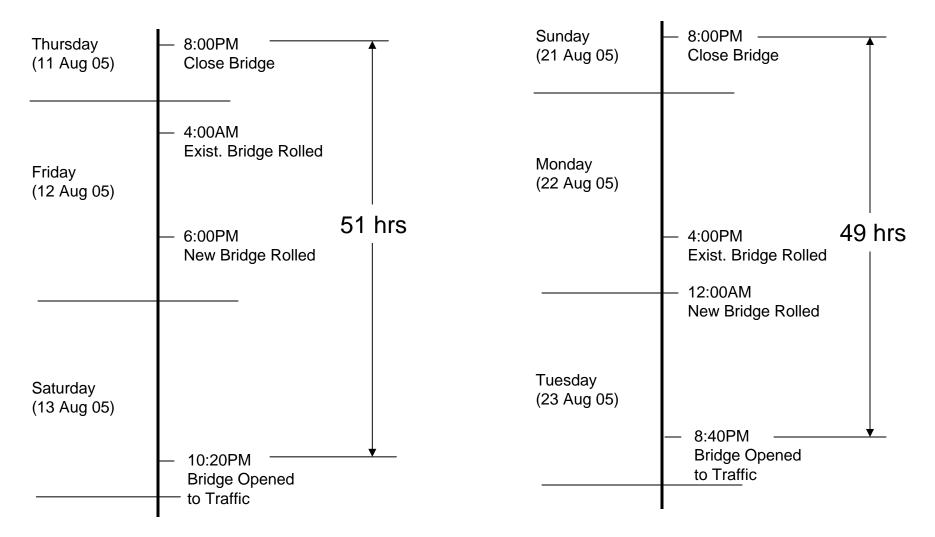
During

After

## **Approach Closure Schedule**

#### West Approach

#### **East Approach**



## **Closure Challenges**

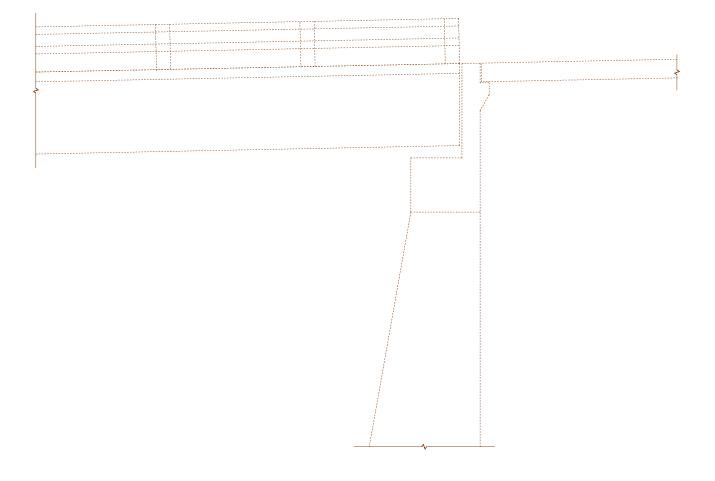


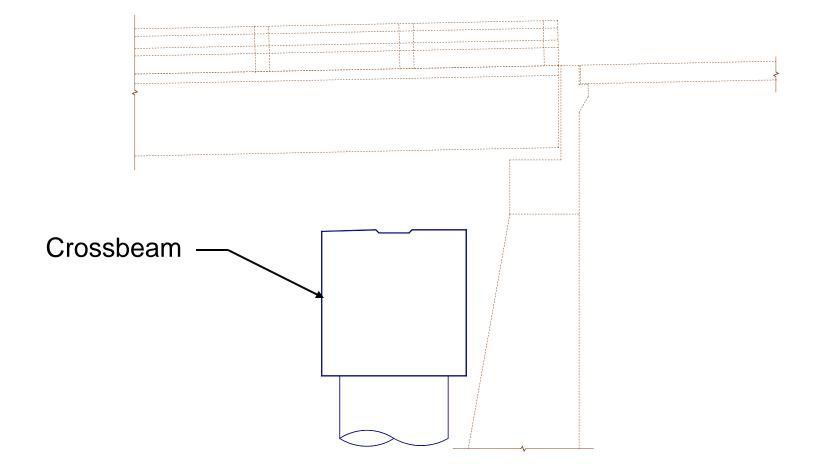
# Abutment and Approach Slabs

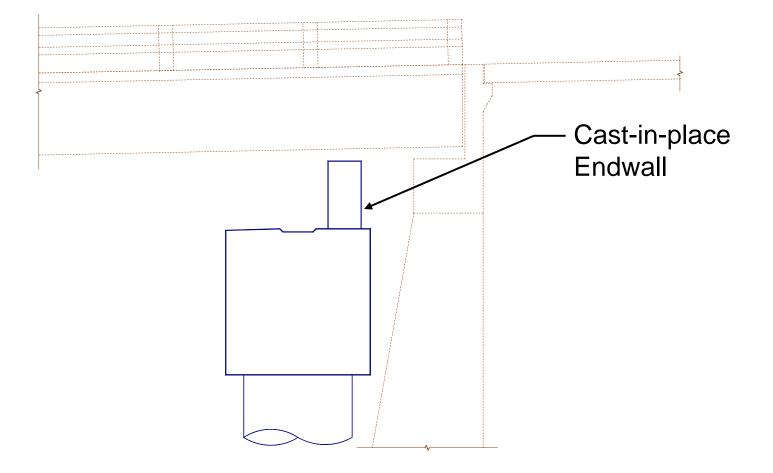
- Precast Abutment Endwall
- Precast Approach Slabs

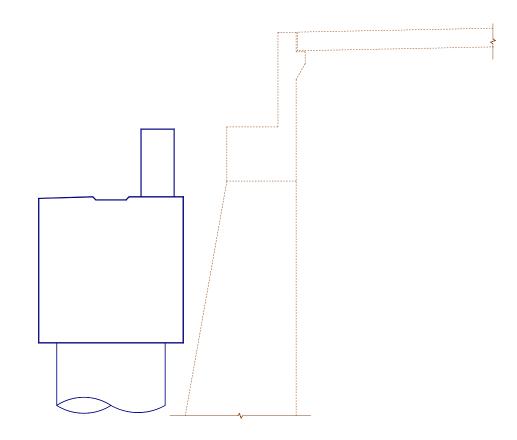


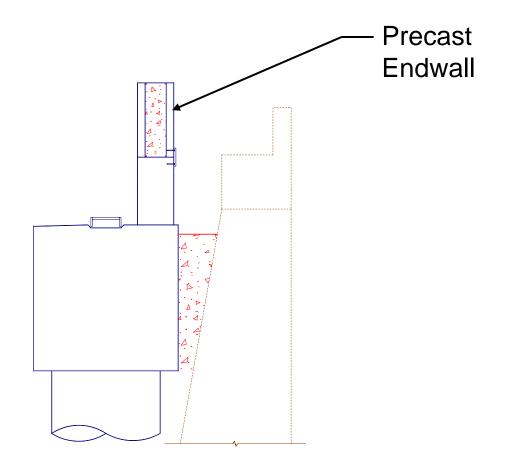


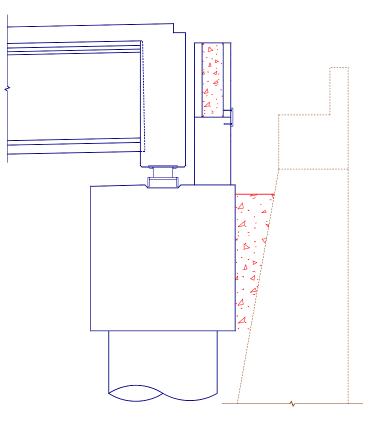


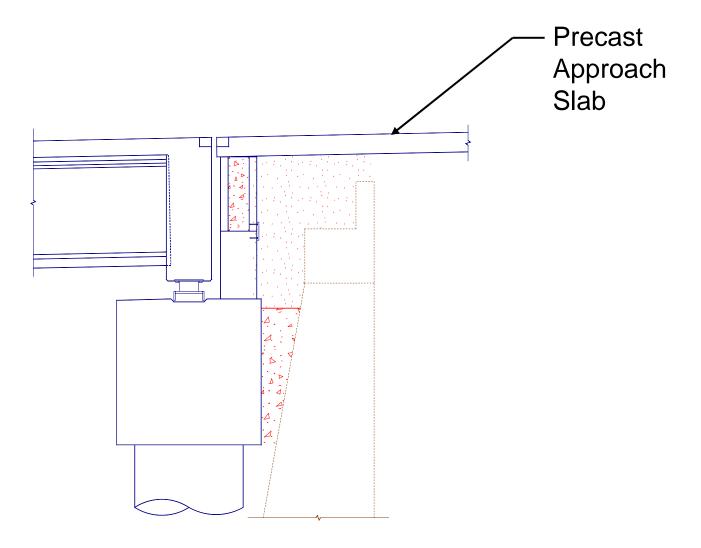












## **Existing Abutment Endwall Demo**



# Precast Abutment Endwall Construction



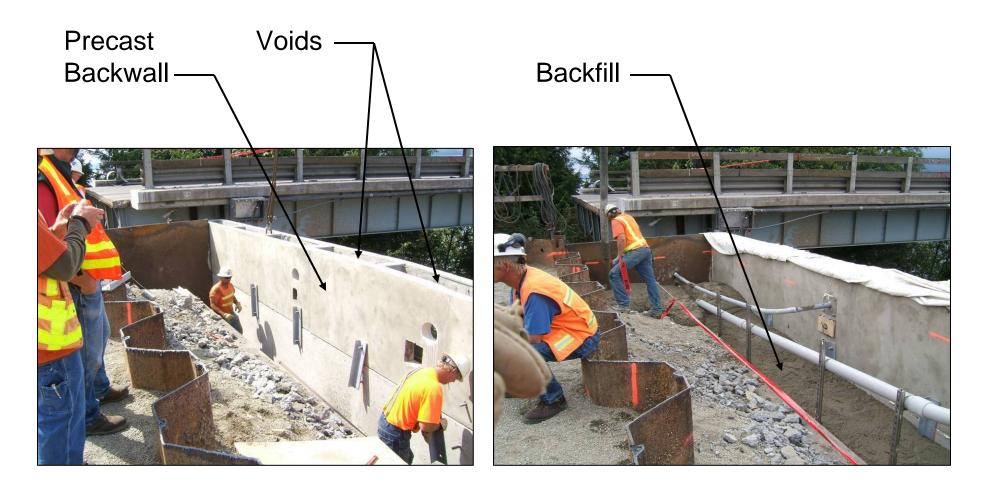
Cast-in-Place Endwall





Precast Endwall

# Precast Abutment Endwall Construction



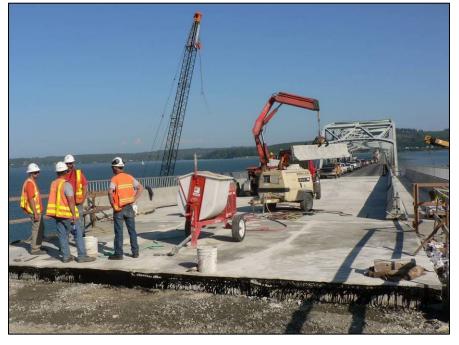
### **Precast Approach Slab**

- 6 Sections
- 25' x 8' x 1'-1"



# Precast Approach Slab







### West Approach Pier Demo



Remove top of Pier 2



### **West Approach Rolled**

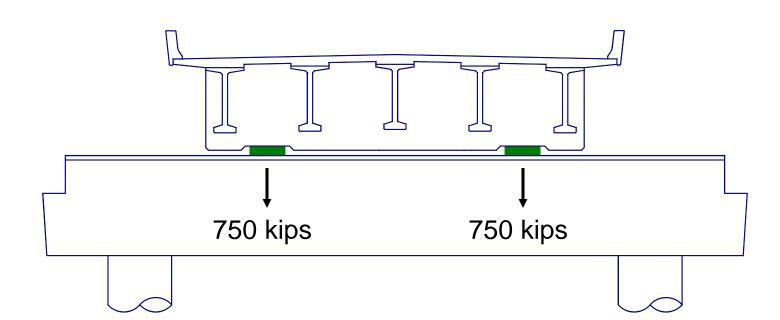


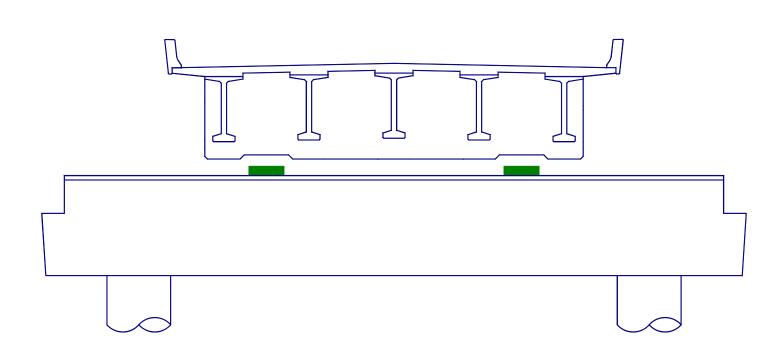
## **East Approach Pier Demo**

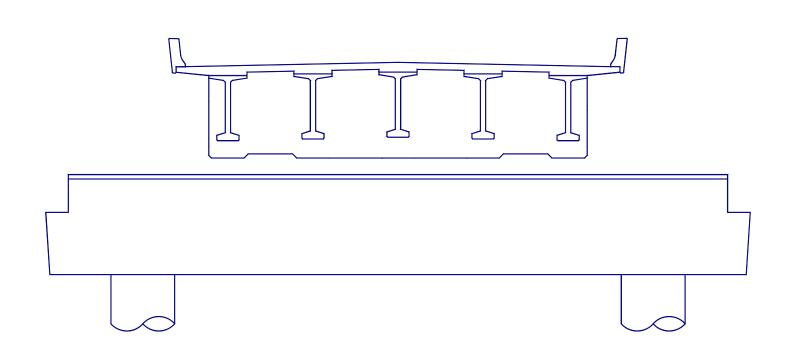
- Remove top 3' of Pier 7
- Sawcut horizontally and vertically
- Partially sawcut prior to closure

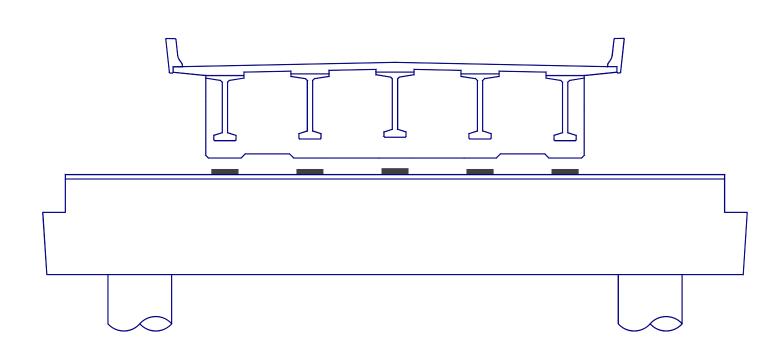


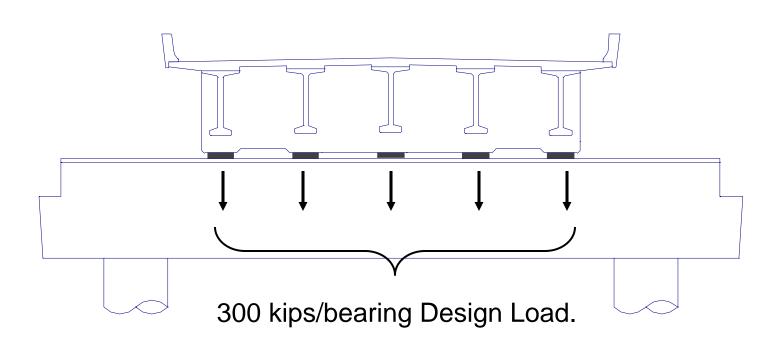


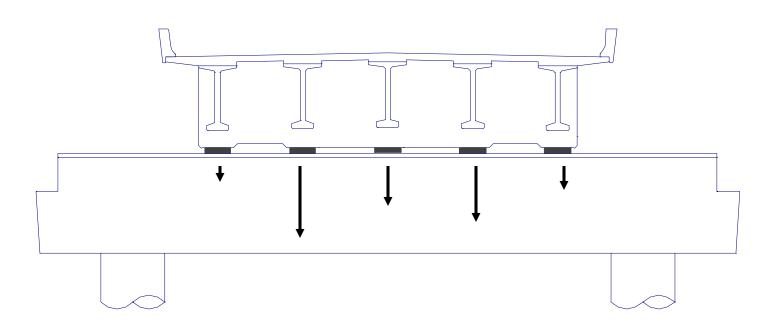












# **Lessons Learned**

- Unequal Bearing Loads
- Jacking and shimming required

Design DL = 300 kips Estimated DL = 500 kips





After Shimming

Prior to Shimming

